ANALYSIS OF FACTORS INFLUENCING ENERGY CONSUMPTION AT AN AIR FORCE BASE

I. Introduction

General

Reducing energy consumption has long been a stated goal of the Department of Defense (DoD). DoD is the largest single energy consumer in the United States; the department consumes 1.6 percent of the total in this country, and approximately 85 percent of the energy consumed by the federal government (Drezner et al, 1994). While energy costs only comprise a small part of DoD's operating expenses, the cost is still significant. Management of energy consumption is of particular interest to base engineering organizations, as utility costs generally are the largest single expense in their annual operating budget. Energy conservation has been an issue since the crisis precipitated by the 1973 oil embargo by the Organization of Petroleum Exporting Countries (OPEC), and has continued to receive attention from Congress and the executive branch since then. It is likely to continue to be an issue as installations strive to improve their pollution prevention efforts, of which energy conservation is a subset. Certainly, energy conservation is sure to be an area of concern for base engineering personnel in DoD for the foreseeable future.

Air Force energy managers face many challenges in performing their duties at the installation level, as well as at higher levels. The Air Force operates hundreds of installations worldwide, in a wide variety of environments. Some bases are located in extremely cold, even arctic, conditions. Most of the energy consumed at these bases is used to heat the base facilities. Others, in hot climates, use the majority of their energy for cooling, both for the comfort of personnel and to avoid damaging sensitive equipment. Likewise, the source of energy purchased

by the installations varies widely with location. Many bases in cold climates operate central heating plants, which serve a number of buildings, in order to increase efficiency. Many of these use coal as their energy source. Some installations have a large number of heating systems which consume fuel oil, although most are attempting to switch to natural gas. All installations use electricity, and much of the conservation effort has been in this area.

While DoD and the Air Force have been practicing energy conservation for over 20 years, not enough is yet known about the factors which influence energy consumption. If the Air Force is to meet the aggressive goals which have been set for reducing energy consumption in the future, we must continue to search for factors which influence energy consumption so that we can more effectively operate our installations with limited resources.

Background

Energy consumption in the DoD has been an issue of concern to leaders since the Arab oil embargo of 1973. In the period preceding that time, the United States had become increasingly dependent on imported oil, the majority of which originated in the Middle East. In 1973, the OPEC imposed an embargo on oil exports in retaliation for the United States' support of Israel in the Yom Kippur war. The result was widespread energy shortages which impacted much of the United States.

Between 1950 and 1973, the price of energy actually decreased in terms of real dollars. The price of residential electricity fell by 55%; gasoline by 21%; and natural gas by 20%. As a result, following the laws of supply and demand, energy consumption increased. Over the period mentioned above, per capita electricity use increased by 350%; natural gas consumption increased by 60% (Buttolph, 1982).

Beginning in October of 1973, and continuing through March 1974, OPEC countries reduced oil production, and imposed embargoes on specific countries, including the United States. From September to November of 1973, the supply of oil from Arab nations was reduced by over 4 million barrels per day. The fact that this quantity amounts to less than 8% of world oil production is indicative of the fact that there was not much spare production capacity at that time; hence the OPEC countries were able to exercise a high degree of control over the level of reductions imposed on importers as a group (Krapels, 1980).

Following the oil embargo, the reduced supply of oil, as well as its increased prices, caused energy consumption to decline rapidly. Over the two year period from 1973 to 1975, per capita energy use in the United States declined by 7%, and total use declined by 5%. (Buttolph, 10) This is especially significant when one considers the changes that would have occurred in order to precipitate this change. Many of the changes which would occur later, and which would be encouraged by national policies, involved making changes in facilities, vehicles, and utilities to make them more energy efficient. However, these are long term changes, and two years is insufficient time to implement them to any degree. Hence, these figures show that Americans were taking the energy crisis seriously, and were changing their behavior patterns as a result.

The federal government, following the lead of other American consumers, began to take measures to change its behavior patterns soon after the crisis. The first major piece of legislation to address energy consumption in federal facilities was the Energy Policy and Conservation Act (EPCA) of 1975. While including few details about how to achieve energy savings, EPCA directed the President to develop a comprehensive energy management plan.

At the same time, the Defense Energy Information System (DEIS) was established. DEIS provided a means to centrally manage energy information from all Department of Defense (DoD) installations. Quantities of energy consumed are reported monthly and are broken down by energy type. Some factors which may drive energy consumption are also reported. DEIS is broken down into two subsystems: DEIS I, which manages petroleum products used to support transportation, training, mobility, and readiness requirements; and DEIS II, which manages consumption data for the installations' physical plants.

The separation here is important; the consumption tracked by DEIS I was consumption largely driven by external forces such as mobility commitments. While operating more efficiently was made a goal, in many cases to do so is impossible due to mission requirements. Mobility energy has historically comprised 75 to 80 percent of total DoD energy consumption (Drezner et al, 1994). Facility energy consumption (the DEIS II data) generally comprises only 20 to 25 percent of the total (Drezner et al, 1994); however, much of the focus of energy conservation efforts is in this area. A third category, industrial facilities energy, is also included in the DEIS II data. Some installations, such as depots, operate specialized equipment used for repairing or overhauling equipment, and the energy consumed by this equipment is reported separately from that used to support the facilities themselves. Historically, the energy consumed by industrial process equipment comprises less than 5 percent of total energy consumption (Drezner et al, 1994). So, with the advent of DEIS reporting less than two years after the beginning of the energy crisis, DoD energy managers acquired a useful tool for managing energy conservation efforts.

In 1977 Congress passed the Department of Energy Organization Act (DOEOA). This act established a management committee consisting of an assistant secretary or assistant administrator from all major federal departments and agencies. The intent of the formation of this committee was to provide a forum to focus on national energy conservation issues rather than issues specific to one department or agency.

Also in 1977, President Carter issued Executive Order (EO) 12003, which set forth the first energy consumption reduction goals for federal facilities. The goals stated were to develop a conservation plan which would reduce energy consumption in existing facilities by 20 percent between 1975 and 1985. Also, a goal was set to reduce energy consumption by 45 percent in all newly constructed facilities.

The National Energy Conservation Policy Act (NECPA) of 1978 built upon some of the provisions of the EPCA of 1977. Whereas EPCA was very general and contained few details concerning how to implement an energy conservation policy, NEPCA contained some specific instructions. One such instruction specified the use of a life cycle costing methodology as the basis of energy policies. Also, facility energy audits were mandated for all facilities whose size exceeded 1000 square feet.

In 1988, the Federal Energy Management Improvement Act (FEMIA) established new goals as a follow-on to those established by EO 12003. The goals were to reduce energy consumption in federal facilities by 10 percent between 1985 and 1995. This act also marked the first time that a level of savings was specified for energy expenditures.

The National Defense Authorization Acts (NDAA) for the years 1989 through 1991 provided an incentive for installation-level commanders and managers to reduce their

consumption by allowing them to retain a portion of the funds saved by energy conservation measures. This provision of the NDAA also promoted continuing funding of energy conservation programs by requiring that two-thirds of the funds retained be spent on additional energy conservation programs; the remaining funds could be used at the installation commanders' discretion for base improvements or to improve morale.

EO 12759 was issued in 1991. It contained revised federal facility consumption goals, requiring a 20 percent reduction from 1985 to 2000. It also required a 20 percent reduction in energy consumption at industrial facilities by 20 percent during the same period.

The most recent legislation to address federal energy consumption, The Energy Policy Act (EPA) of 1992, contains a long list of specific instructions directing federal agencies to undertake specific actions to reduce their energy consumption.

In the future, it is likely that energy consumption will be addressed in terms of pollution prevention in addition to the current emphasis on reducing energy consumption in order to meet fiscal and resource constraints. This will bring a new set of players into the energy management arena, as current energy policies are generally implemented through the DOE. Many of the pollution prevention policies are implemented through the Environmental Protection Agency, and it remains to be seen what effect this potential sharing of responsibility would have on energy management within DoD.

This brief overview of the impact of the crisis brought on by the OPEC oil embargo of 1973, and its effect on federal energy conservation policy, shows how the emphasis has increased over the last twenty-two years. Energy conservation originally began as a reaction to reduced petroleum supplies and the effects of these reductions upon energy prices. The goal of the

conservation policies was twofold: first, to reduce the energy requirements of the federal government and its vulnerability to pressures from overseas suppliers; second, to reduce operating costs for all federal facilities by reducing the amount that must be spent on energy to maintain those facilities.

Problem

The DoD has set a goal of reducing facility energy consumption per square foot of floor space by 20 percent by the year 2000, using 1985 as a baseline. Initially, progress was able to keep up with the goal. However, in recent years that progress has slowed (Nelson). Currently, the Air Force Civil Engineering Support Agency (AFCESA) is unsure what is causing the slowdown.

The issue of energy consumption will be receiving more attention in the future, as the EPA of 1992 and EO 12759 have mandated additional goals and management actions. The types of programs available to energy managers have become much more aggressive in recent years.

Programs such as Shared Energy Savings (SES) contracts, in which no initial investment on the part of the government, have become more commonplace—the contractors agree to receive a portion of the funds saved by improvements made to facilities as payment for making the improvements. Energy audits have received more emphasis as well. The Department of Energy (DOE) was required by the Energy Policy Act of 1992 to establish energy audit teams and make them available to other agencies.

Although these programs and others will be a great help to energy managers and to commanders who wish to reduce energy consumption at their installations, it is likely that the returns from such programs will diminish over time. This is due to the fact that most of the

changes which can provide a large energy savings for a relatively small investment will be prioritized and funded early on; the remaining improvements will most likely be harder to identify, prioritize, and fund.

The goals which have been set are to be applied to all bases in an identical fashion; all bases are to reduce their energy consumption by 20 percent by the year 2000. However, there may be factors beyond the control of commanders and Base Civil Engineer personnel that may make the task of reducing consumption easier for some bases than for others. This is especially true as the programs mandated by the Energy Policy Act of 1992 take effect and the high value/low investment improvements are made at various. Air Force facilities. Once these are made, further improvements that may be necessary in order to equalize energy consumption among various facilities may require a higher capital cost, which may or may not be available.

If this is the case, knowledge of the factors inherent to a given facility that influence energy consumption will be of great value to both base level personnel and personnel at higher levels who must compare bases' energy conservation performance. For example, if per-square-foot energy consumption is driven by the number of aircraft assigned to a base, and the number assigned to a given base is reduced, then that base should reduce their energy consumption by more than the 20 percent goal. Conversely, if the number assigned is increased, they should not be required to meet the goal of 20 percent reduction, but rather some lesser goal. A more equitable means of setting goals would be to determine what factors drive per-square-foot energy consumption, and then to use these factors to generate activity indices which would create base-specific goals. While the DoD would still reduce overall energy consumption by 20 percent by the year 2000, more of the burden would be borne by bases which are more capable of reducing

their consumption. This knowledge could also be used during future base closure decisions, because it would be advantageous to close a base at which energy use reduction is more difficult.

Knowledge about which factors most influence energy consumption would also be useful for factors which are under the control of base personnel. Base Civil Engineer organizations generally are resource-constrained; managers must constantly make decisions regarding the prioritization of competing uses for money, manpower, and materiel. By spending his limited energy conservation resources on items which will have a maximum impact on energy consumption, a manager will be able to maximize the use of these resources.

Objectives

This thesis will have two objectives. The first objective will be to identify certain inherent characteristics of DoD installations which influence facility energy consumption. These characteristics may be either quantitative, as in square feet of facility floor space, or qualitative, as in which command operates a particular base.

The second objective will be to use these factors to develop a model to predict energy consumption at an Air Force base. The predictions developed by this model could then be used for either planning or baselining purposes.

Scope

This thesis will consider only bases located in the continental United States (CONUS).

The energy consumption figures obtained through AFCESA personnel will be assumed to have been accurately reported. Also, the energy purchased during a given month will be assumed to have been consumed during that same month. This is a straightforward assumption for electricity

and natural gas purchases, but is not so for coal and fuel oil, which may be stockpiled. The data from fiscal years 1991 through 1994 will be considered.

II. Literature Review

Introduction

Before describing the methodology used in this thesis to analyze factors which influence energy consumption at Air Force bases, a review of previous efforts to identify similar factors at military installations is necessary. Several studies have been completed in the Department of Defense following the 1973 oil crisis; the scopes of these studies varied widely. These studies can be generally categorized as macro or micro scale, and as type-specific or type-nonspecific.

Macro scale studies involve data gathered on an installation level from a wide number of installations, and generally do not include energy data gathered on a facility-by-facility basis.

Some macro scale studies, while considering installation-level energy consumption, were limited to specific types of installations. Micro scale studies, on the other hand, include data from a relatively small number of installations, and consider energy consumed by each individual facility in the study.

Type-specific studies consider energy of only one type, such as electricity, natural gas, coal, or heating oil. Type-nonspecific studies, conversely, convert energy consumed in all types to a common unit, usually million British thermal units (MBTU).

A search of literature reveals that no studies have been done to date to attempt to develop factors which influence Air Force installations' energy consumption on a macro scale and typenonspecific level. However, previous research efforts have contributed to a knowledge base of factors which are highly likely to influence consumption, and also provide several factors which will be considered as candidates in this thesis.

This literature review will consider only those studies which relate primarily to facility energy consumption. A number of studies have also been done which attempt to predict consumption of petroleum distillates for readiness or mobility purposes. Consideration of those types of energy consumption is beyond the scope of this thesis.

Results of Other Department of Defense Studies

<u>U.S. Army</u>. The U.S. Army has been active in researching factors influencing facility energy consumption since shortly after the 1973 oil crisis. Through both the Facilities Engineering Support Agency and the Construction Engineering Research Laboratory, several studies have been accomplished on various levels.

1977. This, the first energy consumption study published by the U.S. Army Corps of Engineers, was a macro scale, type-specific study which considered heating oil delivery data for buildings at three Army installations in the Washington, D.C. area (Botros, 1977). The objective of this effort was to identify the building types which are the largest consumers of heating energy, and therefore have the greatest potential for application of conservation measures. Using fuel oil consumption data ensures that the energy will be used only for a specific facility, as each facility generally has its own heating oil storage tank.

Twenty-four different types of buildings were identified for the study; monthly fuel oil delivery data were collected for fiscal years 1975 and 1976. Using this data, heating consumption for each building type was computed in British thermal units (BTU) per thousand square feet per year. The results of the study are given in table 2-1. The types of facilities which were the largest consumers of energy were found to be maintenance and community service facilities. These facilities generally have high ceilings and, in the case of

Table 2-1 Ranked Consumption by Consumer Group (Botros, 1977)

Rank	Building Type	Heating Consumption BTU x 10 ³ /ft ² /year
1	Fire Station	323*
2	Museum	302^*
3	Theater	213
4	Gymnasium	213*
5	Band Auditorium	210^*
6	Motor Repair Shop	176
7	Field House	169 [*]
8	Chapel	156
9	Enlisted Barracks	136
10	General Instructional Building	g 123
11	Library	117*
12	Post Exchange	106
13	Officers' Mess	102*
14	Bachelor Officers' Quarters	102
15	Enlisted Mess	101
16	Laboratory	100
17	Recreation Center	99
18	Warehouse	93
19	Enlisted Barracks with Mess	89
20	Administrative Office	86
21	Officers' Family Housing	85
22	NCO Family Housing	64
23	Commissary	41
24	Bowling Alley	36 [*]
*Denotes	single sample	

maintenance facilities, large bay doors which allow the escape of heated air when opened.

While providing a good deal of insight into which facilities require the most heating energy, this study was too limited in scope to allow application of its results to installations other than the three considered. It did not consider heat from sources other than fuel oil. Also, the three installations studied were in the same geographic area; the results could be different in

another climate. For some of the building types, and for half of the ten highest consumers, only one sample was obtained. Finally, only heating energy was considered. While information concerning heating energy is useful, for many of the types of buildings identified the amount of energy used for cooling could equal or exceed that used for heating. Nonetheless, the information identified is valuable and shows that there are wide variances in the amount of energy used among different building types.

1979. In 1979 the Army published the results of a study of facility energy consumption begun in 1976 (Sliwinski et al, 1979). There were three goals of this study: "(1) to collect data relating to the flow, demand patterns, and uses of the various forms of energy consumed on Army installations, (2) to compile a data file for use in later analysis, and (3) to analyze the collected data to determine how the energy was consumed, identify conservation measures, and improve energy utilization."

This study was conducted as a micro scale, type-nonspecific study. Three Army installations were studied: Fort Belvoir, Virginia; Fort Carson, Colorado; and Fort Hood, Texas. These posts were chosen for their dissimilar sizes, missions, and geographic locations. The facilities on each installation were divided into consumer groups based on the Army's real property inventory system. Seven major categories were used: troop housing, family housing, administration and training, medical and dental, community support, storage, and production and maintenance. A total of 114 buildings were selected for the study. An effort was made to select similar buildings at each of the three locations in order to assess the effects of climate and operational variation on energy consumption. Equipment was installed at each facility to monitor both electricity and heating energy consumption. In addition, the local weather was monitored in

order include information concerning heating degree days (HDD) and cooling degree days (CDD) in the analysis of the data. A heating or cooling degree day is defined as the departure of daily mean temperature from 65 degrees Fahrenheit. If the daily mean temperature is below 65 degrees, then the difference is expressed in heating degree days; if it is higher, then it is expressed in cooling degree days. Degree days (heating or cooling) may be summed to produce quantities such as monthly heating/cooling degree days.

The data used in the report were collected between September of 1976 and January of 1978. The results of this study in terms of average annual energy consumption by consumer group are shown in Table 2-2. In this table, as in the original report, two of the seven categories are further broken down into subcategories. Troop housing was divided into three groupings: "old" barracks, which were constructed prior to 1966; "new, nonmodular" barracks, which were constructed after 1966 but do not conform to the new modular design; and "new, modular" barracks, which represented the Army's current design at the time the report was written. Community facilities were divided into two categories: clubs/commissaries, and fieldhouses/gymnasiums. This distinction was made for heating energy only, and thus is likely an effort to take into account the large open spaces in the latter category. The largest consumers of heating energy, as determined by this study were modular barracks, community facilities, maintenance facilities, and medical/dental facilities. Maintenance and community facilities were also found to be among the highest consumer groups in the earlier study of heating energy by the Army Facilities Engineering Support Agency.

One characteristic of this study which distinguishes it from the previous one is that it develops a predictive capability. For each category of building, a regression equation was

Table 2-2 Average Annual Energy Consumption by Consumer Group (Sliwinski et al, 1979) (Energy/ft²/year)

		Electric (KWh)				
Building Type Heating	ng (MBTU)	Air Cond	Non-Air Cond			
Family Housing	1.27	8.49	6.06			
Troop Housing						
Old	1.18	N/A	2.37			
New, nonmodular	.63	7.96	5.55			
New, modular	2.59	N/A*	5.55			
Administration/Training	1.12	1	12.37			
Community Facilities		2	24.49			
Fieldhouses/gyms	1.70					
Clubs/Commissaries	1.40					
Maintenance	2.08		9.82			
Medical/Dental	2.00	1	15.99			
Storage	1.73		5.04			
*Cooling supplied by central plant.						

developed which could be used to predict energy consumption at other installations using square footage of each type of building, as well as HDD and CDD. Prediction of energy consumption at the installation level would require a detailed inventory of the number of square feet of each type of facility. The accuracy of such a prediction would depend on the similarity of the installation's buildings to those used in this study, and the prediction would not account for energy that is consumed by systems not associated with any particular facility, such as water pumps and street lights.

1980. The objectives of this study were to "(1) describe how electrical energy is being used on military installations, (2) describe the major causes for changes in electrical energy usage, and (3) suggest operational changes and equipment techniques that will reduce electrical

energy consumption which Facilities Engineers can use to plan and execute effective electrical conservation programs." The study was a micro scale, type-specific one (Windingland, 1980).

Two Army installations were used in this study: Fort Carson, Colorado, and Fort Belvoir, Virginia. The data gathered for this report consisted of two distinct types: consumption data for twenty buildings on the two installations, collected on both an hourly and a monthly basis; and electrical feeder consumption, collected on both a daily and monthly basis. The feeder data was collected for Fort Carson only, and measured the total electrical consumption on the eight feeders which distribute commercially obtained electricity to the various areas of the installation.

The feeder data were initially collected in order to try to identify the major consumers of electricity on the installation by area; however, this was not possible due to the wide month-to-month fluctuations in feeder consumption. The daily consumption figures were used to determine what portion of the installation's electrical consumption can be considered "baseline" and what portion is due to operational activity. This was accomplished by comparing the consumption on a Sunday (when it can be assumed that most buildings are unoccupied) to consumption on a Tuesday. Based on this data, the report stated that approximately 70 percent of an installations electrical consumption is due to baseline activities; the remaining 30 percent is due to operational activity.

The individual facilities monitored were located at both Fort Carson and Fort Belvoir. For each building, the monthly electrical consumption, weekday and weekend daily consumption, and hourly minimum and maximum demands were measured. From this data, the results of the feeder measurements were confirmed; that is, a major portion of a building's energy consumption takes place during unoccupied or nonduty hours. Although the seasonal data were collected in the

hopes of establishing a trend for higher consumption during the heating or cooling season, there did not appear to be any significant trends. Some buildings evidenced higher consumption during the summer months (which is to be expected due to air conditioning equipment), but others had a higher consumption during the winter, and some buildings evidenced no seasonal trend whatsoever.

The main conclusion drawn by this study is that the minimum electrical demand of a facility, which may account for as much as 70 to 75 percent of its total consumption, is not related to building occupancy. Rather, this portion of electrical demand can be attributed mainly to heating and cooling system operation. This model did not attempt to develop a predictive capability; rather, it failed to validate building occupancy as a factor which influences energy consumption at an Army installation.

1986. This study attempted to correlate the effects of production level and other measures of level of activity to energy consumption at these facilities (Sliwinski, 1986). This study was macro scale and type nonspecific, although the scope was limited in that only AMC installations were considered. It was undertaken because although energy consumption within AMC declined by 26 percent between 1975 and 1981, the level of production decreased during the same period as well. It was felt that some means of tying energy consumption to level of production was necessary in order to accurately measure the effectiveness of energy conservation measures.

Energy consumption data was gathered for the period 1975 through 1983, as well as data regarding weather and process parameters at each installation. Multiple regression analysis was used to develop prediction equations for both the individual installation level and for the entire

command. It was found that the estimates for the entire command were generally more accurate, probably because of the averaging effect of having a large number of installations within the population.

Two distinct groups of installations were noted. For the first group, only heating degree days seemed to have a significant influence on energy consumption; for the second, heating degree days and the size of the labor force had influence. The author felt that his model could enhance evaluation of energy conservation programs by allowing prediction of energy consumption at an AMC installation, but at least in the case of the first group it appears that the goal of finding a link between production level and energy consumption at AMC installations was not achieved.

U.S. Navy

This effort was intended to improve the methods used to evaluate progress toward energy conservation goals (Buttolph, 1982). It involved data collected from Naval Regional Medical Centers (NRMCs) and considered the effects of both seasonal weather variations and of categories of use on total energy consumption. This was a macro scale, type-specific study. It considers only electricity use, although it continually refers to electrical consumption as energy consumption as though all energy types have been considered. Also, while this is a macro scale study because it considers the aggregated energy consumption for each NRMC, these are somewhat specialized installations and could not be considered to be representative of Navy installations.

The data base used consisted of monthly electrical consumption data from twelve NRMCs located in various climates. The data was collected during fiscal year 1975, which was also the baseline year for the first mandatory conservation efforts within the DoD.

The study was conducted in two phases. In the first, regression models and time series analysis were used to develop forecasting models for energy consumption. The regression model chosen as the best model used heating degree days (HDD), cooling degree days (CDD), and precipitation as independent variables. Average monthly temperature was also considered as an independent variable, but was not included in the model for simplicity, and also because it was strongly correlated with both heating degree days and cooling degree days.

The second phase of this study attempted to forecast energy use as a function of the areas of different types of functional uses of total floor space. Ten categories were created to account for the different uses of floor space within the NRMCs: mission (hospital space), personnel living space, maintenance/industrial, data processing, administrative, commercial, morale and welfare (community services), morale and welfare (recreation), and storage. Regression was then performed using all ten categories as independent variables, and the number of categories used in the model was reduced. The study found that a model using only three of the categories, mission, storage, and maintenance/industrial would provide satisfactory results. However, it also stated that the data base used was too small to support a test for all ten categories of use.

The results of this limited study show, first, that climatic conditions strongly influence electrical consumption at NRMCs, and also that certain types of use category contribute more to electrical consumption than do others. This corresponds to the conclusions drawn by the Army studies. Only one of the three use categories used in the three-variable model was identified by

the Army studies as being a high energy consumer, maintenance/industrial. This author feels that this may be due to the fact that NRMCs are more specialized facilities, while the facilities considered by the Army studies are parts of much larger installations. Still, the information provided by this study is valuable in that it clearly supports a belief that the use of a given amount of floor space to some extent determines the rate at which it will consume energy.

Defense Logistics Agency

This study's goal was to develop a methodology to develop energy consumption goals based on factors which may vary from month to month, rather than the method then in use of basing consumption goals on the previous year's consumption. The study was a macro scale, type-nonspecific one, although it also broke energy consumption down into electric and non-electric, as well as total energy usage (Defense Logistics Agency, 1988).

Three years of monthly energy consumption data were used for this effort. The factors considered were developed by surveying all Defense Logistics Agency (DLA) installations which were accountable for their own energy use to determine what factors the installation managers felt influenced their energy consumption. These factors were then evaluated using regression, and the factors which did not have a significant impact were discarded.

The result of the regression analysis was that the models which were developed produced confidence intervals which were uselessly large, and therefore could not be used in setting energy consumption goals. However, the models did show that a definite relationship exists between climatic and workload factors and energy consumption. This somewhat contradicts the findings of the 1980 CERL study, which found that most of a facility's energy is consumed during unoccupied periods. This could be due, however, to the fact that DLA facilities are more likely to

involve energy-intensive industrial processes. The consumption of these processes may equal or exceed that of the heating, ventilating, and air conditioning (HVAC) equipment that the CERL study found accounted for the majority of the baseline energy consumption.

U.S. Air Force

1980. This was one of the earliest facility energy studies published by the Air Force Institute of Technology (AFIT) (Hatch and Mansfield, 1980). The objective was to examine the possibility of providing energy self-sufficiency for the five Air Logistics Centers (ALCs). The ALCs are relatively large, highly industrial facilities where overhauls and major repairs are performed on aerospace vehicles. In order to determine future requirements for achieving energy self-sufficiency, the authors developed a prediction model using data from all five ALCs. This study can be considered to be macro scale since it considers all energy consumed by each ALC, and type-nonspecific because it aggregates all energy consumed at each ALC regardless of source.

Monthly energy consumption data were gathered for the period from July 1975 through September 1979 for each ALC. These figures were then consolidated to produce an overall energy consumption figure. The energy consumption for the ALCs, measured in MBTU, was taken to be the dependent variable, and five independent variables were considered: square footage of floor space; heating degree days; cooling degree days; manmonths worked; and capital investment. These quantities were also consolidated for all ALCs to correspond to the consolidated energy figures. The first three independent variables were chosen for obvious reasons, and had been considered by earlier Army studies. Mandays worked was chosen to try to incorporate a level of activity indicator for the ALCs, and in this way to account for that portion

of energy used to support industrial processes. Capital investment was chosen to represent additional loads added to each ALC, whether in the form of additional space, or of additional process or industrial equipment.

The result of this analysis was that heating and cooling degree days were found to have the most significant influence on energy consumption at the five ALCs. The model presented by the authors uses only these factors to predict energy consumption for the ALCs. The authors state that the majority of energy consumed by the ALCs is for industrial processes rather than for heating and cooling, so these results are somewhat surprising; if their statement were true then manhours could be expected to influence energy consumption if it is a valid indicator of level of activity. However, the Army's 1980 study of Fort Belvoir and Fort Carson supports the authors' claim. As mentioned previously, that study determined that up to 70 percent of an installation's energy consumption was not tied to occupancy of its facilities, but instead was a baseline level, mainly consisting of HVAC loads. While the study of ALC energy consumption may be a special case since these are highly industrialized installations, that both studies agree strongly supports heating and cooling degree days as drivers of energy consumption.

1981 (Weck, 1981). This study of installation electrical energy consumption examined bases from various commands rather than limiting the study to one. It was a macro scale, type specific study which attempted to develop a multiple linear regression model to forecast electrical consumption at Air Force bases. The study considered heating and cooling degree days, total square footage of facilities, and base population as prospective independent variables, and used data from fifteen bases located in the continental United States. The bases were chosen specifically for their varying sizes and climates, and also represented three different major

commands. Monthly consumption data was gathered for the seven years between fiscal year 1975 and 1981.

Although energy consumption figures for military family housing (MFH) are recorded and reported separately in the DEIS II system, they were combined with other consumption figures for this study. The base population figures used for this study consisted of all assigned military and civilian personnel, Non-Appropriated Fund employees, contractor personnel, and all dependents residing in MFH.

The results of this analysis were that of the four factors considered, only heating and cooling degree days were found to be valid for use in a model to predict electrical consumption at an Air Force Base. Neither base population nor total facility square footage were found to be valid factors. That total facility square footage was not found to be a useful predictor is probably due to one of the assumptions that was made for this effort: that all facilities making up the total square footage of a base consume electricity at equal rates.

1981. Published at the same time as the one discussed previously, this was a study to develop a forecasting methodology for coal, heating oil, and natural gas consumption for Air Force bases (Tinsley, 1981). The same four parameters (heating degree days, cooling degree days, square footage, and base population) were used for this study as for the last one. Data from eight bases was used, and as in the previous study they were chosen for their differing sizes and climates. The data was gathered over the same period, from fiscal year 1975 to 1981. Both this effort and the previous one relied heavily on data from the DEIS II program for the dependent variable. The study was a macro scale, type-specific one, because although it considered multiple energy types, it excluded electricity.

This study uses multiple linear regression, as well as the more advanced techniques of moving averages and exponential smoothing, to try to develop a model to predict consumption of these heating fuels at Air Force bases. The objectives were to first find the most appropriate method for predicting heating energy consumption, then to identify which of the four parameters are most important, and finally to develop a model which may be used by energy managers to predict future consumption.

The study found that multiple linear regression was the most appropriate forecasting technique, and that the use of all four variables in the prediction model produced the most practical model and the best results. Both this study and the previous one noted also that there were relationships among the independent variables, especially heating and cooling degree days. A high number of heating degree days would indicate a cold climate and thus a likelihood of fewer cooling degree days. Conversely, a hot climate would likely produce many cooling degree days and fewer heating degree days. The models developed by these two studies may be of limited use separately since one considers only heating energy and one considers only electricity, but used together they may enable fairly accurate predictions. The feasibility of combining the two models has not been examined.

1983. This effort sought to evaluate the effectiveness of Energy Management and Control Systems (EMCS) as a conservation measure (Boulware and Williamson, 1983). (For readers unfamiliar with EMCS, it is a system which automates the operation and control of HVAC systems and theoretically ensures that they are operated in an energy efficient fashion. They may consist of centrally located computer equipment, as well as remote sensors and electromechanical HVAC controls). In order evaluate EMCS's effectiveness, it included development of a multiple

linear regression model for energy consumption. This was a macro scale, type-nonspecific study which used data from twelve bases (eight with operational EMCSs) to develop a model to predict energy consumption. The authors then compared these predictions to actual energy consumption to determine whether any actual savings were realized.

Data was collected for the period from October 1974 to September 1982. The following factors were considered as possible drivers of energy consumption: heating degree days, cooling degree days, population, total square footage, number of EMCS sensor/controller points, number of buildings controlled by EMCS, and dollar value of energy projects. A dummy variable was also used to represent the presence or absence of an operational EMCS system. The role of the dummy variable will be explained in a later chapter.

The result of this study's multiple linear regression analysis was that five variables were identified as having a significant influence on energy consumption. They are, in decreasing order of significance: heating degree days, cooling degree days, population, dollars value of energy projects, and total square footage. Also, EMCS was found to contribute to energy conservation efforts, although it appears that as little as one percent savings may be attained. Also, some of the data seemed to indicate that energy consumption at ALCs may be tied more closely to industrial processes than to facility energy consumption. The data for McClellan AFB, which is an ALC, indicated that energy consumption there has risen steadily over the period of the study. This is a contrast with all of the other (non-ALC) bases, whose energy consumption declined.

1985. Another AFIT study, this one sought to evaluate the effectiveness of the thencurrent method of measuring energy conservation progress (Morrill, 1985). This was a macro scale, type-nonspecific study which used data from 77 Air Force bases. Annual energy consumption data was gathered for the period from 1980 to 1984. Fifteen independent variables were selected for multiple linear regression analysis. These are shown in Table 2-3.

This effort differed from previous Air Force efforts in two important ways. First, it considered total annual consumption rather than the monthly consumption considered by most previous studies. The advantage of this approach is that it may reduce the impact of seasonal fluctuations caused by the switch from heating to cooling seasons. The second way that it differs is that in addition to the actual values of quantities such as heating and cooling degree days, it also considers the impact of changes in these quantities. It also considers the representativeness of CDD and HDD values for each installation in the baseline year of 1975, since consumption in that year was being used for comparison at the time this thesis was written. This was accomplished by comparing the values with climate data for the installations.

The result of this study's multiple linear regression analysis is that nine of the fifteen independent variables were determined to significantly affect energy consumption at an Air Force Base; these nine variables are identified in Table 2-3. One interesting note is that bases which belonged to Tactical Air Command (TAC) were found to have more successful energy conservation programs than other commands' bases. Overall, the regression model for energy consumption developed by this thesis only accounted for approximately 25 percent of the variability in bases' energy consumption. It also concluded that the current method of measuring bases' energy conservation progress, i.e. comparison to a baseline, does not provide a true indication of energy conservation efforts. There are many independent factors which drive energy consumption, and a model should be developed to try to include them in energy consumption projections.

Table 2-3 Selected Independent Variables (Morill, 1985)

Dependent Variable	Energy Conservation (percent reduction	
	in MBTU per square foot)	
	**	
	Major Command**	
	Climatic Zone	
	Base Mission**	
	Cooling Degree Days**	
	Heating Degree Days	
	Base Population	
Candidate Independent Variables	Costs of Completed ECIP* Projects**	
	Costs of Completed EMCS Projects**	
	Total Square Footage**	
	Cooling Degree Day Change	
	Heating Degree Day Change	
	Base Population Change	
	Total Square Footage Change (from	
	baseline)**	
	Baseline Cooling Degree Day Change**	
	Baseline Heating Degree Day Change**	
	*5	
	*Energy Conservation Investment	
	Program. This is a means of funding	
	EMCS and building/HVAC retrofit	
	projects through the Military Construc-	
	tion Program.	
	**Factors found to be significant after	
	multiple linear regression analysis.	
	multiple inical regression analysis.	

Conclusions

The various studies which have been performed by the various DoD agencies over the last two decades have been successful in identifying many of the factors which influence energy consumption at military installations.

In all studies in which they were considered, climatic factors were found to have an influence on energy consumption. This result is hardly unexpected, since a large portion of the facility energy consumed is used to support HVAC equipment. The weather conditions in which an HVAC system must operate will obviously influence the amount of energy consumed. Further, several of the studies noted that the three most commonly used measures of an installation's climate, HDD, CDD, and mean temperature, are not independent. An installation in a primarily cold weather climate will have a relatively high value for HDD, and relatively low values for CDD and mean temperature. For an installation in a hot weather climate, the converse would be true. Although the energy consumption models produced by different studies used differing combinations of these variables, the conclusion can be drawn that weather conditions have a significant influence on facility energy consumption.

The two Army studies which considered energy consumption in various types of facilities both concluded that there is a significant difference in energy consumption. However, the data set used for both of these was somewhat limited, consisting of a maximum of three installations. It is unclear whether the model developed could be applied to other installations.

Two studies of heavily industrialized installations, one by the Army and one by the Air Force, reached conflicting conclusions regarding the influence of level of industrial activity on energy consumption at these facilities. The Army study found that at some AMC installations, level of activity indicators could be included in an energy consumption model. The Air Force study of ALCs found that it was not a significant influence. Another study by DLA did conclude that level of activity indicators may have an influence on energy consumption, but was unable to develop a useful model. It is unclear whether energy at these installations is consumed in a similar

manner to other, more operations-oriented ones. It is clear from the 1980 CERL study that the majority of energy consumed by facilities at operational installations is used to operate HVAC systems; this same conclusion may not be true for more industrial installations.

Looking at all of the previous work summarized in this chapter, two conclusions can be drawn. First, multiple linear regression is the most appropriate method for predicting energy consumption at a military installation. Several other methods were examined, but the authors concluded that multiple linear regression had the best results. Second, climatic factors must be included in any energy consumption model. They are the only factors which were included in all of the models. It is not clear, however, which variables have the most influence.

So, while a definitive model has not yet been developed which can consistently predict energy consumption at a military installation, many of the factors which influence consumption have been identified. These factors will provide a starting point for this thesis, so that other factors may be added to try to create a model which will more accurately predict energy consumption at an Air Force Base.

III. Methodology

Introduction

This chapter will present an overview of the process used to determine factors which influence facility energy consumption at an Air Force base. The chapter will be presented in three sections. The first will provide a general overview of the steps used to analyze the data, from definition of the population to the development of the final multiple linear regression model. The second section will provide a more detailed description of the data collection process, and the third will describe the statistical tools used to analyze and characterize the data. A small subset of the set of data analyzed in chapter IV will be used in this section for illustration purposes.

Overview of Methodology

In chapter I, two research objectives were defined. The first was to identify a set of variables which could be used to predict energy consumption at an Air Force base. The second was to use those variables to construct one or more models which accomplish this prediction. In order to accomplish these two objectives, a set of data was collected for a number of members of the population. Each observation in this data set consisted of a value for the dependent variable, as well as several candidate independent variables. The choice of candidate independent variables was guided by the previous research summarized in chapter II. The candidate variables were evaluated using the techniques described later in this chapter, and those which are determined to have low predictive value were discarded. Using some additional statistical techniques, an attempt was made to group the observations based on characteristics of the bases they represent. For each group, a multiple linear regression (MLR) model was created. For one such grouping,

additional information about the bases' infrastructure was collected through the base civil engineers' Work Information Management System (WIMS). Finally, a second MLR model was developed using this additional information.

<u>Population</u>. The population in this case consists of all active duty Air Force installations (Reserve installations were excluded) which record energy consumption and report it to the Air Force Civil Engineering Support Agency (AFCESA), located at Tyndall AFB.

Sample. The sample consisted of all Air Force installations located within the continental United States (CONUS) and belonging to the five major commands (MAJCOMS) which oversee the operation of more than one base. A brief description of each MAJCOM follows. These descriptions are not intended to duplicate the mission statements or descriptions of the MAJCOMS; rather, the intent is to provide a brief synopsis of the types of activities at each MAJCOM's bases:

<u>Air Combat Command (ACC)</u>: Operates bases from which fighter, attack, bomber, tanker, and intra-theater airlift aircraft are flown and maintained.

Air Mobility Command (AMC): Operates bases from which inter-theater transport and tanker aircraft are flown and maintained from both training and operational airlift missions.

Air Force Materiel Command (AFMC): Operates bases which perform functions related to research, development, design, testing, procurement, and depot level maintenance of aerospace and related systems.

<u>Air Education and Training Command (AETC)</u>: Operates bases which conduct basic military, technical, and flying training, as well as professional military education.

Space Command (SPC): Operates bases which launch, monitor, and control space systems.

Three other commands also operate bases within the CONUS, Special Operations

Command, Air Force District of Washington, and the U.S. Air Force Academy. However, these

MAJCOMS were not considered because each only consists of one base.

Description of Data

The majority of the data used in this thesis was obtained from AFCESA in the form of reports which detailed each base's inputs to the DUERS system. These reports were obtained for all of the bases in the aforementioned commands for the period from October 1990 to September 1994. Although the reports contained a great deal of information regarding costs and quantities of energy acquired from various sources, three independent variables (HDD, CDD, and SQFT) were initially used in this thesis. The values of all but one of these variables were reported on a monthly basis; thus for each base there are a maximum of 48 observations. Categorical variables denoting the controlling major command and type of mission for each base were used to divide the data into subgroups, and then data describing two additional independent variables and the dependent are described below:

Heating Degree Days (HDD): This independent variable represent the sum of all the daily heating degree days for each month. One heating degree day occurs for each degree of difference between the mean daily temperature and 65 degrees Fahrenheit. (Note: this variable has a minimum value of zero. If the mean daily temperature is above 65 degrees Fahrenheit, the value

of HDD will be zero and the value of Cooling Degree Days, below, will be positive). HDD is reported on a monthly basis.

Cooling Degree Days (CDD): This variable, also independent, represents the monthly sum of the differences between the mean daily temperature and 65 degrees Fahrenheit, when the mean daily temperature is above 65 degrees Fahrenheit. Thus, for a day on which the mean daily temperature is 70 degrees, the value of CDD would be 5. As is the case for HDD, this variable can only have nonnegative values and is reported on a monthly basis.

Million British Thermal Units per Square Foot (MBTU/SF): This variable is a measure of the total energy consumed per square foot of facility floor space, and is the dependent variable for this thesis. It is reported on an monthly basis. The energy may come from a number of sources; use of electricity, natural gas, coal, fuel (heating) oil, or purchased steam are common. The consumed quantity of each product is converted to MBTU using the following relationships, and the total is divided by the total number of square feet of facility floor space on the installation (Leigh, 1993):

Electricity: 3.413 MBTU per megawatt hour Coal (Anthracite): 25.4 MBTU per ton Coal (Bituminous): 25.58 MBTU per ton Natural Gas: 1.03 MBTU per 1000 cubic feet Fuel Oil Distillate: 5.825 MBTU per barrel Saturated Steam: 1340 MBTU per pound

This thesis is only concerned with the total quantity of energy consumed per square foot of floor space; no effort will be made to differentiate between energy obtained from different sources.

Square Feet of Facility Floor Space (SF). This is also an independent variable which represents the total facility floor space at an installation. It is only updated annually, so all the value of SF will be the same for each month of a given fiscal year. It was assumed that any

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increases or reductions in the amount of facility floor space occurred at the beginning of the year, and that the space was used for the entire year. There is no differentiation between the various uses of floor space; all uses are aggregated into this variable. It was assumed that all reported floor space is energized, even though this is probably not the case.

The following are the categorical variables which were used to evaluate dividing the data into subgroups:

<u>Presence of an Active Flying Mission (FLY)</u>. This is a categorical variable which identifies bases which support an active flying wing.

<u>Presence of a Depot (DEPOT)</u>. This is another categorical variable which identifies bases which support a depot used for the overhaul of either aircraft or space systems.

<u>Major Command (MAJCOM)</u>. This categorical variable identifies the MAJCOM which operates each base.

Analysis of these factors was used to divide the bases into subgroups for development of MLR models. Additionally, for some bases in Air Combat Command, information was collected regarding the bases' real property. Optimally, this data would have been obtained for all of the MAJCOMS, but time constraints placed on this research precluded such a comprehensive study. Air Combat Command was chosen because it is the largest CONUS command, which increased the likelihood of gathering a sufficient number of responses, and also because it operates bases in a wide variety of climates. The two additional variables which were added are:

Mean Age of Real Property (RPAGE). The value of this variable was obtained by use of a computer report program which queried each bases' real property inventory and determined total square footage and date constructed for selected real property category codes.

All Air Force facilities are assigned a category code which identifies the primary use of the facility. Since category codes are assigned to objects other than buildings, such as roads, sidewalks, runways, utility systems, and the like, only category codes which identify buildings were selected. The number of square feet in each facility was used to weight the mean age of facilities by the following procedure: For each facility, the age was determined using the date the facility was constructed. The age was then multiplied by the square footage for each facility. The total of these products (for all facilities) was then divided by the total quantity of facility floor space for each installation to determine the weighted mean age for the installation. An example of the spreadsheet used to compute this value is shown at Appendix A. Note that it also computes the average age of the facilities so that any wide deviation between these two quantities can be noted.

Ratio of Large Maintenance and Storage Facilities (MAINT). This variable reflects the percentage of the installation's facilities which are large, open-bay maintenance facilities. As mentioned in chapter two of this thesis, previous research efforts have identified these facilities as being greater energy consumers due to their high-bay doors which release heated or cooled air to the exterior of the building (Botros, 1977). This information was also obtained by means of a computer report program. It produced a spreadsheet similar to the one used to generate values for RPAGE, but with the date constructed omitted. Also, only the category codes associated with particular types of buildings were included. The facility floor area of maintenance and storage facilities was summed, and divided by the corresponding value of SF obtained from the DUERS data.

Since the computer report programs which generate values for both RPAGE and MAINT are only capable of querying the current real property inventory, only the current age and ratio

were able to be obtained. RPAGE was adjusted for each of the previous years by simply subtracting the appropriate number of years; however, this is inaccurate because it would not account for facilities which were demolished between October 1990 and the present. No adjustments were made to MAINT. The denominator of the ratio, total facility floor area, was taken from the FY 1994 DUERS report. The author felt that changing the denominator from one fiscal year to the next would add little value to the effort, since any changes in facility floor space which would affect the denominator would also have an effect on the numerator. Without access to previous years' real property inventories, the changes in the numerator could not be determined. These two independent variables were added to the group selected for additional study in an attempt to develop an improved MLR model.

Computer Software

The primary software package used to analyze the data for this thesis was Statistix 4.1. This is a program which is run on an IBM PC or compatible computer, and provides the ability to perform all of the statistical techniques which are described in this section (Statistix, 1992). The advantage of Statistix over minicomputer- or mainframe-based programs is that it is a menudriven, user friendly program. In addition to performing statistical analysis, Statistix was used to enter all of the data observation obtained for this thesis.

Evaluation of Candidate Independent Variables

Overview. This section will describe the various statistical tools used to evaluate each of the candidate independent variables, which have already been presented. This section is concerned with the methodology used to meet the first objective of the research, identifying factors which could be used to predict energy consumption at an Air Force Base. The evaluation began by using qualitative techniques to observe the behavior of the dependent variable relative to changes in each candidate independent variable. Also, relationships among the candidate independent variables themselves were examined. As the research progressed, the techniques used switched from qualitative to more quantitative method. Decision rules were formulated in order to eliminate certain of the candidate independent variables as statistically insignificant for modeling purposes. For each of these quantitative methods described in this section, the test statistic and the decision rule which were used will be specified. All of the analysis used in this thesis will employ a level of significance, or α , of 0.05. As mentioned at the beginning of this chapter, a subset of the sample used in chapter IV will be used to illustrate the methods described in the following sections. This subset consists of 79 monthly observations from seven AMC bases, and can be found at Appendix A-1.

Descriptive Statistics

Descriptive statistics are methods that are used for the "organization and summarization of data" (Devore, 1991). There are two general categories of descriptive statistics: pictorial and tabular, or numerical (Devore, 1991). Both methods were used to examine and present the data set in this thesis. A brief description of some of the specific techniques used is given below.

Several graphical techniques were used to examine the data points in a qualitative manner.

Performing this type of analysis prior to applying numerical analysis provided two benefits. First,

the qualitative analysis techniques helped to visualize relationships between the variables, as well as their distributions. Second, and equally important, these techniques made detection of erroneous values possible. Since all of the data had to be manually keyed into the computer, this was an important benefit. The three primary tools for performing qualitative analysis were histograms, box and whisker plots, Wilk-Shapiro/Rankit plots, and scatter plots. All of these techniques will be used in the following chapter to present the data and make inferences regarding the distributions of the variables.

A histogram of the data set is shown at Figure 3-1. At first examination, the data seems to be somewhat skewed right. However, the sample used for illustration purposes in this chapter is fairly small, and some other test will be performed to determine whether the data appear to be normal and the effects of any outliers, or extreme values.

Figure 3-2 is a box and whisker plot of the data. The box and whisker plot orders the data from smallest to largest observation, and then dividing it into fourths. The horizontal line across the center of the box represents the sample mean, and each half of the box represents the fourth above and below the mean. The two vertical lines extending from the box, the whiskers, represent the upper and lower fourths. Were there any outliers in the data set, they would be represented by an asterisk for a possible outlier, or a circle for a definite outlier. This plot is useful because it pictorially represents the center, spread, symmetry, and the presence of outliers (Devore, 1991).

Figure 3-1 Example Histogram A Wilk-Shapiro/Rankit plot is shown at Figure 3-3. This plot, and the accompanying Wilk-Shapiro statistic, are used to determine the normality of the data. If the data is normally distributed, this plot should appear to be linear. The Wilk-Shapiro statistic can assume values between zero and one, with higher values indicating that the data approximates a normal distribution. There is know threshold at which the data can be said to definitely approximate a normal distribution; some subjective judgement must be exercised.

Scatter plots help to visualize the relationship between two variables. The independent variable is plotted along the horizontal axis, and the dependent variable along the vertical axis. Scatter plots for three independent variables are given at Figures 3-4, 3-5, and 3-6. In the first the independent variable is HDD. This plot shows quite clearly that when HDD increases, MBTU also tends to increase. The second plot, CDD vs. MBTU, seems to show that as CDD increases, MBTU tends to decrease. However, the trend is not as clear as in the first scatter plot. The third plot, SQFT vs. MBTU, is not as useful as the first two since the independent variable has the same value for all monthly observations in a given year. Scatter plots were used in this thesis to find out which variables were valid candidates for regression modeling.

Tabular methods used include computation of summary statistics such as the sample mean, sample variance, and the like. These values may be used to make inferences about the population from which the sample is drawn.

For a sample consisting of n observations of a variable X, the sample mean, or x, is calculated as follows:

Figure 3-2 Example Box and Whisker Plot

Figure 3-3
Example Wilk-Shapiro/Rankit Plot

Figure 3-4
Example Scatter Plot: MBTU vs. HDD

Figure 3-5
Example Scatter Plot: MBTU vs. CDD

Figure 3-6 Example Scatter Plot: MBTU vs. SQFT

$$x = \frac{\sum_{i=1}^{n} x_i}{n}$$

The sample mean is used to approximate the population mean, given by μ .

Another statistic similar to the sample mean is the sample median. For the same sample as the above example, the median is obtained by ordering the observations from smallest to largest. The median is given by either the single middle value if n is odd, or the average of the two middle values if n is even. The mean and median can be used in conjunction with each other to determine whether the sample data is skewed. For example, if the mean is less than the median, this would indicate a negative skew. Likewise, if the mean is greater, a positive skew would be indicated. For a sample drawn from a symmetric population, the two values would be expected to be approximately equal.

For the same sample of size n, the sample variance, or S^2 , is calculated as:

$$S^2 = \sum_{i=1}^{n} \frac{(x_i - x)^2}{n}$$

This statistic describes the variability of the sample data. When S^2 is small, this indicates that most of the observations have values relatively close to the sample mean, while a larger value indicates that the observations have more variability or spread.

Table 3-1 shows an output of descriptive statistics from <u>Statistix 4.1</u>. Note that this program shows SD rather than S^2 . SD is the standard deviation, which is simply the square root of the sample variance.

Table 3-1

STATISTIX 4 11:04	.1			CH3DATA, 09/13/95,	
DESCRIPTIVE	STATISTICS				
	MBTU	CDD	HDD	SQFT	
N	79	79	79	79	
MEAN	0.0156	90.380	464.54	3843.5	
SD	7.756E-03	148.40	492.89	1060.1	
MINIMUM	4.400E-03	0.0000	0.0000	2315.0	
MEDIAN	0.0138	7.0000	284.00	3719.0	
MAXIMUM	0.0324	537.00	2198.0	5898.0	

Correlation

Correlation provides a method for measuring the strength of a linear relation between two variables. Correlation is a powerful tool. First, it is not affected by a change in units of measurement, provided the conversion from one unit to another is linear (Devore, 1991). Also, it allows comparison of the strength of the linear relation of one pair of variables to another pair (Weck, 1981). If, as is the case for this thesis, more than two variables are to be considered, correlation analysis must be performed on a pairwise basis.

The quantity used to measure the strength of each pair's linear relationship is the Pearson correlation coefficient, or ρ . The maximum value of ρ is +1.0, and this value indicates the strongest possible positive linear relationship between the two variables of concern. Likewise, its minimum value is -1.0, and this value indicates the strongest possible negative linear relationship. If there is no linear relationship between the two variables, then r will be zero. For purposes of this thesis, the relationship will be described as "strong" if $|\rho| \ge 0.8$, "moderate" if $0.5 \le |\rho| < 0.8$, and "weak" if $|\rho| < 0.5$. If $\rho = 0$, the two variables are said to be uncorrelated. It is important to note that when the two variables are independent, ρ will always equal zero. However, the fact

that $\rho=0$ does not imply independence. It simply means that a linear relationship between the two variables does not exist. Two uncorrelated variables could still be dependent, but through a nonlinear relationship. If $\rho=0$, the two variables are said to be uncorrelated (Devore, 1991).

The fact that two variables are strongly or moderately correlated does not imply any causal relationship between them. The high degree of correlation means only that the high or low values tend to be associated with corresponding high or low values (Devore, 1991). Investigation and knowledge of the activity which the two variables represent must precede any implications as to a causal relationship between them.

For each pair of variables for which a value of ρ was determined, the null hypothesis was that the two variables were uncorrelated. Statistix 4.1 reported both a correlation coefficient and the significance level for that coefficient. If the significance level was less that 0.05, then the null hypothesis was rejected, and the two variables were determined to have either a strong, moderate, or weak linear relationship as appropriate. So, in summary:

$$H_0$$
: $\rho = 0$

$$H_A$$
: $\rho \neq 0$.

The test statistic used for the correlation analysis of the candidate independent variables is the P-value. A P-value is "the smallest level of significance at which H₀ would be rejected when a specified test procedure is used on a given data set" (Devore, 1991). Statistix 4.1 simplifies the use of P-values in correlation analysis by presenting a P-value along with the correlation coefficient in the correlation matrix.

Table 3-2 shows a correlation matrix created by <u>Statistix 4.1</u>. Note that the results of the correlation analysis complement the qualitative analysis performed by means of scatter plots. The

correlation coefficients computed are all statistically significant except for that between CDD and HDD, since all but that one are less than α . Note also that the dependent variable is strongly correlated with HDD and SQFT, while it is weakly correlated with CDD. Note also that CDD and HDD are moderately correlated with SQFT, although there is no reason to suspect that there is a causal relationship between them.

Table 3-2
Example Correlation Matrix

STATISTIX 13:00	4.1			CH3DATA,	09/13/95,		
CORRELATIONS (PEARSON) ZERO INTERCEPT OPTION SELECTED: CORRELATIONS = COSINES							
HDD P-VALUE	CDD 0.0174 0.8793	HDD	SQFT				
SQFT	0.4924 0.0000	0.6608					
MBTU	0.2602 0.0205	0.9046 0.0000	0.8665				
CASES INCLUDED 79 MISSING CASES 0							

Analysis of Variance(Devore, 1991)

Analysis of Variance (ANOVA) is the name for a set of statistical procedures and analysis techniques used to examine data gathered from two or more populations. The different populations are identified by the differences in the factor under consideration. The goal of ANOVA is to determine whether the means of the various populations differ to a significant extent. Consider the case of a data set consisting of I treatments. (Note: ANOVA is easier performed if each treatment consists of the same number of observations. However, it is not necessary and that assumption will not be made in this case. The formulas used to compute these

statistics are somewhat more complex than the case where the sample sizes for the various treatments are equal). The null hypothesis in this case is that the means are all equal, and the alternate hypothesis is that at least one mean is not equal to the others, or:

$$H_0$$
: $\mu_1 = \mu_2 = ... = \mu_i$

$$H_A$$
: at least one $\mu_a \neq \mu_b$

In order to examine the validity of the null and alternate, several quantities are used to examine the i sample means. These three quantities are known generally as the sums of squares, and consist of the total sum of squares (SST), the treatment sum of squares (SSTr), and the error sum of squares (SSE). For a data set of I treatments, each of which consists of J_i observations, and with the total number of observations given by

 $n = \Sigma_i J_i$, their formulas are given by:

SST=
$$\sum_{i=1}^{I} \left[\sum_{j=1}^{J_i} X_{ij}^2 - \frac{1}{n} X_{..}^2 \right]$$

$$SSTr = \left[\sum_{i=1}^{I} \frac{1}{J_i} \cdot X_{i}^2 - \frac{1}{n} \cdot X_{i}^2 \right]$$

These are used to calculate the Mean Square for Treatments (MSTr) and the Mean Square for Error (MSE). These statistics measure respectively the variation among the i sample means, and the variation over all I samples regardless of treatment. When the null hypothesis is true, the values of MSTr and MSE should be similar, so the ratio of MSTr to MSE should be close to one. However, when the alternate hypothesis is true, MSTr should greatly exceed MSE, resulting in a ratio much greater than one. Thus, the test statistic for ANOVA is given by:

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$$f = \frac{MSTr}{MSE}$$

The value of this statistic is compared with the F distribution, and the null hypothesis is rejected if

 $f \ge F_{\alpha,I-1,n-1}$

where α is the desired level of significance for the test.

ANOVA was used extensively in this thesis to evaluate the various categorical variables which were considered. Each categorical variable was used as a factor, and ANOVA was performed on the entire data set to determine how to group the observations for MLR modeling.

This technique requires that the user make two assumptions: First, that all of the treatment distributions are normally distributed, and second, that their variances are equal, $or\sigma_1^2 = \sigma_2^2 = ... = \sigma_i^2$. Supplemental tests were performed on the data in order to verify the validity of the first assumption, but research found that performing tests to ensure the validity of the second were not recommended (Devore, 1991).

Comparisons between multiple treatments in this thesis used Tukey's procedure. This procedure uses a probability distribution called the Studentized Range distribution to obtain confidence intervals for comparison of means between two populations I and J. It is given by:

$$X_{i.} - X_{j.} - Q_{\alpha,I,I(J-1)} \sqrt{MSE \, / \, J} \leq \mu_i - \mu_j \leq X_{i.} - X_{j.} + Q_{\alpha,I,I(J-1)} \sqrt{MSE \, / \, J}$$

This procedure is used to group the data into groups whose confidence intervals do not "overlap". These will be considered to be significantly different at the level of significance α which has been specified (Devore, 1991). Table 3-3 shows the <u>Statistix 4.1</u> output for a one way ANOVA

analysis, with the seven bases used as the treatments, and Table 3-4 shows the output from a Tukey procedure.

The ANOVA output clearly shows that the null hypothesis, that all μ 's are equal, should be rejected. As with the correlation matrix, <u>Statistix 4.1</u> calculates a P-value for this procedure, which can be used to interpret the statistical significance. In this case, P is less than 0.05, so the results are statistically significant for the α specified in this thesis.

The Tukey procedure determined that there were three groups whose means were significantly different at $\alpha = 0.05$. Bases 5 and 6 are in the first group, base 1 is in the second, and bases 3 and 4 are in the third. The group to which bases 2 and 7 belonged could not be determined, as they overlapped more than one group.

Development of Model

Overview. In order to satisfy the second research objective stated in chapter I, which was to construct a model to predict energy consumption at an Air Force base, this thesis will concentrate on the use of multiple linear regression (MLR). Other research efforts have found this to be the most appropriate method for forecasting energy consumption (Weck, 1981; Tinsley, 1981; and Morill, 1985).

This section will present a brief description of the MLR technique, a definition of the test statistic used to determine the predictive ability of the model, and will list the assumptions which were made in using this technique.

<u>Description of Technique</u>

A regression model is a means of expressing a statistical relationship in which the following two conditions are present (Neter et al, 1983):

- 1. A tendency of the dependent variable Y to vary with the independent variable or variables in a systematic fashion.
- 2. A scattering of observations around the curve of statistical relationship.

Multiple linear regression, then, is "a statistical method relating the value of a dependent variable to the influence of two or more independent variables, all acting at some time" (Tinsley, 1981).

A simple linear regression model is expressed as an equation which describes a straight line which may or may not pass through the origin. As variables are added, the equation describes a plane, and then a hyperplane. In the case where n independent variables are used, the equation would describe a hyperplane in n + 1 dimensions, and would be given as:

$$Y_i = \beta_0 + \beta_1 X_{1i} + \beta_2 X_{2i} + ... + \beta_n X_{ni} + \epsilon_i$$

Where:

Y_i is the response (dependent) variable for the ith trial

 β_0 , β_1 , β_2 , ... β_n are parameters

 $X_{1i}, X_{2i}, ..., X_{ni}$ are the values of the independent variables for the ith trial

 ε_i is a random error term with expected value of zero (Neter et al, 1983).

(The fact that an equation with a large number of independent variables describes an object which is difficult to visualize is not important).

Table 3-3 Example Analysis of Variance

STATISTIX 13:40	4.1				CH3DATA,	09/13/95,	
ONE-WAY AC	OV FOR MBTU BY	BASE					
SOURCE	DF SS	MS	F	P			
WITHIN	6 0.0017 72 0.0029 78 0.0046	0 4.025E-05	7.43	0.0000			
EQUAL V COCHRAN'S LARGEST VA COMPONENT	CHI-SQ DF P BARTLETT'S TEST OF EQUAL VARIANCES 28.48 6 0.0001 COCHRAN'S Q 0.2756 LARGEST VAR / SMALLEST VAR 50.922 COMPONENT OF VARIANCE FOR BETWEEN GROUPS 2.297E-05 EFFECTIVE CELL SIZE 11.3 SAMPLE GROUP						
BASE	MEAN	SIZE ST	D DEV				
1 2 3 4 5 6 7 TOTAL	0.0100 0.0166 0.0146 0.0215 0.0220 8.692E-03	12 8.83 12 5.11 10 6.72 12 6.88 12 6.56 9 6.44 12 1.23 79 6.34	6E-03 8E-03 4E-03 5E-03 9E-03				

Table 3-4
Tukey Comparison of Means

STATISTIX 4.1 CH3DATA, 09/13/95, 13:40

TUKEY (HSD) PAIRWISE COMPARISONS OF MEANS OF MBTU BY BASE

BASE	MEAN	HOMOGENEOUS GROUPS			
6	0.0220	I			
5	0.0215	I			
1	0.0173	ΙΙ			
3	0.0166	ΙΙΙ			
4	0.0146	ΙΙΙ			
2	0.0100	I I			
7	8.692E-03	I			

THERE ARE 3 GROUPS IN WHICH THE MEANS ARE NOT SIGNIFICANTLY DIFFERENT FROM ONE ANOTHER.

CRITICAL Q VALUE 4.289 REJECTION LEVEL 0.050 STANDARD ERRORS AND CRITICAL VALUES OF DIFFERENCES VARY BETWEEN COMPARISONS BECAUSE OF UNEQUAL SAMPLE SIZES.

The goal of the analysis described in the previous section was to determine which of the candidate independent variables would be included in the model. Once that was done, the goal of the subsequent model development was to determine the values of the model parameters, and to assess the model's predictive ability.

Many of the statistics which were described in the ANOVA section will also be used to determine values for the parameters. SST and SSE are calculated for the model by the same techniques used in ANOVA. An additional statistic is used to account for the difference between these two sums of squares, the regression sum of squares, or SSR. this quantity is given by the formula:

$$SSR = \Sigma \left(Y_i - Y \right)^2$$

where each Y_i is a value of the dependent variable predicted by the model, and Y is the mean of these predictions. SSR measures the variation of the predictions from the mean, while SSE measures the variation of the predictions from the regression line (for the case of one independent variable) or the regression plane (for more than one independent variable). When constructing a model, the goal is to define the regression line (or plane) such that all of the points fall as close to it as possible. If the fit were perfect, SSE would equal zero. The primary tool for measuring a model's effectiveness is the coefficient of determination, r^2 . It is given by the formula:

$$r^2 = 1 - SSE/SSTO$$
,

with $0 \le r^2 \le 1$. Large values of r^2 indicate a good fit, while small ones indicate a poor one. This statistic was used extensively in this thesis to quickly evaluate the various models which were constructed.

Test Statistic

The test statistic used to accept or reject regression models for this thesis was the F statistic. The value of F for a given model is calculated using some of the statistics described above. Also, the number of observations upon which the model is based, n, is used. First, the regression mean square, MSR, and the mean square for error, MSE are calculated:

$$MSR = \frac{S}{MSR} = \frac{SSR}{1} = SSR$$

$$MSE = \frac{S}{n} = \frac{SSE}{n-2}$$

The value of the test statistic was then calculated for each model by:

f = MSR/MSE

and the value compared with the value of the F statistic, and the model is accepted if:

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Assumptions

This section describes assumptions which were made specific to the application of the linear regression model to the data set. Each assumption is listed along with methods used to verify its validity.

The first assumption that will be made is that the activity to which the regression model is being fit is linear. The linear regression model will not be appropriate if the independent variable(s) and the dependent variable are not linearly related. As stated earlier, previous research has indicated that this model is indeed appropriate for modeling energy consumption. The validity of this assumption will be verified qualitatively by means of scatter plots, and quantitatively by means of the correlation coefficients.

Another assumption is that the error terms in the regression model, ϵ_i , have constant variance. When this condition is true, it is said that the observations are homoscedastic, while in the case of unequal variances they are said to be heteroscedastic. Residual plots will be used to verify that the data is homoscedastic, or nearly so.

A related assumption is that the error terms are normally distributed. Small departures from normality will not greatly affect the application of the linear regression model. However, large departures will render the model useless. The primary means for verifying the normality will be by means of Wilk-Shapiro plots of the residuals. This test will be used subjectively in conjunction with the other information to determine aptness of the model (Neter et al, 1983).

Example

An example of the type of regression analysis performed in chapter IV is given below for the data subset used previously in this chapter. Table 3-5 shows the output from a <u>Statistix 4.1</u> regression model. In this case, HDD, CDD, and SQFT were chosen as the independent variables based on the results of the correlation analysis performed earlier in this chapter.

The column labeled "COEFFICIENT" represents the values for $\beta 0$, $\beta 1$, ... βn . As with the other <u>Statistix 4.1</u> products, this table provides a P-value for each of these coefficients. The R-squared value of 0.8045 is closer to one than to zero, which indicates that the regression model is probably appropriate in this case.

Statistix 4.1 provides a valuable tool for checking the validity of the assumption that the error functions are normally distributed. This is a Wilk-Shapiro/Rankit plot of standardized residuals, shown at Figure 3-7. This plot, and the accompany statistic, are interpreted in the same way as earlier in this chapter. Note that the high value (0.9564) for the Wilk-Shapiro statistic indicates that the assumption that the error functions are normally distributed was probably valid.

Table 3-5 Example Regression Analysis

STATISTIX 4.1 14:09	1					CH3D.	ATA,	09/13/95,
UNWEIGHTED L	EAST SÇ	QUARES LIN	IEAR	REGRESSIC	ON OF MBTU			
PREDICTOR VARIABLES	COEFF	ICIENT	STD	ERROR	STUDENT'S	Т	P	VIF
CONSTANT HDD CDD SQFT	1.340 -4.033)E-05 3E-06	9.65 3.21	8E-07 2E-06	13.88	0. 0.	2132	1.4 1.4
R-SQUARED ADJUSTED R-SQ								
SOURCE	DF	SS		MS	F	P		
REGRESSION RESIDUAL TOTAL	75		ł			0.0000		
CASES INCLUDED 79 MISSING CASES 0								

Figure 3-7
Example Plot of Standardized Residuals versus Fitted Values

Figure 3-8 Example Wilk-Shapiro/Rankit Plot of Standardized Residuals

IV. Results

Introduction

This chapter will present the results of the statistical procedures described in the previous chapter on the data collected for this thesis. First, the results obtained for the entire data set will be presented and discussed. Next, ANOVA will be used to examine prospective ways of dividing the data set into smaller groups for regression modeling. The same statistical procedures will be performed on these groups, and the results compared with those obtained earlier for the entire data set. Finally, the additional data obtained for selected ACC bases will be added to see if an improved model results.

Analysis of Entire Data Set

The first step in the analysis of data for this thesis was to evaluate the set of data for all CONUS bases, select prospective independent variables, assess the data's aptness for the linear regression model, and construct a linear regression model for energy consumption. The data set initially consisted of 3,936 observations for each variable. Some observations were obviously erroneous. Some, for example had values of zero for both CDD and HDD. This would indicate that the mean daily temperature was 65 degrees Fahrenheit every day of that month. Other observations had a value of zero for MBTU, which would indicate that no energy was consumed by the installation during that month. If either of these two conditions were met, the observation was discarded. Also discarded were observations from the following MAJCOMs because each only controls one base: U.S. Air Force Academy, Air Force District of Washington, and Special Operations Command.

The histogram of MBTU, Figure 4-1, shows a marked skew right, with many apparent outliers. Figure 4-2, the box and whiskers plot, confirms this impression. A Wilk-Shapiro/Rankit plot (Figure 4-3) was then performed to evaluate the normality of the MBTU data. The value of the Wilk-Shapiro statistic, 0.5629, indicates that the data are not normally distributed.

Scatter plots were constructed (Figures 4-4 and 4-5) of MBTU versus HDD and CDD. Both of these seem to display some degree of linear tendency, although the graph of CDD versus MBTU appears to have more of a constant slope. both graphs appear to have a large number of outliers above the apparent regression line. Also, there are a number of points which have a high positive value for MBTU while the independent variable is equal to zero. These values occur during the seasons of most severe temperatures, summer and winter. Energy consumption during these seasons tends to be the highest due to heating and cooling loads. However, during the season (winter) when HDD is expected to have its highest values, CDD can be expected to have its lowest, and vice versa. These values would make the fitting of a regression model more difficult, since the value of the dependent variable would vary widely at a constant value of the independent variable. In order to try to mitigate this effect, a new variable, CHDD, was created where, for each monthly observation:

$$CHDD = CDD + HDD.$$

This new variable was intended to eliminate the cases where CDD or HDD is zero during the extreme temperature seasons by constructing a variable which would treat high or low temperatures generically as they deviated from the 65 degree daily mean. The scatter plot of CHDD versus MBTU is shown at Figure 4-6. Although there still appear to be a great number

Figure 4-1 Histogram of MBTU (Entire Data Set)

Figure 4-3 Wilk-Shapiro/Rankit Plot of MBTU (Entire Data Set)

Figure 4-4 Scatter Plot of MBTU vs HDD (Entire Data Set)

Figure 4-6 Scatter Plot of MBTU vs. CHDD (Entire Data Set) of outliers above the apparent regression line, this graph shows the most prominent appearance of linear behavior of the three temperature-related variables.

A scatter plot was also constructed of SQFT versus MBTU (Figure 4-7). This plot does not show an easily visible linear relationship since the value of SQFT remains constant for each base over each of the four fiscal years. Thus, for each discrete value of SQFT there will be twelve different values of MBTU. The graph does not show any obvious evidence of linear behavior.

The next step in assessing the potential for each of these variables is to perform a correlation analysis. Although as mentioned above, some of the variables showed more promise than others, all were included in this analysis. (The variables AGE and MAINT were not included because this data was obtained for only a small number of bases. They are discussed in the section entitled "ACC bases with Supplemental Data"). The results are given in Table 4-1. The table shows that all of the independent values were positively correlated with MBTU; the strongest correlation was with CHDD, followed by HDD, SQFT, and CDD. All of these were moderately correlated with MBTU, with the exception of CDD which was weakly correlated. The P-values shown for these correlation coefficients (all were less than 0.0001) show that these results are statistically significant at $\alpha = 0.05$.

The next step will be to attempt to incorporate the moderately correlated variables in a linear regression model. The following variables will be included: CHDD and SQFT. HDD is also moderately correlated with MBTU; however, it has a high degree of correlation with CHDD, and therefore should not be included. CDD will be omitted because it is only weakly correlated with MBTU. The results of the regression analysis using these variables is shown in Table 4-2.

Table 4-1 Correlation Matrix (Entire Data Set)

STATISTIX	4.1				, 09/18	/95,	9:01		
CORRELATIONS (PEARSON) ZERO INTERCEPT OPTION SELECTED: CORRELATIONS = COSINES									
CDD P-VALUE	HDD 0.0223 0.1955	CDD	CHDD	SQFT					
CHDD	0.8998 0.0000	0.4563 0.0000							
SQFT	0.5094 0.0000	0.4763 0.0000	0.6612 0.0000						
MBTU	0.6780 0.0000	0.3496 0.0000	0.7561 0.0000	0.5765 0.0000					
CASES INCL	UDED 3365	MISSING	CASES 0						

The P-values returned by <u>Statistix 4.1</u> show that these coefficients are statistically significant at $\alpha = 0.05$.

The R² value obtained by using CHDD and SQFT as the independent variables in a regression model was 0.1265, which does not indicate a good fit. Although the P-values indicate that the results of this analysis are statistically significant, this model could not be used to predict energy consumption. One interesting note is that the coefficient for SQFT is negative, which would indicate that larger installations generally use less energy per square foot than smaller ones.

In order to determine whether the linear regression model was appropriate, several tests were run on this regression model in order to check for aptness. Recalling the assumptions necessary for the use of the regression model (listed in chapter III), the first test that was

Table 4-2 Regression Analysis Table (Entire Data Set)

STATISTIX 4	.1				,	09/18/95,	13:40
UNWEIGHTED :	LEAST SQ	UARES LIN	IEAR REGRESSIC	ON OF MBTU			
PREDICTOR VARIABLES	COEFFI	CIENT	STD ERROR	STUDENT'S	T P	VIF	
CHDD	1.530	E-05	4.919E-04 7.197E-07 6.689E-08	21.26	0.000	00 00 1.0 00 1.0	
~			RESIDUAL STANDARD				
SOURCE	DF	SS	MS	F	P		
REGRESSION RESIDUAL TOTAL			0.03659 0.1535E-04		0.0000		
CASES INCLU	DED 3295	MISSIN	IG CASES 0				

performed was the plot of standardized residuals versus fitted values. If regression analysis is appropriate, all of the values should fall in a symmetrical band above and below zero. In this case (Figure 4-8), the graphical presentation seems to show that the error terms, ε_i , were equal.

Another test, the Wilk-Shapiro/Rankit plot, was performed to determine whether the error terms ϵ_i were normally distributed. The results of this test are given in Figure 4-9. The Wilk-Shapiro statistic value of 0.4856 indicates strongly that the error terms are not normally distributed.

So, constructing a model using the results of the entire data set is not practical because the data do not meet the assumptions necessary to apply the linear regression model. The next step performed in this thesis was to use ANOVA analysis to evaluate prospective means of dividing the data into subgroups. The first categorical variable to be evaluated was CMD, which represents the MAJCOM controlling each base. The results of this ANOVA are shown in Table 4-3. Table 4-4 shows the results of a Tukey test to determine

whether any of the Major Commands exhibit similar means for energy consumption. The results show that two commands, AFMC and SPC, had means significantly higher than the others. AMC and AETC were lower, but their means were significantly different from each other. ACC's mean was not significantly different from either AMC or AETC. However, this test shows that grouping the data by Major Command would be a statistically valid technique Flying versus non-flying bases were also evaluated using the ANOVA technique. The results of this analysis are shown in Tables 4-5 and 4-6. These tables show that the means of flying bases are significantly different from those of nonflying bases.

Another categorical variable which was evaluated for possible use in grouping the bases was DEPOT, which reflected whether a base supported a depot used for overhaul of aircraft or missile systems. The results of this analysis are given in Table 4-7. Since the P-value is greater than 0.05, there was no significant difference between the means of the two groups, so this variable was discarded as a possible grouping variable.

Table 4-8 shows the ANOVA results for the final categorical variable, FY. There is no significant difference between the mean values of MBTU for each fiscal year. In fact, the mean actually increased each year from FY 91 to FY 94.

Table 4-3 ANOVA (MBTU by Major Command)

STATISTIX	4.1				, 09/18/95	5, 13:42			
ONE-WAY A	OV FOR MBTU	BY CMD							
SOURCE	DF SS	MS	S F	Р					
WITHIN 3	4 0.04 290 0.53 294 0.57	550 1.628E		01 0.0000					
CHI-SQ DF P BARTLETT'S TEST OF EQUAL VARIANCES 1813.92 4 0.0000									
	Q AR / SMALLES		.5220 .2.141						
	OF VARIANCE CELL SIZE	FOR BETWEE	N GROUPS	1.652E-05 640.7					
CMD	MEAN		GROUP STD DEV						
AETC AFMC AMC SPC	0.0129 0.0122 0.0215 0.0144 0.0197	799 617 624 298	7.452E-03 0.0227 8.027E-03 0.0176	_					
CASES INC	LUDED 3295	MISSING C	CASES 0						

Table 4-4
Tukey Comparison of Means (MBTU by Major Command)

STATISTIX 4	1.1		,	09/18/95,	13:42			
TUKEY (HSD)	PAIRWISE	COMPARISONS OF MEANS OF MBTU BY CMD						
		HOMOGENEOUS						
CMD	MEAN	GROUPS						
AFMC	0.0215	I						
SPC	0.0197	I						
AMC	0.0144	I						
ACC	0.0129	I I						
AETC	0.0122	I						
THERE ARE 3	GROUPS IN	WHICH THE MEANS ARE						
NOT SIGNIFI	NOT SIGNIFICANTLY DIFFERENT FROM ONE ANOTHER.							
CRITICAL Q VALUE 3.857 REJECTION LEVEL 0.050								
STANDARD ER	RRORS AND C	RITICAL VALUES OF DIFFERENCES						

Table 4-5 ANOVA Table (MBTU by Flying/Nonflying Mission)

STATISTIX 4.1					,	09/18/95,	14:05	
ONE-WAY AOV FO	R MBTU BY FLY	7						
SOURCE DF	SS	MS	F	P				
BETWEEN 1 WITHIN 3293 TOTAL 3294	0.55203 1		157.78	0.0000				
CHI-SQ DF P BARTLETT'S TEST OF EQUAL VARIANCES 1635.35 1 0.0000								
COCHRAN'S Q LARGEST VAR /		0.885 7.761						
COMPONENT OF V.		BETWEEN GF	ROUPS 1.	760E-05 1493.6				
FLY	SAM MEAN SI	MPLE G						
	0.0191 114							
Y TOTAL	0.0132 215 0.0152 329							
CASES INCLUDED	3295 MISS	SING CASES	S 0					

Table 4-6
Tukey Comparison of Means (MBTU by Flying/Nonflying Mission)

STATISTIX	X 4.1		, (09/18/95,	14:04				
TUKEY (HS	SD) PAIRWISE	COMPARISONS OF MEANS OF MBTU BY FLY							
FLY	MEAN	HOMOGENEOUS GROUPS							
N Y	0.0191 0.0132								
ALL 2 MEA	ALL 2 MEANS ARE SIGNIFICANTLY DIFFERENT FROM ONE ANOTHER.								
STANDARD	ERRORS AND (2 REJECTION LEVEL 0.050 RITICAL VALUES OF DIFFERENCES SONS BECAUSE OF UNEQUAL SAMPLE SIZES.							

Table 4-7 ANOVA Table (MBTU by Presence of Depot)

STATISTIX 4	.1				, 09/18/95,	14:14
ONE-WAY AOV	FOR MBTU BY	DEPOT				
SOURCE D	F SS	MS	F	Р		
WITHIN 329		5 5.055E-05 3 1.757E-04 8		0.5917		
	TEST OF	-SQ DF .83 1				
		0.59 VAR 1.48				
COMPONENT OF		OR BETWEEN G	ROUPS -3.	.086E-07 405.4		
DEPOT	MEAN	SAMPLE SIZE S				
Y	0.0148	3078 217 3295	0.0159			
CASES INCLU	DED 3295	MISSING CASE	s 0			

Table 4-8 ANOVA Table (MBTU by Fiscal Year)

STATISTIX 9:32	4.1				, 09/28/95,
ONE-WAY AO'	V FOR MBTU BY F	Y			
SOURCE 1	DF SS	MS	F	Р	
WITHIN 32	3 8.791E-04 91 0.57760 94 0.57848		1.67	0.1695	
		Q DF	P		
	TEST OF ARIANCES 312.4		0.0000		
	Q R / SMALLEST VA				
COMPONENT (OF VARIANCE FOR CELL SIZE	BETWEEN GR	OUPS 1.	428E-07 823.3	
FY	S. MEAN	AMPLE G			
	0.0146				
	0.0149				
93	0.0155	820 0	0.0129		
94 TOTAL	0.0159 0.0152 3				
CASES INCL	UDED 3295 MI	SSING CASES	3 0		

Analysis of Bases by Major Command

The following results were obtained by dividing the sample into the three groups mentioned above. Since ACC could be grouped with either AMC or AETC, both of these groupings will be tried; each of these three commands will also be examined alone.

SPC and AFMC. The graphical analysis of the data for these commands is contained in Appendix D. Both the histogram and the box and whiskers graph show the presence of a large number of outliers. The Wilk-Shapiro statistic's value of 0.5668 suggests that the data is not normally distributed. The three scatter plots of MBTU versus CDD, HDD, and CHDD all show

evidence of a linear trend among most of the observations; however, there seem to me a fairly significant number of points for which a relatively high value of MBTU was observed at a relatively low value of the independent variable. The scatter plot of MBTU versus SQFT shows no clearly discernible linear trend.

Table 4-9 shows the results of the correlation analysis of the data for the AFMC and SPC bases. HDD and CHDD are moderately correlated with MBTU; CDD and SQFT are weakly correlated. All of these correlation coefficients are statistically significant at $\alpha = 0.05$. CHDD and SQFT were then used to construct a linear regression model; the results are given in Table 4-10. This model has an even lower R^2 , 0.0959, than the one constructed for all CONUS bases, and would probably not be useful for predicting energy consumption. Figure D-9 is the plot

Table 4-9 Correlation Matrix (AFMC and SPC Bases)

STAT 9:40	ISTIX 4.1				,	09/20/95,				
	MC /DENDCO	NT \								
	CORRELATIONS (PEARSON) ZERO INTERCEPT OPTION SELECTED: CORRELATIONS = COSINES									
CDD P-VALUE	HDD 0.0229 0.4889	CDD	CHDD	SQFT						
CHDD	0.9035 0.0000	0.4491 0.0000								
SQFT	0.4893 0.0000	0.4985 0.0000	0.6510 0.0000							
MBTU	0.5881 0.0000	0.3482 0.0000	0.6749 0.0000	0.4544 0.0000						
CASES INCL	UDED 915	MISSING C	ASES 0							

Table 4-10 Regression Analysis Table (AFMC and SPC Bases)

STATISTIX 4.3	STATISTIX 4.1 , 09/20/95, 9:49									
UNWEIGHTED LEAST SQUARES LINEAR REGRESSION OF MBTU										
PREDICTOR VARIABLES	COEFFI	CIENT	STD ERROR	STUDENT'S	T P	VIF				
CHDD	1.603	E-05	0.00152 2.390E-06 1.345E-07	6.71	0.000	0 1.0				
~			RESIDUAL STANDARD	~						
SOURCE	DF	SS	MS	F	P					
RESIDUAL			0.01971 4.075E-04		0.0000					
CASES INCLUD	ED 915	MISSING	CASES 0							

of standardized residuals versus fitted values for this regression model, and Figure D-9 is the Wilk-Shapiro/Rankit plot. These plots show that this data may not have met the basic assumptions of the linear regression model. The plot of standardized residuals (Figure D-8) versus fitted values shows that the data appear to be heteroscedastic, and the Wilk-Shapiro/Rankit plot and statistic (Figure D-9) suggest that the error terms are strongly nonnormal. As stated in the previous chapter, any large departure from the normal distribution makes the use of the linear regression model inappropriate.

The poor results obtained in this linear regression model may be related to the extremely diverse physical plants found in AFMC and SPC. Tables 4-11 and 4-12 show the results of an ANOVA analysis and a Tukey analysis which was performed on the data for all of the CONUS bases. The dependent variable in each case was SQFT, and the analysis shows that AFMC has the highest mean of the MAJCOMs, and SPC had the lowest.

Table 4-11 ANOVA Table (Facility Floor Area by Major Command)

STATIS	TIX 4.1						, 0	9/25/95,
	Y AOV FO	R SOFT BY	CMD					
SOURCE	DF	SS	M	IS	F	P		
WITHIN	3290 3294	2.326E+3			91.97	0.0000		
		CH	I-SQ I	F	P			
	TT'S TES' AL VARIA	-		4 0.	0000			
COCHRA	N'S Q T VAR / :		VAR					
	ENT OF V	_	FOR BETWE	EN GROU	PS 4.	314E+06 640.7		
		5111	SAMPLE	GRO	UP	0 2 0 1 7		
CMD)	MEAN	SIZE	STD	DEV			
ACC		3370.0	957	106	4.2			
AFMC			617		8.8			
AMC			624		9.8			
SPC		2793.0	298	160	0.7			
TOTAL		4322.0	3295	265	8.8			
CASES	INCLUDED	3295	MISSING	CASES 0				

Table 4-12
Tukey Comparison of Means (Facility Floor Area by Major Command)

STATISTIX 4	.1		, 09/25/95,
	PAIRWISE	COMPARISONS OF MEANS OF SQFT BY CMD	
CMD	MEAN	HOMOGENEOUS GROUPS	
AFMC	8098.9	I	
AMC	3887.6	I	
AETC	3455.2	I	
ACC	3370.0	I	
SPC	2793.0	I	
NOT SIGNIFIC	CANTLY DIF	WHICH THE MEANS ARE FERENT FROM ONE ANOTHER. 7 REJECTION LEVEL 0.050 RITICAL VALUES OF DIFFERENCES	
VARY BETWEED	N COMPARIS	ONS BECAUSE OF UNEQUAL SAMPLE SIZES.	

AMC and ACC. Both the histogram and the box and whiskers plot (Figures E-1 and E-2) show that there are fewer outliers when the bases in these two MAJCOMs are grouped. The histogram shows a slight right skew, but the Wilk-Shapiro/Rankit plot (Figure E-3) show the data to be close to normally distributed.

The scatter plots of MBTU versus HDD, CDD, and CHDD (Figures E-4, E-5, and E-6) seem to indicate linear behavior much more clearly than the previous groupings, while the plot of MBTU versus SQFT (E-7) is again difficult to interpret visually.

Table 4-13 shows the results of the correlation analysis performed on this data. HDD, CHDD, and SQFT are all strongly correlated with MBTU, and that CDD is moderately correlated. The P-values supplied by Statistix 4.1 show that the results of the correlation analysis are statistically significant at $\alpha = 0.05$. Based on the results of the correlation analysis, as well as the appearance of the scatter plots, a linear regression model for this group of

Table 4-13
Correlation Matrix (AMC and ACC Bases)

STATISTIX	4.1				,	09/20/9	5,	10:09		
CORRELATIONS (PEARSON) ZERO INTERCEPT OPTION SELECTED: CORRELATIONS = COSINES										
CDD P-VALUE	HDD 0.0219 0.3849	CDD	CHDD	SQFT						
CHDD	0.9322 0.0000	0.3822 0.0000								
SQFT	0.6261 0.0000	0.5297 0.0000	0.7704 0.0000							
MBTU	0.8783 0.0000	0.3366 0.0000	0.9337 0.0000	0.8288 0.0000						
CASES INCL	UDED 1581	MISSING (CASES 0							

bases was constructed with the following independent variables: HDD, CHDD, and SQFT. The results of this analysis are shown in Table 4-14. Using the R^2 and F-statistic values as an indicators of goodness of fit shows that using the linear regression model to predict energy consumption for this group of bases is much more feasible than to do so for the group of AFMC and SPC bases. This may be due to the fact that the bases are more similar in size (see Tables 4-11 and 4-12). The P-values show that the coefficients have been determined to be statistically significant at $\alpha = 0.05$. Figure E-8, the plot of standardized residuals versus fitted values, shows that the error terms appear to be homoscedastic, and Figure E-9, the Wilk-Shapiro/Rankit plot of standardized residuals, shows that a normal distribution is plausible.

Table 4-14
Regression Analysis Table (AMC and ACC Bases)

STATISTIX 4	.1				CAHUNA	11/07/95,
15:58						
UNWEIGHTED I	LEAST SQU	JARES LINE	EAR REGRESSIO	ON OF MBTU		
PREDICTOR						
VARIABLES	COEFFI	CIENT S	STD ERROR	STUDENT'S	T P	VIF
CONSTANT	0.00	 0662 3	3.870E-04	17.10	0.000	10
SQFT	-2.9501	E-07 9	9.347E-08	-3.16	0.001	.6 1.0
			3.225E-07			
			RESIDUAL STANDARD			
SOURCE	DF	SS	MS	F	Р	
RESIDUAL	1578		0.02543 1.953E-05		0.0000	
CASES INCLUI	DED 1581	MISSING	G CASES 0			

These tests show that the assumptions of the linear regression model appear to have been met in the case of the group of ACC and AMC.

ACC and AETC. The graphs for this data are contained in Appendix F. The histogram and box and whiskers plot (Figures F-1 and F-2) show the familiar skew right found in previous analyses. The scatter plots of MBTU versus HDD, CDD, and CHDD (Figures F-3, F-4, and F-5) seem to show a linear tendency. However, there are a small number of points located above the main group in all three of these plots. No linear pattern is discernible in the plot of MBTU versus SQFT.

Table 4-15 shows that CHDD is strongly correlated with MBTU; SQFT and HDD are moderately correlated, and CDD is weakly correlated, all of which were significant at $\alpha = 0.05$.

The strongly and moderately correlated variables were included in a linear regression model; the results are shown at Table 4-16. Again, SQFT has a negative coefficient, while the constant and the coefficients for CHDD and HDD were negative. All of these values were significant at $\alpha = 0.05$. The R^2 value for this model is 0.4620, which indicates that the model fit the data rather poorly.

Figures F-8 and F-9, the plot of standardized residuals versus fitted values and the Wilk-Shapiro/Rankit plot of standardized residuals, show that the error terms may have been heteroscedastic, and that the error terms do not strongly resemble a normal distribution. The model constructed by grouping the data for AETC and ACC exhibited neither the goodness of fit nor the model aptness of the previous grouping, even though the installations in these two commands are more similar in size than those in AMC and ACC (See Tables 4-11 and 4-12).

Table 4-15 Correlation Matrix (AETC and ACC Bases)

STATISTIX	4.1				,	09/20/95	10:31			
CORRELATIONS (PEARSON) ZERO INTERCEPT OPTION SELECTED: CORRELATIONS = COSINES										
CDD P-VALUE	HDD 0.0233 0.3281	CDD	CHDD	SQFT						
CHDD	0.8654 0.0000	0.5211 0.0000								
SQFT	0.5632 0.0000	0.5548 0.0000	0.7589 0.0000							
MBTU	0.7858 0.0000	0.4386 0.0000	0.8907 0.0000	0.7459 0.0000						
CASES INCL	UDED 1756	MISSING	CASES 164							

Table 4-16 Regression Analysis Table (AETC and ACC Bases)

STATISTIX 4	.1					CAH	JNA,	11/07/95,
16:08								
UNWEIGHTED :	LEAST SQ	UARES LIN	IEAR	REGRESSIC	ON OF MBTU			
PREDICTOR VARIABLES	COEFFI	CIENT	STD	ERROR	STUDENT'S	Т	P	VIF
CONSTANT	0.0	 0847	3.4	 74E-04	24.39	0.0	0000	
SOFT	-6.987	E-07	7.5	42E-08	-9.26	0.0	0000	1.0
					31.77		0000	
					MEAN SQUARE ERROR OF ES			
SOURCE	DF	SS		MS	F	P		
RESIDUAL	1753		<u> </u>		536.91	0.0000		
CASES INCLU	DED 1756	MISSIN	IG C.	ASES 0				

ACC Only

The graphical presentation of this data is found in Appendix G. The histogram and box and whiskers plots (Figures G-1 and G-2) show the same right skew seen in the other data groups, while the Wilk-Shapiro/Rankit plot (Figure G-3) shows that the data approximate a normal distribution. The scatter plots of MBTU versus HDD and CHDD (Figures G-4 and G-6) show an apparent positive linear relationship, while those for CDD and SQFT (Figures G-5 and G-7) show no easily discernible trend.

Table 4-17 shows the results of the correlation analysis. HDD, CHDD, and SQFT are all strongly correlated, while CDD is weakly correlated. Based on this information, a linear regression model was constructed using the three strongly correlated variables. The results are given in table 4-18. The regression model shows that, as in previous cases, all of the variables except for SQFT had positive coefficients; its coefficient was negative. The P-values show that all of the coefficients obtained were statistically significant at $\alpha = 0.05$. The R² value is the highest obtained thus far.

The plot of standardized residuals versus fitted values (Figure G-8) appears to show homoscedasticity. The Wilk-Shapiro/Rankit plot (Figure G-9) shows that the data approximate a normal distribution. So, it appears that the basic assumptions of the linear regression model have been met for this data set.

Table 4-17 Correlation Matrix (ACC Bases)

STATISTIX	4.1				, (09/20/95,	10:51			
CORRELATIONS (PEARSON) ZERO INTERCEPT OPTION SELECTED: CORRELATIONS = COSINES										
CDD P-VALUE	HDD 0.0218 0.5007	CDD	CHDD	SQFT						
CHDD	0.9134 0.0000	0.4268 0.0000								
SQFT	0.6319 0.0000	0.5595 0.0000	0.7994 0.0000							
MBTU	0.8688 0.0000	0.3731 0.0000	0.9378 0.0000	0.8602 0.0000						
CASES INCL	UDED 957	MISSING C	ASES 0							

Table 4-18 Regression Analysis Table (ACC Bases)

STATISTIX 4.	1				,	09/25/95,	10:50
UNWEIGHTED L	EAST SQ	UARES LIN	EAR REGRESSIO	ON OF MBTU			
PREDICTOR	go====	G =	C== =====				
VARIABLES	COELLT	CIENI.	STD ERROR	STUDENT'S	I. P	VIF	
CONSTANT	0.0	0823	3.775E-04	21.81	0.000	00	
			6.609E-07			00 4.7	
HDD	1.159	E-05	5.447E-07	21.27	0.000	00 4.7	
SQFT	-2.088	E-07	9.835E-08	-2.12	0.034	1.0	
			RESIDUAL STANDARD				
SOURCE	DF	SS	MS	F	P		
REGRESSION	3	0.03082	0.01027	7 994.64	0.0000		
RESIDUAL	953	0.00984	1.033E-05	5			
TOTAL	956	0.04067					
CASES INCLUD	ED 957	MISSING	CASES 0				

ACC With Supplemental Data. As described in the previous chapter, a WIMS report was used to collect additional data from bases in ACC. This report was sent by electronic mail to all ACC bases; unfortunately only ten responses were received. One of the responses was found to be erroneous in the area of maintenance facility area; the quantity generated by the report exceeded the total facility floor area reported annually to AFCESA. The data for the base in question was therefore discarded. The data for the nine bases which was used in this section is located at Appendix B.

The histogram of data (Figure H-1) shows the same right skew that has been present in the previous data subsets. However, the box and whiskers plot (Figure H-2) shows the presence of fewer outliers than in previous cases, possibly due to the smaller data set. According to the Wilk-Shapiro/Rankit plot (Figure H-3) and its accompanying statistic, the data for MBTU approximate a normal distribution. Scatter plots of MBTU versus HDD, CDD, CHDD, SQFT, AGE, and MAINT are located at Figures H-4 through H-9. HDD and CHDD show evidence of linear behavior by visual inspection, while CDD seems to lack it; for the other variables it is hard to discern a pattern because these are annual observations while MBTU is recorded monthly.

Table 4-19 shows the results of a correlation analysis performed using data from these nine bases. All of the variables except for CDD were seen to be strongly correlated with MBTU, and therefore were included in the linear regression model.

Table 4-20 shows the results of this regression analysis. All of the coefficients in this case are positive. However, the constant β_0 , SQFT, and MAINT were not determined to be statistically significant at $\alpha = 0.05$, since the P-values were greater than 0.05. The plot of standardized

residuals versus fitted values (Figure H-10) and the Wilk-Shapiro/Rankit plot (Figure H-11) show that the data appear to be homoscedastic and approximately normally distributed.

Table 4-19 Correlation Matrix (ACC Bases with Supplemental Data)

STATISTIX	4.1					, 09/20/95,	15:25
CORRELATIO	INES						
CDD P-VALUE	HDD 0.0283 0.5637	CDD	CHDD	SQFT	MAINT	AGE	
CHDD	0.8665 0.0000	0.5234 0.0000					
SQFT	0.6351 0.0000	0.5907 0.0000	0.8363 0.0000				
MAINT	0.5754 0.0000	0.5479 0.0000	0.7641 0.0000	0.7787 0.0000			
AGE	0.6412 0.0000	0.6405 0.0000	0.8664 0.0000	0.9553 0.0000	0.8730 0.0000		
MBTU	0.8363 0.0000	0.4509 0.0000	0.9380 0.0000	0.8932 0.0000	0.8233 0.0000	0.9271 0.0000	
CASES INCL	UDED 420	MISSING C	ASES 0				

Table 4-20 Regression Analysis (ACC Bases w/ Supplemental Data)

STATISTIX 4.	1				CAHUNA	1, 11/07/95,
16:23						
UNWEIGHTED L	EAST SQ	UARES LIN	IEAR REGRESSIO	ON OF MBTU		
PREDICTOR						
VARIABLES	COEFFI	CIENT	STD ERROR	STUDENT'S	T P	VIF
CONCEANE		0220	0.00120	2.44		
CONSTANT	-0.0	0338	0.00139	-2.44	0.015	
SQFT			1.720E-07			
CHDD			6.167E-07			0 1.1
AGE	3.186	E-04	6.310E-05	5.05	0.000	0 1.6
MAINT	0.0	0298	4.232E-04	7.04	0.000	0 1.2
			RESIDUAL STANDARD			
SOURCE	DF	SS	MS	F	P	
	463	0.00529	0.00192 0.1142E-05		0.0000	
CASES INCLUD	ED 468	MISSING	CASES 489			

Analysis of Bases by Flying/Nonflying Mission

Flying Mission. The histogram and box and whiskers plots (Figures 4-10 and 4-11) show the familiar right skew. The scatter plots of HDD and CHDD (Figures 4-13 and 4-15) show a positive linear relationship, while those for CDD and SQFT (Figures 4-14 and 4-16) are inconclusive. Table 4-21 shows the results of the correlation analysis performed on this data set. HDD and CHDD were strongly correlated, while SQFT was moderately correlated, so these three variables were included in the regression model. CDD was omitted because it was only weakly correlated. The results of the regression analysis are given in Table 4-22. In this case, all of the variables had positive coefficients, which is a departure from the previous analyses in which SQFT

was found to have a negative coefficient. All of the variables' coefficients were found to be statistically significant at $\alpha = 0.05$. The R² value obtained for this model and the P-value of 0.0000 indicate that the model fits this data set.

Figure 4-17, the plot of standardized residuals versus fitted values, appears to show homoscedasticity. The Wilk-Shapiro/Rankit plot of standardized residuals (Figure 4-18) shows that the residuals strongly approximate a normal distribution, and that the assumptions of the linear regression model appear to have been met.

Nonflying Mission. The graphs for this set of observations is found in Appendix I. The histogram and the box and whiskers plot (Figures I-1 and I-2) show a very large number of outliers and a strong skew to the right. The scatter plots (Figures I-4 through I-7) show the same tendencies as earlier data sets; HDD and CHDD (Figures I-4 and I-6) show an apparent positive linear relationship, while CDD and SQFT (Figures I-5 and I-7) are inconclusive. The results of the correlation analysis (Table 4-23) show that HDD and CHDD are moderately correlated with MBTU, while CDD and SQFT are weakly correlated. These results are statistically significant at $\alpha = 0.05$. The correlation coefficients obtained here are lower than for previous groupings. The two variables which were moderately correlated were included in the linear regression model, the results of which are given in Table 4-24. The only variable for which a coefficient was found which was significant at a = 0.05 was HDD. The R^2 value shows that this linear regression model fit the data set poorly. The plot of standardized residuals versus fitted values (Figure I-8) shows that the data appear to be heteroscedastic. The Wilk-Shapiro/Rankit plot (Figure I-9) shows that the residuals do not approximate a normal distribution. Therefore, the linear model is not applicable to this data set.

Table 4-21 Correlation Matrix (Flying Bases)

STATISTIX 10:33	4.1				, 09/28/95,
CORRELATIO	•	•	: CORRELAT	IONS = COSINES	
CDD P-VALUE	HDD 0.0217 0.3147	CDD	CHDD	SQFT	
CHDD	0.9100 0.0000	0.4343 0.0000			
SQFT	0.5793 0.0000	0.4899 0.0000	0.7251 0.0000		
MBTU	0.8568 0.0000	0.3620 0.0000	0.9221 0.0000	0.7877 0.0000	
CASES INCL	UDED 2151	MISSING	CASES 0		

Table 4-22 Regression Analysis (Flying Bases)

STATISTIX 4	.1					CAHU	JNA,	11/07/95,
16:34								
UNWEIGHTED	LEAST SQ	UARES LI	NEAR R	EGRESSIO	N OF MBTU			
PREDICTOR								
VARIABLES	COEFFI	CIENT	STD E	RROR	STUDENT'S	T	P	VIF
CONSTANT							0000	
~					3.65		0003	1.0
CHDD	1.611	E-05	3.228	E-07	49.91	0.0	0000	1.0
R-SQUARED								
ADJUSTED R-	SQUARED	0.5377	S	TANDARD	ERROR OF E	STIMATE	0.	.00481
					_	_		
SOURCE	DF	SS		MS	F	P		
REGRESSION					1251.24	0.0000		
RESIDUAL	_			.316E-05	•			
TOTAL		0.1076						
CASES INCLU	DED 2151	MISSI	NG CAS	ES 0				

Figure 4-10 Histogram (Flying Bases)

Figure 4-11 Box and Whisker Plot (Flying Bases)

Figure 4-12 Wilk-Shapiro/Rankit Plot (Flying Bases)

Figure 4-14 Scatter Plot: MBTU vs. CDD (Flying Bases)

Figure 4-15 Scatter Plot: MBTU vs. CHDD (Flying Bases)

Figure 4-16 Scatter Plot: MBTU vs. SQFT (Flying Bases)

Table 4-23 Correlation Matrix (Nonflying Bases)

STATISTIX 14:24	4.1				,	09/28/95,
CORRELATIO	•	•	: CORRELAT	IONS = COSINES		
CDD P-VALUE	HDD 0.0248 0.4013	CDD	CHDD	SQFT		
CHDD	0.8661 0.0000	0.5213 0.0000				
SQFT	0.4785 0.0000	0.4978 0.0000	0.6574 0.0000			
MBTU	0.5757 0.0000	0.3661 0.0000	0.6745 0.0000	0.4446 0.0000		
CASES INCL	UDED 1144	MISSING	CASES 0			

Table 4-24 Regression Analysis Table (Nonflying Bases)

STATISTIX 4 16:45	.1					CAHUN	A, 11/07/95,
UNWEIGHTED 1	LEAST SQU	JARES LIN	IEAR	REGRESSIO	N OF MBTU		
PREDICTOR VARIABLES	COEFFI	CIENT	STD	ERROR	STUDENT'S	Г Р	
CONSTANT					10.99 7.19		
R-SQUARED ADJUSTED R-S							
SOURCE	DF	SS	_	MS	F	P	
REGRESSION RESIDUAL TOTAL	1142	0.42509)			0.0000	
CASES INCLUI	DED 1144	MISSIN	ig C	ASES 0			

Summary

This chapter has presented the results of analyzing the data obtained from the DUERS report, as well as supplemental data obtained for nine ACC bases. When a model was constructed for all of the bases in this data set, it was found to be improper because the data did not fulfill the basic assumptions of the linear regression model. Four prospective methods for dividing the data set into subgroups were evaluated: by MAJCOM, by flying versus nonflying mission, by presence of a depot, and by fiscal year. Two of these, MAJCOM and flying/nonflying mission, were found to have substantially different mean levels of energy consumption.

By dividing the data into subsets by Major Command, much better results were obtained. The most satisfactory models were those constructed using data from bases in the commands whose major activity is flying operations: AMC, ACC, and AETC. The model constructed for AFMC and SPC demonstrated a poor fit. Adding variables which describe a bases infrastructure showed that these variables, MAINT and AGE, enhanced the ability to predict energy consumption when included in a linear regression model. The primary effect of dividing the data into subgroups seemed to be a reduction in the number of outliers and their effect on the linear regression model. There were two separate types of outliers which became apparent as the research progressed: The first was extreme values of either the dependent or independent variable for an individual installation. This could take the form of an unusually hot or cold month, or of an abnormally high or low level of energy consumption. The second type of outlier results from an installation which consistently produces extreme values of either the

dependent or independent variables in comparison with the other installations. Dividing the data into subgroups seemed to have the effect of reducing the number of the second type of outliers.

A large number of outliers were consistently seen above the apparent regression line in the plots of MBTU vs. CHDD. These may have occurred during periods when both the heating and cooling systems were operating. During the "transition months", wide swings may occur in mean daily temperature, which may have resulted in the systems' being unable to operate at a constant rate. This could conceivably have caused inefficiencies which would result in a higher energy consumption rate.

Dividing the data into two groups by flying versus nonflying mission showed that energy consumption at the bases with a flying mission could be successfully modeled using the existing set of variables, while the bases without a flying mission could not be modeled using the same techniques and variables.

V. Conclusions

Results of Research

Two objectives were identified in Chapter I: 1) To identify factors inherent to Air Force installations which influence energy consumption, and 2) To use these factors to develop a model or models which can be used to predict energy consumption at an Air Force base. The research and analysis described in previous chapters was directed toward these two goals.

First Research Objective. In the previous chapter, analysis of the data showed that climatic factors had the strongest influence on energy consumption per square foot. Cooling Degree Days, however, were consistently weakly correlated with energy consumption, and this variable was not included in any of the linear regression models. Heating Degree Days was often strongly correlated with energy consumption, as was the sum of Heating and Cooling Degree Days. The coefficient for these variables in all of the various regression models was positive. This is the expected result, as departure from a mean daily temperature of 65 degrees Fahrenheit will cause increased use of heating, ventilating, and air conditioning HVAC systems.

There are at least two possible explanations for the weak correlation between energy consumption and Cooling Degree Days:

- 1) The HVAC systems used to cool facilities at the installations studied in this thesis is inherently more efficient than that which is used to heat them.
- 2) All of the facilities at a given installation must be heated to a certain minimum temperature, while not all facilities must be cooled. During periods when the outside temperature drops below the freezing point, facilities must be heated in order to prevent damage to plumbing and fire-suppression systems. Cooling is primarily used to maintain a comfortable indoor working

environment. The exceptions to this would be the case of cold-storage facilities, and computer and communications facilities which must be cooled to offset the heat produced by electronic equipment.

In all but one of the regression models, square feet of facility floor space was found to be correlated with energy consumption, but its coefficient was negative. This would seem to indicate that larger installations are able to operate more efficiently, but the author has no explanation for this behavior. This variable was found to have a significant influence on energy consumption in only some of the models.

The two additional variables which were obtained for nine selected ACC bases, mean age of facilities and ratio of large maintenance facilities to total facility area, were found to be strongly correlated with energy consumption. However, when the linear regression model was constructed, only age was a significant influence. As was expected, energy consumption tended to increase as the mean age of facilities increased.

ANOVA analysis showed that dividing the data set into groups by major command and flying versus nonflying mission was valid, while there was no noticeable difference in energy consumption between those bases with a depot and those without. The factors in the first two analyses, however, were essentially very much the same, since the flying mission in the CONUS in concentrated in AMC, ACC, and AETC.

The final ANOVA analysis showed that there has been no significant annual reduction in mean monthly energy consumption per square foot for the four years considered in this thesis.

This indicates that using only energy consumption per square foot as a measure of merit may not

be practical; baselining using some form of regression model such as the ones constructed in this thesis would more realistically assess our energy conservation efforts.

Second Research Objective. Construction of a single linear regression model to predict energy consumption per square foot at any given Air Force base is not feasible. It appears that an adequate model could be constructed for the Major Commands whose major mission involves flight operations. When the data was separated into flying and nonflying bases, it was shown that the data for flying bases met the basic assumptions for the application of the linear regression model, while that for nonflying bases did not. This may be due to the fact that flying bases tend to have a fixed configuration, e.g. aircraft maintenance facilities, warehouse space, flight operations buildings, etc., while nonflying bases are much more diverse.

The linear regression models constructed for the flying commands were found to provide statistically significant predictions of energy consumption at a=0.05, with most R^2 values falling between 0.50 and 0.75. The analysis showed that modeling energy consumption with a multiple linear regression model is feasible for bases with a flying mission.

Recommendations for Further Research

There are three areas in which further research could improve upon the results of this thesis. The first would be to try to obtain more data on age and types of facilities at the various installations. While the data collected from the nine ACC bases was shown to be correlated with energy consumption at these bases, the sample was by no means complete. A larger number of bases would more fully enable the researcher to explore the impact of these variables on energy consumption.

Second, additional factors which may influence energy consumption could be considered. This is particularly true of the bases which do not have an active flying mission; this thesis showed that using the independent variables described herein, the linear regression model is not appropriate for these bases. Additional factors could be investigated which would allow the use of this powerful model to predict energy consumption at these bases.

Finally, other models could be applied to this type of data which might better predict energy consumption. All of the histograms examined in this thesis showed some degree of right skew, which could indicate the applicability of a logarithmic model. In addition, the data could be modeled on a time-series basis, since all of the observations were consecutive over a period of four years.

Conclusions

This thesis showed the feasibility of modeling energy consumption. As stated earlier, reducing our energy consumption has been a stated goal of the DoD since the mid-1970's. With the advent of pollution prevention programs, of which energy conservation is a part, this subject has increased in importance and will continue to do so. Since 1975, several goals for reduction of energy consumption have been established and tracked since that time; however, none has addressed the effects of external influences on our ability to meet energy use reduction goals. Conducting the research necessary to develop models against which our consumption could be baselined would allow us to more accurately measure the effectiveness of our conservation efforts, and to more effectively manage our energy use reduction programs.

Appendix A

STATISTIX 4.1 , 09/26/95, 9:22

VIEW DATA

CASE	BASE	FY	HDD	CDD	SQFT	MBTU CMD	D E F P L O Y T
CASE 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52	BASE 33.000 33.000 33.000 33.000 33.000 33.000 33.000 33.000 33.000 33.000 34.000 34.000 34.000 34.000 34.000 34.000 35.000	FY 94.000	HDD 142.00 420.00 541.00 625.00 442.00 295.00 109.00 31.000 0.0000	CDD 101.00 16.000 1.0000 0.0000 9.0000 11.000 152.00 430.00 464.00 414.00 269.00 0.0000	SQFT 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 2773.0 2339.0	MBTU CMD 0.0088 ACC 0.0084 ACC 0.0123 ACC 0.0133 ACC 0.0109 ACC 0.0092 ACC 0.0068 ACC 0.0064 ACC 0.0057 ACC 0.0057 ACC 0.0051 ACC 0.0051 ACC 0.0054 ACC 0.0054 ACC 0.0055 ACC 0.0073 ACC 0.0054 ACC 0.0057 ACC 0.0057 ACC 0.0071 ACC 0.0058 ACC 0.0071 ACC 0.0091 ACC 0.0116 ACC 0.0171 ACC 0.0098 ACC 0.0092 ACC 0.0094 ACC 0.0092 ACC 0.0092 ACC 0.0094 ACC 0.0095 ACC 0.0096 ACC 0.0097 ACC 0.0097 ACC 0.0068 ACC 0.0113 ACC 0.0133 ACC 0.0136 ACC 0.0133 ACC 0.0136 ACC 0.0073 ACC 0.0068 ACC 0.0074 ACC 0.0073 ACC 0.0073 ACC 0.0074 ACC 0.0073 ACC 0.0073 ACC 0.0074 ACC 0.0074 ACC 0.0073 ACC 0.0073 ACC 0.0074 ACC 0.0073 ACC 0.0074 ACC 0.0074 ACC 0.0075 ACC 0.0077 ACC 0	
53 54 55 56	37.000 37.000 37.000 37.000	94.000 94.000 94.000 94.000	299.00 116.00 52.000 1.0000	4.0000 26.000 151.00 292.00	3855.0 3855.0 3855.0 3855.0	0.0101 ACC 0.0089 ACC 0.0086 ACC 0.0067 ACC	Y N Y N Y N

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257 258 259 260	54.000 54.000 54.000 54.000	94.000 94.000 94.000 94.000	441.00 228.00 68.000 45.000	7.0000 25.000 90.000 152.00	2910.0 2910.0 2910.0 2910.0	0.0095 ACC 0.0100 ACC 0.0061 ACC 0.0067 ACC	Y Y Y Y	N N N

270 2712 273 274 275 277 278 279 281 282 288 288 288 288 289 291 292 293 300 300 301 313 313 314 315 317 317 318 318 318 318 318 318 318 318 318 318	55.000 55.000 55.000 55.000 55.000 55.000 55.000 33.000	94.000 94.000 94.000 94.000 94.000 94.000 93.000	575.00 314.00 92.000 4.0000 0.0000 2.0000 72.000 53.000 411.00 576.00 447.00 318.00 11.000 0.0000 0.0000 0.0000 11.000 23.000 338.00 610.00 596.00 406.00 176.00 164.00 25.000 18.000 0.0000	0.0000 26.000 79.000 352.00 374.00 313.00 146.00 65.000 1.0000 3.0000 7.0000 34.000 161.00 433.00 552.00 312.00 117.00 0.0000	2878.0 2878.0 2878.0 2878.0 2878.0 2878.0 2878.0 2879.0 3970.0 3970.0 3970.0 3970.0 3970.0 3970.0 3970.0 2655.0 2655.0 2655.0 2655.0 2655.0 2655.0 2655.0 2655.0 2295.0 23970.	0.0088 ACC 0.0079 ACC 0.0092 ACC 0.0077 ACC 0.0078 ACC 0.0073 ACC 0.0063 ACC 0.0067 ACC	Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	N N N N N N N
315 316 317 318 319 320 321 322 323 324 325	36.000 36.000 36.000 36.000 36.000 36.000 36.000 36.000 36.000 37.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 3767.0	0.0122 ACC 0.0144 ACC 0.0117 ACC 0.0104 ACC 0.0088 ACC 0.0079 ACC 0.0092 ACC 0.0077 ACC 0.0078 ACC 0.0073 ACC 0.0063 ACC	Y Y Y Y Y Y Y Y Y	N N N N N N N N
336 337 338 339 340	37.000 38.000 38.000 38.000 38.000	93.000 93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 0.0000 0.0000	474.00 0.0000 0.0000 0.0000 0.0000	3767.0 3028.0 3028.0 3028.0 3028.0	0.0067 ACC 0.0064 ACC 0.0092 ACC 0.0171 ACC 0.0160 ACC	Y Y Y Y Y	N N N N

34433445678901234567890123456789001234567890012345678900123456789001234567890012	38.000 38.000 38.000 38.000 38.000 38.000 38.000 39.000 39.000 39.000 39.000 39.000 39.000 39.000 40.000 40.000 40.000 40.000 40.000 40.000 41.000	93.000 93.000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 493.00 973.00 1418.0 1515.0 1390.0 842.00 666.00 264.00 171.00 666.000 146.00 281.00 624.00 797.00 1123.0 1248.0 1439.0 1099.0 551.00 279.00 1128.00 7.0000 17.000 212.00 111.00 670.00 670.00 670.00 641.00 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000	3028.0 3028.0 3028.0 3028.0 3028.0 3028.0 3028.0 3028.0 4917.0 4963.0 4979.0 4479.0	0.0149 ACC 0.0134 ACC 0.0094 ACC 0.0068 ACC 0.0074 ACC 0.0082 ACC 0.0078 ACC 0.0071 ACC 0.0135 ACC 0.0155 ACC 0.0179 ACC 0.0263 ACC 0.0241 ACC 0.0209 ACC 0.0069 ACC 0.0069 ACC 0.0069 ACC 0.0069 ACC 0.0069 ACC 0.0069 ACC 0.0235 ACC 0.0215 ACC 0.0215 ACC 0.0235 ACC 0.0235 ACC 0.0262 ACC 0.0283 ACC 0.0283 ACC 0.0283 ACC 0.0283 ACC 0.0262 ACC 0.0283 ACC 0.0276 ACC 0.0224 ACC 0.0105 ACC 0.0105 ACC 0.0105 ACC 0.0105 ACC 0.0107 ACC 0.0107 ACC 0.0137 ACC 0.0146 ACC 0.0147 ACC 0.0147 ACC 0.0148 ACC 0.0148 ACC 0.0149 ACC 0.0149 ACC 0.0140 ACC 0.0141 ACC	λ	\mathbf{n}
396 397 398 399 400 401	42.000 43.000 43.000 43.000 43.000 43.000	93.000 93.000 93.000 93.000 93.000 93.000	0.0000 238.00 394.00 676.00 761.00 723.00	0.0000 15.000 7.0000 0.0000 0.0000	2628.0 4170.0 4170.0 4170.0 4170.0 4170.0	0.0129 ACC 0.0085 ACC 0.0116 ACC 0.0181 ACC 0.0173 ACC 0.0191 ACC	Y Y Y Y Y	N N N N N

$\begin{array}{c} 4114\\4116\\789\\0\\123\\442\\234\\422\\34\\433\\433\\433\\433\\434\\434$	44.000 44.000 44.000 44.000 44.000 44.000 44.000 45.000 45.000 45.000 45.000 45.000 45.000 45.000 45.000 45.000 45.000 46.000 46.000 46.000 46.000 46.000 46.000 46.000 46.000 47.000 48.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000	286.00 178.00 55.000 0.0000 0.0000 0.0000	1.0000 47.000 63.000 346.00 526.00 624.00 577.00	3121.0 3121.0 3121.0 3121.0 3121.0 3121.0 3121.0 3121.0 3750.0	0.0085 ACC 0.0086 ACC 0.0066 ACC 0.0073 ACC 0.0082 ACC 0.0089 ACC 0.0085 ACC	X X X X X X X X X X X X X X X X X X X	N N N
458 459 460 461 462 463 464 465 466	48.000 48.000 48.000 48.000 48.000 48.000 48.000 48.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	174.00 268.00 186.00 286.00 178.00 55.000 0.0000 0.0000	104.00 21.000 33.000 1.0000 47.000 63.000 346.00 526.00 624.00	1826.0 1826.0 1826.0 1826.0 1826.0 1826.0 1826.0 1826.0	0.0070 ACC 0.0102 ACC 0.0100 ACC 0.0085 ACC 0.0086 ACC 0.0066 ACC 0.0073 ACC 0.0082 ACC 0.0089 ACC	Y Y Y Y Y Y Y	

483 484 485 486 487 488	50.000 50.000 50.000 50.000 50.000 50.000	93.000 93.000 93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000	4612.0 4612.0 4612.0 4612.0 4612.0 4612.0	0.0104 ACC 0.0118 ACC 0.0098 ACC 0.0069 ACC 0.0062 ACC 0.0060 ACC	Y Y Y Y Y	N N N N N
489 490 491 492 493	50.000 50.000 50.000 50.000 51.000	93.000 93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 0.0000 342.00	0.0000 808.00 767.00 0.0000 18.000	4612.0 4612.0 4612.0 4612.0 6015.0	0.0069 ACC 0.0076 ACC 0.0085 ACC 0.0071 ACC 0.0159 ACC	Y Y Y Y	N N N N
494 495 496 497	51.000 51.000 51.000 51.000	93.000 93.000 93.000 93.000	874.00 1131.0 1376.0 1191.0	0.0000 0.0000 0.0000 0.0000	6015.0 6015.0 6015.0 6015.0	0.0198 ACC 0.0232 ACC 0.0260 ACC 0.0229 ACC	Y Y Y Y	N N N
498 499 500 501 502	51.000 51.000 51.000 51.000 51.000	93.000 93.000 93.000 93.000	894.00 510.00 143.00 33.000 0.0000	0.0000 0.0000 24.000 191.00 319.00	6015.0 6015.0 6015.0 6015.0	0.0221 ACC 0.0174 ACC 0.0139 ACC 0.0145 ACC 0.0155 ACC	Y Y Y Y Y	N N N N
503 504 505 506 507	51.000 51.000 52.000 52.000 52.000	93.000 93.000 93.000 93.000 93.000	2.0000 28.000 180.00 354.00 604.00	320.00 160.00 26.000 25.000 0.0000	6015.0 6015.0 1758.0 1758.0 1758.0	0.0157 ACC 0.0140 ACC 0.0067 ACC 0.0117 ACC 0.0197 ACC	Y Y Y Y Y	N N N N
508 509 510 511 512	52.000 52.000 52.000 52.000 52.000	93.000 93.000 93.000 93.000 93.000	586.00 626.00 446.00 190.00 10.000	2.0000 0.0000 0.0000 27.000 229.00	1758.0 1758.0 1758.0 1758.0 1758.0	0.0188 ACC 0.0169 ACC 0.0147 ACC 0.0128 ACC 0.0215 ACC	Y Y Y Y	N N N N
513 514 515 516 517	52.000 52.000 52.000 52.000 53.000	93.000 93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 14.000 177.00	439.00 586.00 446.00 318.00 33.000	1758.0 1758.0 1758.0 1758.0 2684.0	0.0406 ACC 0.0097 ACC 0.0084 ACC 0.0100 ACC 0.0131 ACC	Y Y Y Y Y	N N N N
518 519 520 521 522	53.000 53.000 53.000 53.000 53.000	93.000 93.000 93.000 93.000 93.000	313.00 592.00 574.00 641.00 442.00	22.000 0.0000 0.0000 0.0000 0.0000	2684.0 2684.0 2684.0 2684.0 2684.0	0.0157 ACC 0.0188 ACC 0.0209 ACC 0.0182 ACC 0.0183 ACC	Y Y Y Y Y	N N N N
523 524 525 526 527	53.000 53.000 53.000 53.000 53.000	93.000 93.000 93.000 93.000 93.000	140.00 2.0000 0.0000 0.0000	41.000 331.00 414.00 611.00 451.00	2684.0 2684.0 2684.0 2684.0 2684.0	0.0129 ACC 0.0096 ACC 0.0092 ACC 0.0096 ACC 0.0103 ACC	Y Y Y Y Y	N N N N
528 529 530 531	53.000 54.000 54.000 54.000	93.000 93.000 93.000 93.000	12.000 136.00 0.0000 580.00	305.00 30.000 0.0000 0.0000	2684.0 2910.0 2910.0 2910.0	0.0085 ACC 0.0074 ACC 0.0092 ACC 0.0123 ACC	Y Y Y Y	N N N
532 533 534 535 536	54.000 54.000 54.000 54.000	93.000 93.000 93.000 93.000	507.00 0.0000 405.00 185.00 9.0000	3.0000 0.0000 0.0000 23.000 196.00	2910.0 2910.0 2910.0 2910.0	0.0138 ACC 0.0125 ACC 0.0138 ACC 0.0093 ACC 0.0075 ACC	Y Y Y Y	N N N N
537 538 539 540 541	54.000 54.000 54.000 54.000 55.000	93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 9.0000 255.00	383.00 622.00 515.00 350.00 30.000	2910.0 2910.0 2910.0 2910.0 2786.0	0.0082 ACC 0.0093 ACC 0.0090 ACC 0.0092 ACC 0.0115 ACC	Y Y Y Y	N N N N
542 543 544 545 546	55.000 55.000 55.000 55.000	93.000 93.000 93.000 93.000	9.0000 921.00 1091.0 972.00 753.00	172.00 0.0000 0.0000 0.0000 0.0000	2786.0 2786.0 2786.0 2786.0 2786.0	0.0162 ACC 0.0177 ACC 0.0214 ACC 0.0129 ACC 0.0132 ACC	Y Y Y Y Y	N N N N
547 548 549 550 551	55.000 55.000 55.000 55.000	93.000 93.000 93.000 93.000 93.000	402.00 82.000 22.000 0.0000 3.0000	0.0000 56.000 278.00 430.00 430.00	2786.0 2786.0 2786.0 2786.0 2786.0	0.0166 ACC 0.0114 ACC 0.0107 ACC 0.0110 ACC 0.0123 ACC	Y Y Y Y Y	N N N N
552 553	55.000 33.000	93.000 92.000	110.00 57.000	76.000 126.00	2786.0 4163.0	0.0131 ACC 0.0085 ACC	Y Y	N N

55555555555555555555555555555555555555	37.000 37.000 37.000 37.000 37.000 37.000 37.000 37.000 37.000 38.000 38.000 38.000 38.000 38.000 38.000 38.000 38.000 38.000 38.000	92.000 92.000	0.0000 433.00 0.0000 0.0000 0.0000 97.000 24.000 0.0000 0.0000 11.000 73.000 0.0000 0.	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 189.00 378.00 281.00 281.00 255.00 0.0000 0.0000 0.0000 0.0000 0.0000 38.000 297.00 309.00 491.00 306.00 17.000 0.0000	4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 4163.0 2655.0 2655.0 2655.0 2655.0 2655.0 2655.0 2655.0 2655.0 2129.0 2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 2779.0 2799.0 2991.0	0.0097 ACC 0.0095 ACC 0.0087 ACC 0.0070 ACC 0.0066 ACC 0.0067 ACC 0.0068 ACC 0.0067 ACC 0.0067 ACC 0.0085 ACC 0.0145 ACC 0.0145 ACC 0.0156 ACC 0.0189 ACC 0.0172 ACC 0.0153 ACC 0.0097 ACC 0.0089 ACC	λ	
619	38.000	92.000	207.00	46.000	2991.0	0.0097 ACC	Y	N

33333333333333333333333333333333333333	9.000 9.000 9.000 9.000 9.000 9.000 9.000 9.000 9.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 2.000 2.000 2.000 2.000 2.000 2.000 2.000 2.000 2.000 3.000 3.000 3.000 3.000 3.000 3.000 3.000 3.000 4.000 4.000 4.000 4.000	92.000 92.000	997.00 0.0000 0.0000 0.0000 0.0000 0.0000 138.00 0.0000 138.00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.53.00 262.00 99.000 34.000 186.00 160.00 251.00 325.00	0.0000 0.0000 0.0000 0.0000 0.0000 36.000 41.000 51.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 42.000 48.000 70.000 42.000 0.0000	4917.0 4917.0 4917.0 4917.0 4917.0 4917.0 4917.0 4917.0 4917.0 4917.0 4963.0 4023.0 4024.0 4124.0	0.0163 ACC 0.0113 ACC 0.0187 ACC 0.0192 ACC 0.0174 ACC 0.0179 ACC 0.0095 ACC 0.0109 ACC 0.0108 ACC 0.0106 ACC 0.0106 ACC 0.0164 ACC 0.0164 ACC 0.0164 ACC 0.0165 ACC 0.0164 ACC 0.0165 ACC	Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	
689 4 690 4 691 4 692 4 693 4 694 4	4.000 4.000 4.000 4.000 4.000 4.000	92.000	419.00	0.0000	2875.0	0.0153 ACC	Y	N

66666777777777777777777777777777777777	44.000 45.000 45.000 45.000 45.000 45.000 45.000 45.000 45.000 46.000 46.000 46.000 46.000 46.000 46.000 46.000 46.000 47.000 49.000 40.000 40.000 40.000 40.000	92.000 92.000	11.000 639.00 988.00 1583.0 1583.0 1583.0 1583.00 1583.00 1583.00 1583.00 1682.0 1551.0 1380.0 873.00 97.000 80.000 87.000 69.000 157.00 60.000 157.00 60.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 1274.0 1481.0 1258.0 1296.0 939.00 892.00 319.00 2256.00 411.00 225.00 2266.00 411.00 225.00 2256.00 411.00 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 149.00 71.000 206.00 313.000 313.000	2.0000 0.0000 0.0000 0.0000 0.0000 12.000 80.000 207.00 253.00 348.00 60.000 285.00	2875.0 3750.0 3750.0 3750.0 3750.0 3750.0 3750.0 3750.0 3750.0 3750.0 3773.0 3773.0 3773.0 3773.0 3773.0 3773.0 3773.0 3774.0	0.0168 ACC 0.0200 ACC 0.0271 ACC 0.0247 ACC 0.0221 ACC 0.0176 ACC 0.0176 ACC 0.0106 ACC 0.0102 ACC 0.0115 ACC 0.0116 ACC 0.0118 ACC 0.0118 ACC	Y Y
752 753 754 755 756	49.000 49.000 49.000 49.000 49.000	92.000 92.000 92.000 92.000 92.000	326.00 81.000 51.000 3.0000 35.000 118.00	12.000 80.000 207.00 253.00 348.00 60.000	2329.0 2329.0 2329.0 2329.0 2329.0	0.0176 ACC 0.0106 ACC 0.0102 ACC 0.0115 ACC 0.0116 ACC 0.0118 ACC	Y N Y N Y N Y N Y N

816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833	50.000 50.000 51.000 51.000 51.000 51.000 51.000 51.000 51.000 51.000 51.000 51.000 51.000 52.000 53.000 53.000 53.000 53.000 53.000 54.000 54.000 54.000 54.000 54.000 54.000 54.000 55.000	92.000 92.000 92.000 92.000 92.000 92.000 92.000 92.000 92.000 92.000 92.000 91.000 91.000 91.000	0.0000 0.0000 388.00 1013.0 910.00 999.00 752.00 643.00 437.00 78.000 6.0000 0.0000 2.0000 81.000 129.00 354.00 363.00 626.00 661.00 317.00 350.00 104.00 16.000 0.0000	801.00 0.0000 9.0000 0.0000 0.0000 0.0000 0.0000 0.0000 11.000 123.00 120.00 61.000 25.000 28.000 0.0000 8.0000 170.00 170.00 170.00 18.000 275.00 28.000 0.0000 81.000 0.0000 81.000 0.0000	4612.0 4612.0 6015.0 6015.0 6015.0 6015.0 6015.0 6015.0 6015.0 6015.0 1758.0 1759.0 1759.0 1759.0 1759.0 1759.0	0.0089 ACC 0.0138 ACC 0.0182 ACC 0.0183 ACC 0.0194 ACC 0.0186 ACC 0.0178 ACC 0.0110 ACC 0.0118 ACC 0.0118 ACC 0.0138 ACC 0.0138 ACC 0.0124 ACC 0.0098 ACC 0.0089 ACC 0.0130 ACC 0.0142 ACC 0.0142 ACC 0.0112 ACC	λ	
834 835 836 837	33.000 33.000 33.000 33.000	91.000 91.000 91.000 91.000	0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 436.00	4022.0 4022.0 4022.0 4022.0	0.0096 ACC 0.0073 ACC 0.0074 ACC 0.0077 ACC	Y Y Y Y	N N N

909	91.000 91.000	25.000 1.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 137.00 415.00 673.00 730.00 506.00 444.00 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	78.000 262.00 0.0000	4633.0 4633.0 4633.0 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 3994.0 3994.0 3994.0 3994.0 3994.0 3994.0 3994.0 3994.0 3994.0 3994.0 3992.0 2392.0	0.0077 ACC 0.0079 ACC 0.0076 ACC 0.0076 ACC 0.0083 ACC 0.0000 ACC 0.0001 ACC 0.0010 ACC 0.0011 ACC 0.0158 ACC 0.0166 ACC 0.0111 ACC 0.0123 ACC 0.0055 ACC 0.0055 ACC 0.0055 ACC 0.0055 ACC 0.0055 ACC 0.0010 ACC 0.0111 ACC 0.0168 ACC 0.0111 ACC 0.0169 ACC 0.0129 ACC 0.0135 ACC 0.0093 ACC 0.0093 ACC 0.0093 ACC 0.0093 ACC 0.0094 ACC 0.0093 ACC 0.0093 ACC 0.0093 ACC 0.0094 ACC 0.0094 ACC 0.0095 ACC 0.0097 ACC 0.0097 ACC 0.0093 ACC 0.0093 ACC 0.0093 ACC 0.0094 ACC 0.0095 ACC 0.0095 ACC 0.0097 ACC	K K K K K K K K K K K K K K K K K K K
975 45.000	91.000	0.0000	0.0000	3750.0	0.0291 ACC	Y N

980	45.000	91.000	0.0000	0.0000	3750.0	0.0174 ACC	Y N
981	45.000	91.000	161.00	51.000	3750.0	0.0079 ACC	Y N
982	45.000	91.000	61.000	108.00	3750.0	0.0047 ACC	Y N
983	45.000	91.000	0.0000	0.0000	3750.0	0.0045 ACC	Y N
984 985 986 987 988	45.000 46.000 46.000	91.000 91.000 91.000 91.000 91.000	0.0000 5.0000 6.0000 77.000 75.000	0.0000 458.00 219.00 131.00 130.00	3750.0 3773.0 3773.0 3773.0 3773.0	0.0053 ACC 0.0086 ACC 0.0080 ACC 0.0073 ACC	Y N Y N Y N
989 990 991 992	46.000 46.000 46.000 46.000	91.000 91.000 91.000 91.000	70.000 37.000 0.0000 0.0000	78.000 161.00 377.00 531.00	3773.0 3773.0 3773.0 3773.0	0.0082 ACC 0.0067 ACC 0.0071 ACC 0.0081 ACC 0.0104 ACC	Y N Y N Y N Y N Y N
993	46.000	91.000	0.0000	534.00	3773.0	0.0098 ACC	Y N
994	46.000	91.000	0.0000	565.00	3773.0	0.0103 ACC	Y N
995	46.000	91.000	0.0000	601.00	3773.0	0.0095 ACC	Y N
996	46.000	91.000	0.0000	563.00	3773.0	0.0098 ACC	Y N
997	47.000	91.000	655.00	0.0000	3345.0	0.0201 ACC	Y N
998	47.000	91.000	0.0000	0.0000	3345.0	0.0266 ACC	Y N
999	47.000	91.000	0.0000	0.0000	3345.0	0.0326 ACC	Y N
1000	47.000	91.000	2022.0	0.0000	3345.0	0.0362 ACC	Y N
1001 1002 1003 1004 1005	47.000 47.000 47.000 47.000	91.000 91.000 91.000 91.000 91.000	1328.0 1144.0 748.00 437.00 22.000	0.0000 0.0000 0.0000 17.000 96.000	3345.0 3345.0 3345.0 3345.0 3345.0	0.0265 ACC 0.0274 ACC 0.0210 ACC 0.0162 ACC 0.0097 ACC	Y N Y N Y N Y N Y N
1005 1006 1007 1008 1009	47.000 47.000 47.000 47.000 48.000	91.000 91.000 91.000 91.000	10.000 12.000 142.00 53.000	166.00 145.00 144.00 212.00	3345.0 3345.0 3345.0 1780.0	0.0109 ACC 0.0113 ACC 0.0110 ACC 0.0076 ACC	Y N Y N Y N Y N
1010	48.000	91.000	148.00	23.000	1780.0	0.0065 ACC	Y N
1011	48.000	91.000	239.00	26.000	1780.0	0.0090 ACC	Y N
1012	48.000	91.000	396.00	6.0000	1780.0	0.0108 ACC	Y N
1013	48.000	91.000	251.00	9.0000	1780.0	0.0089 ACC	Y N
1014	48.000	91.000	144.00	67.000	1780.0	0.0074 ACC	Y N
1015	48.000	91.000	14.000	192.00	1780.0	0.0072 ACC	Y N
1016	48.000	91.000	0.0000	346.00	1780.0	0.0080 ACC	Y N
1017	48.000	91.000	0.0000	448.00	1780.0	0.0077 ACC	Y N
1018	48.000	91.000	0.0000	538.00	1780.0	0.0083 ACC	Y N
1019	48.000	91.000	0.0000	510.00	1780.0	0.0082 ACC	Y N
1020	48.000	91.000	0.0000	430.00	1780.0	0.0076 ACC	Y N
1021	49.000	91.000	487.00	195.00	2516.0	0.0180 ACC	Y N
1022	49.000	91.000	711.00	0.0000	2516.0	0.0192 ACC	Y N
1023	49.000	91.000	1425.0	0.0000	2516.0	0.0193 ACC	Y N
1024	49.000	91.000	1208.0	0.0000	2516.0	0.0292 ACC	Y N
1025	49.000	91.000	670.00	0.0000	2516.0	0.0215 ACC	Y N
1026	49.000	91.000	711.00	0.0000	2516.0	0.0182 ACC	Y N
1027 1028 1029 1030 1031	49.000 49.000 49.000 49.000	91.000 91.000 91.000 91.000 91.000	515.00 315.00 40.000 0.0000 0.0000	0.0000 0.0000 95.000 384.00 371.00	2516.0 2516.0 2516.0 2516.0 2516.0	0.0166 ACC 0.0140 ACC 0.0100 ACC 0.0095 ACC 0.0095 ACC	Y N Y N Y N Y N Y N
1032	49.000	91.000	68.000	89.000	2516.0	0.0104 ACC	Y N
1033	50.000	91.000	26.000	157.00	4398.0	0.0092 ACC	Y N
1034	50.000	91.000	10.000	0.0000	4398.0	0.0081 ACC	Y N
1035	50.000	91.000	792.00	0.0000	4398.0	0.0135 ACC	Y N
1036 1037 1038 1039	50.000 50.000 50.000	91.000 91.000 91.000 91.000	646.00 282.00 339.00 44.000	0.0000 0.0000 0.0000 53.000	4398.0 4398.0 4398.0 4398.0	0.0120 ACC 0.0103 ACC 0.0107 ACC 0.0086 ACC	Y N Y N Y N
1040	50.000	91.000	16.000	194.00	4398.0	0.0084 ACC	Y N
1041	50.000	91.000	0.0000	535.00	4398.0	0.0090 ACC	Y N
1042	50.000	91.000	809.00	0.0000	4398.0	0.0104 ACC	Y N
1043	50.000	91.000	0.0000	725.00	4398.0	0.0112 ACC	Y N
1044	50.000	91.000	0.0000	550.00	4398.0	0.0111 ACC	Y N
1045	51.000	91.000	348.00	11.000	6015.0	0.0167 ACC	Y N
1046	51.000	91.000	633.00	1.0000	6015.0	0.0174 ACC	Y N
1047	51.000	91.000	1314.0	0.0000	6015.0	0.0239 ACC	Y N
1048	51.000	91.000	1476.0	0.0000	6015.0	0.0250 ACC	Y N
1049	51.000	91.000	845.00	0.0000	6015.0	0.0185 ACC	Y N
1050	51.000	91.000	669.00	5.0000	6015.0	0.0201 ACC	Y N

1051 1052 1053 1054 1055 1056 1057 1056 1057 1061 1062 1063 1064 1065 1067 1067 1077 1077 1077 1077 1077 1077	51.000 51.000 51.000 51.000 51.000 51.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 52.000 53.000 54.000 54.000 54.000 54.000 55.000	91.000 91.000	327.00 102.00 0.0000 0.0000 305.00 114.00 100.00 298.00 459.00 650.00 437.00 312.00 99.000 16.000 0.0000 0.0000 17.000 163.00 289.00 439.00 439.00 599.00 465.00 311.00 109.00 114.000 0.0000	19.000 170.00 303.00 303.00 365.00 0.0000 161.00 141.00 0.0000 0.0000 7.0000 44.000 106.00 299.00 411.00 553.00 456.00 283.00 102.00 2.0000 10.000 45.000 104.00 282.00 360.00 530.00 420.00 245.00 151.00 200.00 40.000 40.000 40.000 40.000 40.000 40.000 40.000 533.00 410.00 533.00 420.00 245.00 151.00 200.00 40.000 0.0000 6.0000 40.000 0.0000	6015.0 6015.0 6015.0 6015.0 6015.0 6015.0 1892.0 1892.0 1892.0 1892.0 1892.0 1892.0 1892.0 1892.0 1892.0 1892.0 2639.0 2639.0 2639.0 2639.0 2639.0 2639.0 2639.0 2639.0 2639.0 2850.0 2850.0 2850.0 2850.0 2850.0 2850.0 2850.0 2219.0 2376.0 2376.0 2376.0 2376.0 2376.0 2376.0 2376.0 2376.0	0.0074 ACC 10.0123 ACC 10.0123 ACC 10.0158 ACC 10.0157 ACC 10.0042 ACC 10.0087 ACC 10.0087 ACC 10.0097 ACC 10.0157 ACC 10.0157 ACC 10.0157 ACC 10.0157 ACC 10.0161 ACC 10.0085 ACC 10.0161 ACC 10.0085 ACC 10.0161	
1109 1110 1111 1112 1113	16.000 16.000 16.000 16.000	91.000 91.000 91.000 91.000 91.000	356.00 259.00 62.000 10.000 0.0000	0.0000 21.000 79.000 301.00 443.00	2376.0 2376.0 2376.0 2376.0	0.0128 AETC N 0.0125 AETC N 0.0072 AETC N 0.0066 AETC N	1 N N N N N N N N N N N N N N N N N N N

1122 1123 1124 1125 1126 1127 1128 1129 1130 1131 1133 1134 1135 1136 1137 1138 1139 1140 1141 1142 1143 1144 1145 1146 1151 1152 1153 1154 1155 1156 1157 1158 1159 1161 1162 1163 1164 1167 1168 1170 1171 1172 1173 1174 1177 1178 1177 1178 1177 1178 1179 1180	17.000 17.000 17.000 17.000 17.000 17.000 17.000 17.000 18.000 18.000 18.000 18.000 18.000 18.000 18.000 18.000 19.000 19.000 19.000 19.000 19.000 19.000 19.000 19.000 20.000 20.000 20.000 20.000 20.000 20.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 22.000 22.000 22.000 22.000 22.000	91.000 91.000	628.00 232.00 53.000 0.0000 0.0000 0.0000 0.0000 175.000 251.000 488.000 424.00 284.00 51.000 6.0000 0.0000 0.0000 124.00 257.00 610.00 651.00 364.00 214.00 257.00 651.00 364.00 214.00 38.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000	0.0000 25.000 263.00 449.00 386.00 225.00 81.000 16.000 2.0000 0.0000 43.000 66.000 289.00 418.00 548.00 328.00 38.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 30.000 98.000 413.00 65.000 11.000 407.00 539.00 12.000 11.000 407.00 539.00	4631.0 4631.0 4631.0 4631.0 4631.0 4631.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 1475.0 14790.0 1790.	0.0153 AETC N 10.0125 AETC N 10.0129 AETC N 10.0131 AETC N 10.0131 AETC N 10.0107 AETC N 10.0082 AETC Y 10.0108 AETC Y 10.0108 AETC Y 10.0144 AETC Y 10.0174 AETC Y 10.0104 AETC Y 10.0093 AETC Y 10.0093 AETC Y 10.0096 AETC Y 10.0096 AETC Y 10.0096 AETC N 10.0134 AETC N 10.0103 AETC N 10.0086 AETC N 10.0086 AETC N 10.0096 AETC N 10.0086 AETC N 10.0095 AETC N 10.0132 AETC N 10.0134	
1174 1175 1176 1177 1178 1179 1180 1181 1182	21.000 21.000 21.000 22.000 22.000 22.000	91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 0.0000 34.000 164.00 442.00	556.00 543.00 381.00 226.00 83.000 23.000	7019.0 7019.0 7019.0 10326.0 10326.0 10326.0	0.0097 AETC N N 0.0110 AETC N N 0.0091 AETC N N 0.0044 AETC N N 0.0043 AETC N N 0.0060 AETC N N 0.0069 AETC N N 0.0052 AETC N N 0.0052 AETC N N 0.0043 AETC N N 0.0043 AETC N N 0.0043 AETC N N 0.0044 AETC N 0.0044 AET	N N N N N
1183 1184 1185 1186 1187 1188 1189 1190 1191 1192	22.000 22.000 22.000 22.000 22.000 22.000 23.000 23.000 23.000 23.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	9.0000 0.0000 0.0000 0.0000 6.0000 58.000 125.00 338.00 359.00	210.00 378.00 523.00 579.00 630.00 372.00 158.00 81.000 1.0000	10326.0 10326.0 10326.0 10326.0 10326.0 10326.0 1447.0 1447.0 1447.0	0.0047 AETC N 1 0.0050 AETC N 1 0.0046 AETC N 1 0.0049 AETC N 1 0.0043 AETC N 1 0.0077 AETC Y 1 0.0095 AETC Y 1	

1193	23.000	91.000	163.00	21.000	1447.0	0.0091 AETC Y N
1194	23.000	91.000	35.000	147.00	1447.0	0.0079 AETC Y N
1195	23.000	91.000	0.0000	357.00	1447.0	0.0079 AETC Y N
1196	23.000	91.000	0.0000	578.00	1447.0	0.0095 AETC Y N
1197	23.000	91.000	0.0000	638.00	1447.0	0.0083 AETC Y N
1198	23.000	91.000	0.0000	703.00	1447.0	0.0091 AETC Y N
1199 1200	23.000	91.000 91.000	0.0000	741.00 419.00	1447.0 1447.0	0.0098 AETC Y N 0.0081 AETC Y N
1201	24.000	91.000	400.00	3.0000	5152.0	0.0116 AETC Y N
1202	24.000	91.000	646.00	0.0000	5152.0	0.0154 AETC Y N
1203 1204	24.000 24.000 24.000	91.000 91.000 91.000	1175.0 1209.0	0.0000	5152.0 5152.0	0.0227 AETC Y N 0.0224 AETC Y N
1205	24.000	91.000	714.00	0.0000	5152.0	0.0171 AETC Y N
1206	24.000	91.000	726.00	0.0000	5152.0	0.0202 AETC Y N
1207	24.000	91.000	573.00	1.0000	5152.0	0.0143 AETC Y N
1208	24.000	91.000	209.00	22.000	5152.0	0.0085 AETC Y N
1209	24.000	91.000		139.00	5152.0	0.0064 AETC Y N
1210	24.000	91.000	14.000	227.00	5152.0	0.0063 AETC Y N
1211	24.000	91.000	7.0000	182.00	5152.0	0.0062 AETC Y N
1212	24.000	91.000	194.00	48.000	5152.0	0.0066 AETC Y N
1213	25.000	91.000	0.0000	294.00	3446.0	0.0091 AETC Y N
1214	25.000	91.000	130.00	36.000	3446.0	0.0058 AETC Y N
1215	25.000	91.000	447.00	0.0000	3446.0	0.0126 AETC Y N
1216	25.000	91.000	363.00		3446.0	0.0125 AETC Y N
1217	25.000	91.000	79.000	13.000	3446.0	0.0109 AETC Y N
1218	25.000	91.000	29.000		3446.0	0.0090 AETC Y N
1219	25.000	91.000	19.000	114.00	3446.0	0.0094 AETC Y N
1220	25.000	91.000	153.00	29.000	3446.0	0.0094 AETC Y N
1221	25.000	91.000	0.0000	624.00	3446.0	0.0096 AETC Y N
1222	25.000	91.000	0.0000	860.00	3446.0	0.0095 AETC Y N
1223	25.000	91.000		830.00	3446.0	0.0093 AETC Y N
1224	25.000	91.000	0.0000	0.0000	3446.0	0.0082 AETC Y N
1225	26.000	91.000	92.000	157.00	3725.0	0.0120 AETC N N
1226	26.000	91.000	229.00	12.000	3725.0	0.0127 AETC N N
1227	26.000	91.000	365.00	11.000	3725.0	0.0163 AETC N N
1228	26.000	91.000	520.00	0.0000	3725.0	0.0189 AETC N N
1229	26.000	91.000	322.00	4.0000	3725.0	0.0148 AETC N N
1230	26.000	91.000	224.00		3725.0	0.0141 AETC N N
1231 1232	26.000 26.000	91.000 91.000	29.000	130.00	3725.0 3725.0	0.0113 AETC N N 0.0142 AETC N N
1233	26.000	91.000	0.0000	407.00	3725.0	0.0158 AETC N N
1234	26.000	91.000	0.0000	539.00	3725.0	0.0145 AETC N N
1235	26.000	91.000	0.0000	508.00	3725.0	0.0138 AETC N N
1236	26.000	91.000	1.0000	355.00	3725.0	0.0110 AETC N N
1237	27.000	91.000	60.000	194.00	3542.0	0.0096 AETC Y N
1238	27.000	91.000	144.00	95.000	3542.0	0.0098 AETC Y N
1239	27.000	91.000	393.00	37.000	3542.0	0.0153 AETC Y N
1240	27.000	91.000	466.00	0.0000	3542.0	0.0159 AETC Y N
1241 1242	27.000 27.000 27.000	91.000 91.000 91.000	240.00 118.00	12.000 72.000	3542.0 3542.0 3542.0	0.0159 AETC Y N 0.0117 AETC Y N 0.0093 AETC Y N
1243	27.000	91.000	10.000	212.00	3542.0	0.0089 AETC Y N
1244	27.000	91.000		382.00	3542.0	0.0085 AETC Y N
1245	27.000	91.000	0.0000	523.00	3542.0	0.0090 AETC Y N
1246	27.000	91.000	0.0000	583.00	3542.0	0.0102 AETC Y N
1247	27.000	91.000	0.0000	635.00	3542.0	0.0096 AETC Y N
1248	27.000	91.000	5.0000	386.00	3542.0	0.0088 AETC Y N
1249	28.000	91.000	152.00	20.000	1365.0	0.0109 AETC Y N
1250	28.000	91.000	379.00	4.0000	1365.0	0.0162 AETC Y N
1251	28.000	91.000	792.00		1365.0	0.0209 AETC Y N
1252	28.000	91.000	792.00	0.0000	1365.0	0.0222 AETC Y N
1253	28.000	91.000	424.00	0.0000	1365.0	0.0166 AETC Y N
1254	28.000	91.000	322.00	8.0000	1365.0	0.0154 AETC Y N
1255	28.000	91.000	73.000	53.000	1365.0	0.0111 AETC Y N
1256	28.000	91.000	12.000	339.00	1365.0	0.0089 AETC Y N
1257	28.000	91.000	0.0000	443.00	1365.0	0.0089 AETC Y N
1258	28.000	91.000	0.0000	486.00	1365.0	0.0090 AETC Y N
1259	28.000	91.000	0.0000	462.00	1365.0	0.0087 AETC Y N
1260	28.000	91.000	53.000	208.00	1365.0	0.0078 AETC Y N
1261	29.000	91.000	122.00	95.000	5703.0	0.0069 AETC N N
1262	29.000	91.000	257.00	20.000	5703.0	0.0073 AETC N N
1263	29.000	91.000	745.00		5703.0	0.0137 AETC N N

1264 1265 1266 1267 1268 1269 1270 1271 1272	29.000 29.000 29.000 29.000 29.000 29.000 29.000 29.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	770.00 376.00 243.00 63.000 17.000 0.0000 28.000 28.000	0.0000 1.0000 24.000 80.000 279.00 444.00 241.00 503.00 241.00	5703.0 5703.0 5703.0 5703.0 5703.0 5703.0 5703.0 5703.0	0.0147 AETC N N 0.0098 AETC N N 0.0076 AETC N N 0.0057 AETC N N 0.0063 AETC N N 0.0062 AETC N N 0.0069 AETC N N 0.0066 AETC N N 0.0052 AETC N N
1273 1274 1275 1276 1277 1278 1279 1280	30.000 30.000 30.000 30.000 30.000 30.000 30.000	91.000 91.000 91.000 91.000 91.000 91.000	9.0000 85.000 201.00 278.00 205.00 145.00 9.0000	301.00 43.000 45.000 3.0000 7.0000 47.000 164.00 349.00	3505.0 3505.0 3505.0 3505.0 3505.0 3505.0 3505.0	0.0082 AETC Y N 0.0077 AETC Y N 0.0093 AETC Y N 0.0109 AETC Y N 0.0095 AETC Y N 0.0079 AETC Y N 0.0081 AETC Y N
1281 1282 1283 1284 1285 1286 1287	30.000 30.000 30.000 30.000 31.000 31.000 31.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 0.0000 0.0000 0.0000 210.00 460.00 986.00	415.00 491.00 464.00 403.00 39.000 8.0000	3505.0 3505.0 3505.0 3505.0 1088.0 1088.0	0.0084 AETC Y N 0.0089 AETC Y N 0.0095 AETC Y N 0.0096 AETC Y N 0.0100 AETC Y N 0.0109 AETC Y N 0.0219 AETC Y N
1288 1289 1290 1291 1292 1293 1294 1295	31.000 31.000 31.000 31.000 31.000 31.000 31.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	1030.0 697.00 408.00 225.00 38.000 0.0000 0.0000	0.0000 0.0000 13.000 35.000 240.00 414.00 534.00 495.00	1088.0 1088.0 1088.0 1088.0 1088.0 1088.0 1088.0	0.0211 AETC Y N 0.0215 AETC Y N 0.0123 AETC Y N 0.0090 AETC Y N 0.0083 AETC Y N 0.0073 AETC Y N 0.0094 AETC Y N 0.0080 AETC Y N
1296 1297 1298 1299 1300 1301 1302 1303	31.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	53.000 34.000 164.00 442.00 510.00 256.00 106.00 9.0000	228.00 226.00 83.000 23.000 0.0000 8.0000 88.000 210.00	1088.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0	0.0081 AETC Y N 0.0317 AETC N N 0.0313 AETC N N 0.0316 AETC N N 0.0333 AETC N N 0.0264 AETC N N 0.0290 AETC N N 0.0262 AETC N N
1304 1305 1306 1307 1308 1309 1310 1311	32.000 32.000 32.000 32.000 32.000 16.000 16.000	91.000 91.000 91.000 91.000 91.000 92.000 92.000	0.0000 0.0000 0.0000 0.0000 6.0000 146.00 603.00 624.00	379.00 523.00 579.00 631.00 372.00 105.00 0.0000	1700.0 1700.0 1700.0 1700.0 1700.0 2388.0 2388.0 2388.0	0.0318 AETC N N 0.0315 AETC N N 0.0338 AETC N N 0.0329 AETC N N 0.0302 AETC N N 0.0064 AETC Y N 0.0170 AETC Y N 0.0144 AETC Y N
1312 1313 1314 1315 1316 1317 1318	16.000 16.000 16.000 16.000 16.000 16.000	92.000 92.000 92.000 92.000 92.000 92.000 92.000	656.00 383.00 234.00 108.00 38.000 0.0000	0.0000 0.0000 10.000 69.000 184.00 372.00 525.00	2388.0 2388.0 2388.0 2388.0 2388.0 2388.0 2388.0	0.0168 AETC Y N 0.0109 AETC Y N 0.0110 AETC Y N 0.0074 AETC Y N 0.0064 AETC Y N 0.0071 AETC Y N 0.0073 AETC Y N
1319 1320 1321 1322 1323 1324 1325 1326	16.000 16.000 17.000 17.000 17.000 17.000 17.000	92.000 92.000 92.000 92.000 92.000 92.000 92.000	0.0000 5.0000 247.00 777.00 887.00 1065.0 764.00 651.00	397.00 300.00 36.000 0.0000 0.0000 0.0000 0.0000	2388.0 2388.0 4631.0 4631.0 4631.0 4631.0 4631.0	0.0094 AETC Y N 0.0067 AETC Y N 0.0132 AETC N N 0.0216 AETC N N 0.0237 AETC N N 0.0245 AETC N N 0.0211 AETC N N 0.0195 AETC N N
1327 1328 1329 1330 1331 1332 1333 1334	17.000 17.000 17.000 17.000 17.000 17.000 18.000	92.000 92.000 92.000 92.000 92.000 92.000 92.000	378.00 138.00 21.000 0.0000 9.0000 98.000 110.00 482.00	0.0000 91.000 223.00 303.00 182.00 93.000 90.000 12.000	4631.0 4631.0 4631.0 4631.0 4631.0 4631.0 1454.0	0.0167 AETC N N 0.0129 AETC N N 0.0118 AETC N N 0.0131 AETC N N 0.0142 AETC N N 0.0132 AETC N N 0.0069 AETC Y N 0.0087 AETC Y N

1335	18.000	92.000	303.00	52.000	1454.0	0.0153 AETC Y N
1336	18.000	92.000	681.00	0.0000	1454.0	0.0184 AETC Y N
1337	18.000	92.000	413.00	0.0000	1454.0	0.0127 AETC Y N
1338	18.000	92.000	332.00	7.0000	1454.0	0.0114 AETC Y N
1339	18.000	92.000	70.000	153.00	1454.0	0.0089 AETC Y N
1340	18.000	92.000	27.000	140.00	1454.0	0.0078 AETC Y N
1341	18.000	92.000	0.0000	301.00	1454.0	0.0085 AETC Y N
1342	18.000	92.000	0.0000	479.00	1454.0	0.0079 AETC Y N
1343	18.000	92.000	0.0000	352.00	1454.0	0.0077 AETC Y N
1344	18.000	92.000	6.0000	257.00	1454.0	0.0095 AETC Y N
1345	19.000	92.000	90.000	123.00	1774.0	0.0081 AETC N N
1346	19.000	92.000	443.00	0.0000	1774.0	0.0125 AETC N N
1347	19.000	92.000	482.00	2.0000	1774.0	0.0132 AETC N N
1348	19.000	92.000	592.00	0.0000	1774.0	0.0129 AETC N N
1349	19.000	92.000	344.00	0.0000	1774.0	0.0122 AETC N N 0.0102 AETC N N
1350	19.000	92.000	199.00	3.0000	1774.0	
1351	19.000	92.000	88.000	86.000	1774.0	0.0084 AETC N N
1352	19.000	92.000	20.000	195.00	1774.0	0.0082 AETC N N
1353	19.000	92.000	0.0000	432.00	1774.0	0.0086 AETC N N
1354	19.000	92.000	0.0000	567.00	1774.0	0.0089 AETC N N
1355	19.000	92.000		450.00	1774.0	0.0066 AETC N N
1356	19.000	92.000	0.0000	386.00	1774.0	0.0106 AETC N N
1357	20.000	92.000	69.000	119.00	1717.0	0.0092 AETC N N
1358	20.000	92.000	387.00	15.000	1717.0	0.0122 AETC N N
1359 1360 1361	20.000	92.000 92.000 92.000	447.00 588.00 324.00	18.000 0.0000 5.0000	1717.0 1717.0 1717.0	0.0139 AETC N N 0.0154 AETC N N
1362 1363	20.000 20.000 20.000	92.000 92.000	260.00 126.00	10.000 60.000	1717.0 1717.0	0.0119 AETC N N 0.0095 AETC N N
1364	20.000	92.000	25.000	169.00	1717.0	0.0072 AETC N N
1365	20.000	92.000	0.0000	351.00	1717.0	0.0087 AETC N N
1366	20.000	92.000	0.0000	517.00	1717.0	0.0114 AETC N N
1367	20.000	92.000	0.0000	422.00	1717.0	0.0078 AETC N N 0.0088 AETC N N
1368	20.000	92.000	1.0000	354.00	1717.0	
1369	21.000	92.000	25.000	214.00	6943.0	0.0105 AETC N N
1370	21.000	92.000	306.00	24.000	6943.0	0.0117 AETC N N
1371	21.000	92.000	299.00	10.000	6943.0	0.0106 AETC N N
1372	21.000	92.000	436.00	0.0000	6943.0	0.0124 AETC N N
1373	21.000	92.000	217.00	3.0000	6943.0	0.0104 AETC N N
1374	21.000	92.000	159.00	24.000	6943.0	0.0104 AETC N N
1375	21.000	92.000	44.000	131.00	6943.0	0.0096 AETC N N
1376	21.000	92.000	9.0000	272.00	6943.0	0.0097 AETC N N
1377	21.000	92.000	0.0000	447.00	6943.0	0.0095 AETC N N
1378	21.000	92.000	0.0000	556.00	6943.0	0.0105 AETC N N
1379	21.000	92.000	0.0000	464.00	6943.0	0.0103 AETC N N
1380	21.000	92.000	0.0000	421.00	6943.0	0.0103 AETC N N
1381	22.000	92.000	29.000	292.00	10322.0	0.0040 AETC N N
1382	22.000	92.000	269.00	50.000	10322.0	0.0037 AETC N N
1383	22.000	92.000	309.00	16.000	10322.0	0.0051 AETC N N
1384	22.000	92.000	449.00	0.0000	10322.0	0.0053 AETC N N
1385	22.000	92.000	201.00	12.000	10322.0	0.0040 AETC N N
1386	22.000	92.000	108.00	39.000	10322.0	0.0034 AETC N N
1387	22.000	92.000	37.000	123.00	10322.0	0.0032 AETC N N
1388	22.000	92.000	4.0000	252.00	10322.0	0.0043 AETC N N 0.0048 AETC N N
1389	22.000	92.000	0.0000	501.00	10322.0	
1390	22.000	92.000	0.0000	592.00	10322.0	0.0050 AETC N N
1391	22.000	92.000	0.0000	504.00	10322.0	0.0045 AETC N N
1392	22.000	92.000	0.0000	463.00	10322.0	0.0045 AETC N N
1393	23.000	92.000	22.000	319.00	1441.0	0.0086 AETC Y N
1394	23.000	92.000	164.00	41.000	1441.0	0.0094 AETC Y N
1395	23.000	92.000	245.00	19.000	1441.0	0.0096 AETC Y N
1396	23.000	92.000	352.00	0.0000	1441.0	0.0116 AETC Y N
1397	23.000	92.000	151.00	17.000	1441.0	0.0091 AETC Y N
1398 1399 1400	23.000 23.000 23.000	92.000 92.000 92.000	52.000 27.000 0.0000	106.00 209.00 350.00	1441.0 1441.0 1441.0	0.0079 AETC Y N 0.0078 AETC Y N
1401	23.000	92.000	0.0000	551.00	1441.0	0.0085 AETC Y N
1402	23.000	92.000	0.0000	564.00	1441.0	0.0094 AETC Y N
1403	23.000	92.000	0.0000	517.00	1441.0	0.0083 AETC Y N
1404 1405	23.000 24.000	92.000	0.0000 475.00	458.00 8.0000	1441.0 5152.0	0.0082 AETC Y N 0.0129 AETC N N

1413	1406 1407 1408 1409 1410 1411 1412	24.000 24.000 24.000 24.000 24.000 24.000 24.000	92.000 92.000 92.000 92.000 92.000 92.000	940.00 1045.0 1097.0 769.00 720.00 401.00 201.00	0.0000 0.0000 0.0000 0.0000 0.0000 7.0000 19.000	5152.0 5152.0 5152.0 5152.0 5152.0 5152.0 5152.0	0.0188 AETC N N 0.0203 AETC N N 0.0215 AETC N N 0.0168 AETC N N 0.0156 AETC N N 0.0117 AETC N N 0.0067 AETC N N
1419	1414	24.000	92.000	18.000	153.00	5152.0	0.0064 AETC N N
	1415	24.000	92.000	50.000	132.00	5152.0	0.0063 AETC N N
	1416	24.000	92.000	78.000	61.000	5152.0	0.0060 AETC N N
1423 25.000 92.000 18.000 114.00 3446.0 0.0084 AETC Y N N N 1425 25.000 92.000 0.0000 637.00 3446.0 0.0088 AETC Y N N 1425 25.000 92.000 0.0000 637.00 3446.0 0.0088 AETC Y N N 1426 25.000 92.000 0.0000 805.00 3446.0 0.0094 AETC Y N N 1428 25.000 92.000 0.0000 805.00 3446.0 0.0096 AETC Y N N 1428 25.000 92.000 63.000 119.00 3846.0 0.0090 AETC Y N N 1430 26.000 92.000 387.00 150.000 3840.0 0.0103 AETC N N N 1431 26.000 92.000 588.00 0.0000 3840.0 0.0146 AETC N N N 1432 26.000 92.000 588.00 0.0000 3840.0 0.0174 AETC N N N 1434 26.000 92.000 260.00 100.000 3840.0 0.0191 AETC N N N 1434 26.000 92.000 260.00 100.000 3840.0 0.0144 AETC N N N 1434 26.000 92.000 260.00 100.000 3840.0 0.0144 AETC N N N 1434 26.000 92.000 260.00 100.000 3840.0 0.0144 AETC N N N 1436 26.000 92.000 250.000 169.00 3840.0 0.0144 AETC N N N 1436 26.000 92.000 25.000 169.00 3840.0 0.0124 AETC N N N 1438 26.000 92.000 0.0000 351.00 3840.0 0.0124 AETC N N N 1438 26.000 92.000 0.0000 351.00 3840.0 0.0124 AETC N N N 1438 26.000 92.000 0.0000 351.00 3840.0 0.0135 AETC N N N 1438 26.000 92.000 0.0000 351.00 3840.0 0.0124 AETC N N N 1438 26.000 92.000 0.0000 351.00 3840.0 0.0135 AETC N N N 1439 26.000 92.000 0.0000 351.00 3840.0 0.0135 AETC N N N 1434 27.000 92.000 34.000 3492.0 0.0114 AETC Y N N 1440 27.000 92.000 34.000 3840.0 0.0135 AETC N N N 1444 27.000 92.000 34.000 3492.0 0.0114 AETC Y N N 1444 27.000 92.000 314.000 3492.0 0.0133 AETC Y N N 1445 27.000 92.000 314.000 3492.0 0.0014 AETC Y N N 1445 27.000 92.000 314.000 3492.0 0.0014 AETC Y N N 1445 27.000 92.000 314.000 3492.0 0.0014 AETC Y N N 1446 27.000 92.000 314.000 3492.0 0.0014 AETC Y N N 1446 27.000	1419	25.000	92.000	296.00	0.0000	3446.0	0.0094 AETC Y N
	1420	25.000	92.000	353.00	0.0000	3446.0	0.0104 AETC Y N
	1421	25.000	92.000	152.00	2.0000	3446.0	0.0097 AETC Y N
1428	1423	25.000	92.000	18.000	114.00	3446.0	0.0084 AETC Y N
	1424	25.000	92.000	0.0000	510.00	3446.0	0.0088 AETC Y N
	1425	25.000	92.000	0.0000	637.00	3446.0	0.0088 AETC Y N
	1426	25.000	92.000	0.0000	789.00	3446.0	0.0094 AETC Y N
1433 26.000 92.000 324.00 5.0000 3840.0 0.0144 AETC N N 1434 26.000 92.000 260.00 10.000 3840.0 0.0144 AETC N N 1436 26.000 92.000 25.000 169.00 3840.0 0.0104 AETC N N 1437 26.000 92.000 0.0000 351.00 3840.0 0.0102 AETC N N 1438 26.000 92.000 0.0000 517.00 3840.0 0.0123 AETC N N 1439 26.000 92.000 0.0000 517.00 3840.0 0.0124 AETC N N 1441 27.000 92.000 1.0000 354.00 3840.0 0.0112 AETC N N 1442 27.000 92.000 34.000 293.00 3492.0 0.0011 AETC Y N 1443 27.000 92.000 34.000 24.000 3492.0 0.0112 AETC Y N 1443 27.000 92.000 314.00 24.000 3492.0 0.013 AETC Y N 1445 27.000 92.000 192.00	1428 1429 1430	25.000 26.000 26.000	92.000 92.000 92.000	18.000 69.000 387.00 447.00	114.00 119.00 15.000 18.000	3446.0 3840.0 3840.0 3840.0	0.0090 AETC Y N 0.0103 AETC N N 0.0146 AETC N N 0.0172 AETC N N
1437 26.000 92.000 0.0000 351.00 3840.0 0.0123 AETC N N 1438 26.000 92.000 0.0000 517.00 3840.0 0.0135 AETC N N 1440 26.000 92.000 1.0000 354.00 3840.0 0.0124 AETC N N 1441 27.000 92.000 1.0000 354.00 3840.0 0.0121 AETC N N 1442 27.000 92.000 34.000 293.00 3492.0 0.0011 AETC Y N 1443 27.000 92.000 314.00 24.000 3492.0 0.0113 AETC Y N 1444 27.000 92.000 314.00 24.000 3492.0 0.0113 AETC Y N 1444 27.000 92.000 443.00 0.0000 3492.0 0.01152 AETC Y N 1445 27.000 92.000 42.000 3492.0 0.0104 AETC Y N 1447 27.000 92.000 42.000 33.00 3492.0 0.0104 AETC Y N 1448 27.000 92.000 0.0000 566.00 3492.0 <td>1433</td> <td>26.000</td> <td>92.000</td> <td>324.00</td> <td>5.0000</td> <td>3840.0</td> <td>0.0149 AETC N N</td>	1433	26.000	92.000	324.00	5.0000	3840.0	0.0149 AETC N N
	1434	26.000	92.000	260.00	10.000	3840.0	0.0144 AETC N N
	1435	26.000	92.000	126.00	60.000	3840.0	0.0120 AETC N N
1442 27.000 92.000 278.00 54.000 3492.0 0.0114 AETC Y N 1443 27.000 92.000 314.00 24.000 3492.0 0.0133 AETC Y N 1444 27.000 92.000 443.00 0.0000 3492.0 0.0152 AETC Y N 1445 27.000 92.000 192.00 24.000 3492.0 0.0104 AETC Y N 1446 27.000 92.000 111.00 49.000 3492.0 0.0104 AETC Y N 1447 27.000 92.000 42.000 3492.0 0.0104 AETC Y N 1448 27.000 92.000 42.000 3492.0 0.0104 AETC Y N 1448 27.000 92.000 42.000 3492.0 0.0084 AETC Y N 1449 27.000 92.000 0.0000 513.00 3492.0 0.0083 AETC Y N 1455 27.000 92.000 0.0000 513.00 3492.0 0.0088 AETC Y N 1455 27.000 92.000 0.0000 513.00 3492.0 0.0088 AETC Y N 1455 28.000 92.000 0.0000 518.00 3492.0 0.0087 AETC Y N	1438 1439 1440	26.000 26.000 26.000	92.000 92.000 92.000	0.0000 0.0000 0.0000 1.0000	517.00 422.00 354.00	3840.0 3840.0 3840.0	0.0135 AETC N N 0.0124 AETC N N 0.0111 AETC N N
1447 27.000 92.000 42.000 130.00 3492.0 0.0084 AETC Y N 1448 27.000 92.000 9.0000 266.00 3492.0 0.0083 AETC Y N 149 27.000 92.000 0.0000 513.00 3492.0 0.0089 AETC Y N 1450 27.000 92.000 0.0000 605.00 3492.0 0.0098 AETC Y N 1451 27.000 92.000 0.0000 518.00 3492.0 0.0098 AETC Y N 1452 27.000 92.000 0.0000 483.00 3492.0 0.0098 AETC Y N 1452 27.000 92.000 0.0000 483.00 3492.0 0.0098 AETC Y N 1453 28.000 92.000 0.0000 483.00 3492.0 0.0098 AETC Y N 1454 28.000 92.000 144.00 86.000 1375.0 0.0118 AETC Y N 1455 28.000 92.000 629.00 0.0000 1375.0 0.01207 AETC Y N 1456 28.000 92.000 736.00 0.0000 1375.0 0.0223 AETC Y N 1458 28.000 92.000 436.00 0.0000 1375.0 0.0172 AETC Y N 1458 28.000 92.000 278.00 <	1442	27.000	92.000	278.00	54.000	3492.0	0.0114 AETC Y N
	1443	27.000	92.000	314.00	24.000	3492.0	0.0133 AETC Y N
	1444	27.000	92.000	443.00	0.0000	3492.0	0.0152 AETC Y N
	1445	27.000	92.000	192.00	24.000	3492.0	0.0104 AETC Y N
1452 27.000 92.000 0.0000 483.00 3492.0 0.0087 AETC Y N 1453 28.000 92.000 144.00 86.000 1375.0 0.0118 AETC Y N 1454 28.000 92.000 537.00 0.0000 1375.0 0.0196 AETC Y N 1455 28.000 92.000 629.00 0.0000 1375.0 0.0207 AETC Y N 1456 28.000 92.000 736.00 0.0000 1375.0 0.0207 AETC Y N 1457 28.000 92.000 736.00 0.0000 1375.0 0.0207 AETC Y N 1458 28.000 92.000 436.00 0.0000 1375.0 0.0172 AETC Y N 1458 28.000 92.000 278.00 0.0000 1375.0 0.0172 AETC Y N 1459 28.000 92.000 101.00 93.000 1375.0 0.0151 AETC Y N 1465 28.000 92.000 101.00 93.000 1375.0 0.0110 AETC Y N 1466 28.000 92.000 0.0000 368.00 1375.0 0.0084 AETC Y N 1462 28.000 92.000 0.0000 515.	1447	27.000	92.000	42.000	130.00	3492.0	0.0084 AETC Y N
	1448	27.000	92.000	9.0000	266.00	3492.0	0.0083 AETC Y N
	1449	27.000	92.000	0.0000	513.00	3492.0	0.0089 AETC Y N
	1450	27.000	92.000	0.0000	605.00	3492.0	0.0098 AETC Y N
1457 28.000 92.000 436.00 0.0000 1375.0 0.0172 AETC Y N 1458 28.000 92.000 278.00 0.0000 1375.0 0.0151 AETC Y N 1459 28.000 92.000 101.00 93.000 1375.0 0.0110 AETC Y N 1460 28.000 92.000 29.000 161.00 1375.0 0.0092 AETC Y N 1461 28.000 92.000 0.0000 368.00 1375.0 0.0084 AETC Y N 1462 28.000 92.000 0.0000 515.00 1375.0 0.0094 AETC Y N 1463 28.000 92.000 0.0000 515.00 1375.0 0.0094 AETC Y N 1464 28.000 92.000 0.0000 515.00 1375.0 0.0094 AETC Y N 1464 28.000 92.000 0.0000 515.00 1375.0 0.0094 AETC Y N 1464 28.000 92.000 3.0000 278.00 1375.0 0.0079 AETC Y N 1465 29.000 92.000 3.0000 5703.0 0.0072 AETC N N 1466 29.000 92.000 510.00 3.0000 5703	1452	27.000	92.000	0.0000	483.00	3492.0	0.0087 AETC Y N
	1453	28.000	92.000	144.00	86.000	1375.0	0.0118 AETC Y N
	1454	28.000	92.000	537.00	0.0000	1375.0	0.0196 AETC Y N
	1455	28.000	92.000	629.00	0.0000	1375.0	0.0207 AETC Y N
1462 28.000 92.000 0.0000 515.00 1375.0 0.0094 AETC Y N 1463 28.000 92.000 0.0000 403.00 1375.0 0.0092 AETC Y N 1464 28.000 92.000 3.0000 278.00 1375.0 0.0079 AETC Y N 1465 29.000 92.000 121.00 134.00 5703.0 0.0072 AETC N N 1466 29.000 92.000 510.00 3.0000 5703.0 0.0105 AETC N N 1467 29.000 92.000 569.00 1.0000 5703.0 0.0103 AETC N N 1468 29.000 92.000 682.00 0.0000 5703.0 0.0117 AETC N N 1469 29.000 92.000 426.00 0.0000 5703.0 0.0092 AETC N N 1470 29.000 92.000 299.00 7.0000 5703.0 0.0059 AETC N N 1471 29.000 92.000 105.00 68.000 5703.0 0.0064 AETC N N 1472 29.000 92.000 37.000 174.00 5703.0 0.0053 AETC N N 1473 29.000 92.000 0.0000 5703.0 0.0058 AETC N N 1474 29.000 92.000 0.0000	1457	28.000	92.000	436.00	0.0000	1375.0	0.0172 AETC Y N
	1458	28.000	92.000	278.00	0.0000	1375.0	0.0151 AETC Y N
	1459	28.000	92.000	101.00	93.000	1375.0	0.0110 AETC Y N
	1460	28.000	92.000	29.000	161.00	1375.0	0.0092 AETC Y N
1467 29.000 92.000 569.00 1.0000 5703.0 0.0103 AETC N N 1468 29.000 92.000 682.00 0.0000 5703.0 0.0117 AETC N N 1469 29.000 92.000 426.00 0.0000 5703.0 0.0092 AETC N N 1470 29.000 92.000 299.00 7.0000 5703.0 0.0059 AETC N N 1471 29.000 92.000 105.00 68.000 5703.0 0.0064 AETC N N 1472 29.000 92.000 37.000 174.00 5703.0 0.0053 AETC N N 1473 29.000 92.000 0.0000 405.00 5703.0 0.0058 AETC N N 1474 29.000 92.000 0.0000 569.00 5703.0 0.0058 AETC N N	1462	28.000	92.000	0.0000	515.00	1375.0	0.0094 AETC Y N
	1463	28.000	92.000	0.0000	403.00	1375.0	0.0092 AETC Y N
	1464	28.000	92.000	3.0000	278.00	1375.0	0.0079 AETC Y N
	1465	29.000	92.000	121.00	134.00	5703.0	0.0072 AETC N N
1472 29.000 92.000 37.000 174.00 5703.0 0.0053 AETC N N 1473 29.000 92.000 0.0000 405.00 5703.0 0.0058 AETC N N 1474 29.000 92.000 0.0000 569.00 5703.0 0.0058 AETC N N	1467 1468 1469	29.000 29.000 29.000	92.000 92.000 92.000	569.00 682.00 426.00 299.00	1.0000 0.0000 0.0000	5703.0 5703.0 5703.0 5703.0	0.0103 AETC N N 0.0117 AETC N N 0.0092 AETC N N 0.0059 AETC N N
1475 29.000 92.000 0.0000 435.00 5703.0 0.0059 AETC N N 1476 29.000 92.000 2.0000 319.00 5703.0 0.0050 AETC N N	1472 1473 1474 1475	29.000 29.000 29.000 29.000	92.000 92.000 92.000 92.000	37.000 0.0000 0.0000 0.0000	174.00 405.00 569.00 435.00	5703.0 5703.0 5703.0 5703.0	0.0053 AETC N N 0.0058 AETC N N 0.0058 AETC N N 0.0059 AETC N N

1477 1478 1479 1480 1481 1482 1483 1484 1485 1486 1487 1488 1489 1490 1491 1492 1493 1496 1497 1498 1499 1500 1500	30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000	92.000 92.000	22.000 271.00 283.00 425.00 239.00 191.00 85.000 22.000 0.0000 0.0000 0.0000 203.00 701.00 683.00 733.00 525.00 405.00 199.00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	168.00 32.000 23.000 0.0000 6.0000 11.000 68.000 185.00 405.00 532.00 428.00 76.000 0.0000 0.0000 0.0000 0.0000 0.0000 22.000 88.000 240.00 476.00 282.00 218.00 292.00	3505.0 3505.0 3505.0 3505.0 3505.0 3505.0 3505.0 3505.0 3505.0 3505.0 1088.0 1088.0 1088.0 1088.0 1088.0 1088.0 1088.0 1088.0	0.0081 AETC Y N 0.0096 AETC Y N 0.0102 AETC Y N 0.0119 AETC Y N 0.0119 AETC Y N 0.0092 AETC Y N 0.0082 AETC Y N 0.0083 AETC Y N 0.0083 AETC Y N 0.0096 AETC Y N 0.0096 AETC Y N 0.0097 AETC Y N 0.0091 AETC Y N 0.0170 AETC Y N 0.0170 AETC Y N 0.0170 AETC Y N 0.0173 AETC Y N 0.0131 AETC Y N 0.0137 AETC Y N 0.0095 AETC Y N 0.0077 AETC Y N 0.0078 AETC Y N 0.0078 AETC Y N 0.0078 AETC N N 0.00338 AETC N N
1526 1527 1528 1529 1530	32.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000 16.000 16.000 16.000 16.000 16.000 16.000 16.000 16.000 16.000 17.000 17.000 17.000 17.000	92.000 92.000 92.000 92.000 92.000 92.000 92.000 92.000 92.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	269.00 309.00 449.00 201.00 108.00 37.000 4.0000 0.0000 0.0000 79.000 524.00 719.00 855.00 653.00 424.00 207.00 40.000 0.0000 0.0000 0.0000 20.000 270.00 656.00 988.00 1082.0 1033.0 837.00	50.000 16.000 0.0000 12.000 39.000 123.00 252.00 501.00 592.00 65.000 225.00 65.000 11.000 0.0000 0.0000 0.0000 29.000 164.00 443.00 649.00 520.00 237.00 13.000 0.0000 0.0000 0.0000 0.0000 0.0000	1704.0 1704.0 1704.0 1704.0 1704.0 1704.0 1704.0 1704.0 1704.0 2146.0	0.0330 AETC N N 0.0350 AETC N N 0.0370 AETC N N 0.0370 AETC N N 0.0353 AETC N N 0.0353 AETC N N 0.0339 AETC N N 0.0343 AETC N N 0.0349 AETC N N 0.0357 AETC N N 0.0357 AETC N N 0.0357 AETC N N 0.0357 AETC N N 0.0160 AETC Y N 0.0160 AETC Y N 0.0187 AETC Y N 0.0187 AETC Y N 0.0195 AETC Y N 0.0170 AETC Y N 0.0170 AETC Y N 0.0170 AETC Y N 0.0170 AETC Y N 0.0073 AETC Y N 0.0073 AETC Y N 0.0074 AETC Y N 0.0075 AETC Y N 0.0075 AETC Y N 0.0077 AETC N N 0.0077 AETC N N 0.0120 AETC N N 0.0120 AETC N N 0.0072 AETC N N 0.0127 AETC N N 0.0120 AETC N N 0.0120 AETC N N 0.0120 AETC N N 0.0127 AETC N N 0.0120 AETC N N 0.0120 AETC N N 0.0127 AETC N N 0.0120 AETC N N 0.0120 AETC N N 0.0120 AETC N N
1531 1532 1533 1534 1536 1537 1538 1539 1540 1541 1542 1543 1544 1545 1546 1547	17.000 17.000 17.000 17.000 17.000 17.000 18.000 18.000 18.000 18.000 18.000 18.000 18.000 18.000 18.000 18.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	433.00 64.000 30.000 0.0000 11.000 11.000 413.00 636.00 605.00 579.00 450.00 205.00 19.000 0.0000	0.0000 0.0000 286.00 408.00 376.00 127.00 19.000 0.0000 0.0000 0.0000 3.0000 21.000 152.00 301.00 488.00	4631.0 4631.0 4631.0 4631.0 4631.0 1467.0 1467.0 1467.0 1467.0 1467.0 1467.0 1467.0 1467.0 1467.0	0.0172 AETC N N 0.0083 AETC N N 0.0061 AETC N N 0.0058 AETC N N 0.0053 AETC N N 0.0050 AETC N N 0.0050 AETC Y N 0.0105 AETC Y N 0.0162 AETC Y N 0.0128 AETC Y N 0.0169 AETC Y N 0.0169 AETC Y N 0.0169 AETC Y N 0.0082 AETC Y N 0.0082 AETC Y N 0.0090 AETC Y N 0.0090 AETC Y N 0.0090 AETC Y N

1577	1578	1548 1549 1550 1552 1553 1554 1555 1556 1557 1560 1562 1563 1564 1565 1566 1567 1568 1569 1571 1572 1573 1574 1576 1577	18.000 19.000 19.000 19.000 19.000 19.000 19.000 19.000 19.000 20.000 21.000 21.000 21.000 21.000	93.000 93.000	20.000 27.000 370.00 473.00 619.00 436.00 273.00 89.000 4.0000 0.0000 7.0000 58.000 323.00 474.00 421.00 453.00 339.00 141.00 8.0000 0.0000 0.0000 0.0000 2.0000 7.0000 2.0000 7.0000 243.00 234.00 234.00	350.00 134.00 16.000 3.0000 0.0000 28.000 131.00 239.00 494.00 653.00 608.00 283.00 42.000 8.0000 3.0000 0.0000 2.0000 15.000 468.00 615.00 468.00 615.00 548.00 377.00 127.00 22.0000 5.0000	1467.0 1802.0 1802.0 1802.0 1802.0 1802.0 1802.0 1802.0 1802.0 1802.0 1802.0 1802.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0 1627.0	0.0094 AETC Y N 0.0078 AETC N N 0.0100 AETC N N 0.0130 AETC N N 0.0142 AETC N N 0.0145 AETC N N 0.0110 AETC N N 0.0110 AETC N N 0.0069 AETC N N 0.0085 AETC N N 0.0086 AETC N N 0.0094 AETC N N 0.0094 AETC N N 0.0094 AETC N N 0.0094 AETC N N 0.0110 AETC N N 0.0110 AETC N N 0.0110 AETC N N 0.0113 AETC N N 0.0119 AETC N N 0.0114 AETC N N 0.0115 AETC N N 0.0116 AETC N N 0.0117 AETC N N 0.0118 AETC N N 0.0118 AETC N N 0.0110 AETC N N 0.0110 AETC N N 0.0111 AETC N N 0.0111 AETC N N 0.0112 AETC N N 0.0113 AETC N N 0.0114 AETC N N 0.0115 AETC N N 0.0115 AETC N N 0.0117 AETC N N 0.0118 AETC N N 0.0119 AETC N N
1584	1584	1578 1579 1580 1581	21.000 21.000 21.000 21.000	93.000 93.000 93.000 93.000	253.00 82.000 0.0000 0.0000	16.000 60.000 251.00 488.00	6983.0 6983.0 6983.0 6983.0	0.0108 AETC N N 0.0094 AETC N N 0.0098 AETC N N 0.0101 AETC N N
1589 22.000 93.000 270.00 9.0000 8507.0 0.0045 AETC N N 1590 22.000 93.000 158.00 34.000 8507.0 0.0050 AETC N N 1591 22.000 93.000 43.000 98.000 8507.0 0.0045 AETC N N 1592 22.000 93.000 0.0000 244.00 8507.0 0.0058 AETC N N 1593 22.000 93.000 0.0000 574.00 8507.0 0.0058 AETC N N 1594 22.000 93.000 0.0000 574.00 8507.0 0.0062 AETC N N 1595 22.000 93.000 0.0000 622.00 8507.0 0.0062 AETC N N 1596 22.000 93.000 0.0000 471.00 8507.0 0.0062 AETC N N 1597 23.000 93.000 0.0000 471.00 8507.0 0.0062 AETC N N 1598 23.000 93.000 272.00 23.000 1498.0 0.0076 AETC Y N 1600 23.000 93.000 338.00	1589	1584 1585 1586 1587	21.000 22.000 22.000 22.000	93.000 93.000 93.000 93.000	0.0000 1.0000 275.00 307.00	429.00 225.00 29.000 24.000	6983.0 8507.0 8507.0 8507.0	0.0110 AETC N N 0.0046 AETC N N 0.0045 AETC N N 0.0070 AETC N N
1595 22.000 93.000 0.0000 622.00 8507.0 0.0062 AETC N N N 1596 22.000 93.000 0.0000 471.00 8507.0 0.0054 AETC N N N 1597 23.000 93.000 0.0000 228.00 1498.0 0.0076 AETC Y N N 1598 23.000 93.000 272.00 23.000 1498.0 0.0083 AETC Y N N 1599 23.000 93.000 338.00 2.0000 1498.0 0.0100 AETC Y N N 1600 23.000 93.000 448.00 0.0000 1498.0 0.0099 AETC Y N N 1601 23.000 93.000 266.00 1.0000 1498.0 0.0086 AETC Y N N 1602 23.000 93.000 132.00 61.000 1498.0 0.0086 AETC Y N N 1603 23.000 93.000 164.00 1498.0 0.0075 AETC Y N N 1604 23.000 93.000 0.0000 489.00 1498.0	1595 22.000 93.000 0.0000 622.00 8507.0 0.0062 AETC N N N 1596 22.000 93.000 0.0000 471.00 8507.0 0.0054 AETC N N N 1597 23.000 93.000 0.0000 228.00 1498.0 0.0076 AETC Y N N 1598 23.000 93.000 272.00 23.000 1498.0 0.0083 AETC Y N N 1599 23.000 93.000 338.00 2.0000 1498.0 0.0100 AETC Y N N 1600 23.000 93.000 448.00 0.0000 1498.0 0.0099 AETC Y N N 1601 23.000 93.000 266.00 1.0000 1498.0 0.0086 AETC Y N N 1602 23.000 93.000 132.00 61.000 1498.0 0.0075 AETC Y N N 1603 23.000 93.000 12.000 164.00 1498.0 0.0075 AETC Y N N 1604 23.000 93.000 0.0000 489.00	1589 1590 1591 1592	22.000 22.000 22.000 22.000	93.000 93.000 93.000 93.000	270.00 158.00 43.000 0.0000	9.0000 34.000 98.000 244.00	8507.0 8507.0 8507.0 8507.0	0.0045 AETC N N 0.0050 AETC N N 0.0045 AETC N N 0.0052 AETC N N
1600 23.000 93.000 448.00 0.0000 1498.0 0.0099 AETC Y N 1601 23.000 93.000 266.00 1.0000 1498.0 0.0086 AETC Y N 1602 23.000 93.000 132.00 61.000 1498.0 0.0086 AETC Y N 1603 23.000 93.000 12.000 164.00 1498.0 0.0075 AETC Y N 1604 23.000 93.000 0.0000 351.00 1498.0 0.0077 AETC Y N 1605 23.000 93.000 0.0000 489.00 1498.0 0.0089 AETC Y N 1606 23.000 93.000 0.0000 645.00 1498.0 0.0091 AETC Y N 1608 23.000 93.000 0.0000 676.00 1498.0 0.0094 AETC Y N 1608 23.000 93.000 0.0000 432.00 1498.0 0.0076 AETC Y N 1608 23.000 93.000 0.0000 432.00 1498.0 0.0076 AETC Y N 1608 24.000 93.000 0.0000 5152.0 0.0137 AETC N N	1600 23.000 93.000 448.00 0.0000 1498.0 0.0099 AETC Y N 1601 23.000 93.000 266.00 1.0000 1498.0 0.0086 AETC Y N 1602 23.000 93.000 132.00 61.000 1498.0 0.0086 AETC Y N 1603 23.000 93.000 12.000 164.00 1498.0 0.0075 AETC Y N 1604 23.000 93.000 0.0000 351.00 1498.0 0.0077 AETC Y N 1605 23.000 93.000 0.0000 489.00 1498.0 0.0089 AETC Y N 1606 23.000 93.000 0.0000 645.00 1498.0 0.0091 AETC Y N 1607 23.000 93.000 0.0000 676.00 1498.0 0.0094 AETC Y N 1608 23.000 93.000 0.0000 676.00 1498.0 0.0094 AETC Y N 1609 24.000 93.000 0.0000 432.00 1498.0 0.0076 AETC Y N 1610 24.000 93.000 365.00 3.0000 5152.0 0.0137 AETC N N 1611 24.000 93.000 1198.0 0.0000 5152.0 0.0227 AETC N N 1612 24.000 93.000 1154.0 <	1595 1596 1597 1598	22.000 22.000 23.000 23.000	93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 272.00	622.00 471.00 228.00 23.000	8507.0 8507.0 1498.0 1498.0	0.0062 AETC N N 0.0054 AETC N N 0.0076 AETC Y N 0.0083 AETC Y N
1605 23.000 93.000 0.0000 489.00 1498.0 0.0089 AETC Y N 1606 1606 23.000 93.000 0.0000 645.00 1498.0 0.0091 AETC Y N 1406.0 1607 23.000 93.000 0.0000 676.00 1498.0 0.0094 AETC Y N 1406.0 1608 23.000 93.000 0.0000 432.00 1498.0 0.0076 AETC Y N 1609 24.000 93.000 365.00 3.0000 5152.0 0.0137 AETC N	1605 23.000 93.000 0.0000 489.00 1498.0 0.0089 AETC Y N 1606 23.000 93.000 0.0000 645.00 1498.0 0.0091 AETC Y N 1607 23.000 93.000 0.0000 676.00 1498.0 0.0094 AETC Y N 1608 23.000 93.000 0.0000 432.00 1498.0 0.0076 AETC Y N 1609 24.000 93.000 365.00 3.0000 5152.0 0.0137 AETC N N 1610 24.000 93.000 957.00 0.0000 5152.0 0.0227 AETC N N 1611 24.000 93.000 1198.0 0.0000 5152.0 0.0260 AETC N N 1612 24.000 93.000 1154.0 0.0000 5152.0 0.0245 AETC N N 1613 24.000 93.000 1030.0 0.0000 5152.0 0.0227 AETC N N 1614 24.000 93.000 730.00 0.0000 5152.0 0.0227 AETC N N 1614 24.000 93.000 1030.0 0.0000 5152.0 0.0227 AETC N N 1614 0.0000 10000 10000 10000 10000 10000 10000 100000 100000 100000 100000 <td>1600 1601 1602 1603</td> <td>23.000 23.000 23.000 23.000</td> <td>93.000 93.000 93.000 93.000</td> <td>448.00 266.00 132.00 12.000</td> <td>0.0000 1.0000 61.000 164.00</td> <td>1498.0 1498.0 1498.0 1498.0</td> <td>0.0099 AETC Y N 0.0086 AETC Y N 0.0086 AETC Y N 0.0075 AETC Y N</td>	1600 1601 1602 1603	23.000 23.000 23.000 23.000	93.000 93.000 93.000 93.000	448.00 266.00 132.00 12.000	0.0000 1.0000 61.000 164.00	1498.0 1498.0 1498.0 1498.0	0.0099 AETC Y N 0.0086 AETC Y N 0.0086 AETC Y N 0.0075 AETC Y N
	1611 24.000 93.000 1198.0 0.0000 5152.0 0.0260 AETC N N 1612 24.000 93.000 1154.0 0.0000 5152.0 0.0245 AETC N N 1613 24.000 93.000 1030.0 0.0000 5152.0 0.0227 AETC N N 1614 24.000 93.000 730.00 0.0000 5152.0 0.0199 AETC N N	1605 1606 1607 1608 1609	23.000 23.000 23.000 23.000 24.000	93.000 93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 0.0000 365.00	489.00 645.00 676.00 432.00 3.0000	1498.0 1498.0 1498.0 1498.0 5152.0	0.0089 AETC Y N 0.0091 AETC Y N 0.0094 AETC Y N 0.0076 AETC Y N 0.0137 AETC N N

1620 1621 16223 16223 16225 16226 16226 1633 1633 1633 1633 1633 16	24.000 24.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 26.000 26.000 26.000 26.000 26.000 26.000 26.000 27.000	93.000 93.000	33.000 188.00 0.0000 200.00 410.00 296.00 218.00 92.0000 2.00000 0.0000 0.0000 11.000 0.0000 58.000 474.00 421.00 453.00 339.00 141.00 8.0000 0.0000	149.00 28.000 287.00 2.0000 0.0000 0.0000 0.0000 31.000 188.00 510.00 649.00 8.0000 3.0000 2.0000 16.000 15.000 215.000 468.00 615.000 468.00 615.00 468.00 615.00 468.00 615.00 468.00 615.00 468.00 615.00 62.00 468.00 637.00 662.00 486.00 637.00 662.00 486.00 637.00 662.00 486.00 637.00 662.00 486.00 637.00 662.00 473.00 662.00 486.00 62.000 3.0000 0.0000	5152.0 5152.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3042.0 3931.0 3935.0 1375.0 1375.0 1375.0 1375.0 1375.0 1375.0 1375.0 13850.0 5850.0 5850.0 5850.0 5850.0 5850.0 5850.0 5850.0 5850.0 5850.0 5850.0	0.0075 AETC N N 0.0079 AETC N N 0.0079 AETC Y N 0.0085 AETC Y N 0.0118 AETC Y N 0.0185 AETC Y N 0.0085 AETC Y N 0.0085 AETC Y N 0.0086 AETC Y N 0.0086 AETC Y N 0.0092 AETC Y N 0.0101 AETC Y N 0.0101 AETC Y N 0.0102 AETC Y N 0.0102 AETC Y N 0.0107 AETC N N 0.0107 AETC N N 0.0171 AETC N N 0.0167 AETC N N 0.0124 AETC Y N 0.0125 AETC Y N 0.0126 AETC Y N 0.0127 AETC Y N 0.0128 AETC Y N 0.0088 AETC Y N 0.0096 AETC Y N 0.0096 AETC Y N 0.0097 AETC N N 0.0098 AETC Y N 0.0173 AETC Y N 0.0174 AETC N N 0.0175 AETC N N 0.0175 AETC N N 0.0176 AETC N N 0.0177 AETC N N 0.0178 AETC Y N 0.0178 AETC Y N 0.0179 AETC N N 0.0086 AETC Y N 0.0087 AETC N N 0.0179 AETC N N 0.0087 AETC N N 0.0088 AETC Y N 0.0088 AETC Y N 0.0088 AETC Y N 0.0088 AETC Y N 0.0086 AETC N N 0.0087 AETC N N 0.0086 AETC N N 0.0086 AETC N N 0.0086 AETC N N 0.0087 AETC N N 0.0088 AETC N N
1672 1673 1674 1675 1676 1677	29.000 29.000 29.000 29.000 29.000 29.000	93.000 93.000 93.000 93.000 93.000 93.000	742.00 601.00 392.00 251.00 0.0000	0.0000 0.0000 12.000 38.000 130.00 411.00	5850.0 5850.0 5850.0 5850.0 5850.0 5850.0	0.0123 AETC N N 0.0114 AETC N N 0.0102 AETC N N 0.0067 AETC N N 0.0048 AETC N N 0.0061 AETC N N

1690 1691 1692 1693 1694 1695 1696 1697 1698 16990 1701 1702 1703 1704 1705 1707 1710 1711 1712 1713 1714 1717 1718 1719 1721 1722 1723 1724 1725 1733 1734 1735 1737 1738 1738 1739 1741 1743 1744 1745 1746 1747 1748 1749 1751	30.000 30.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 32.000	93.000 94.000 94.000	0.0000 0.0000 138.00 388.00 540.00 716.00 384.00 200.00 63.000 13.000 0.0000	582.00 579.00 473.00 40.000 0.0000 0.0000 0.0000 0.0000 2.0000 82.000 360.00 618.00 553.00 151.00 225.00 24.000 1.0000 9.0000 34.000 98.000 244.000 471.00 553.00 0.000	3589.0 3589.0 1098.0 1098.0 1098.0 1098.0 1098.0 1098.0 1098.0 1098.0 1098.0 1098.0 1098.0 1704.0 0 1704.0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0077 AETC Y N 0.0103 AETC Y N 0.0890 AETC Y N 0.0087 AETC Y N 0.0148 AETC Y N 0.0194 AETC Y N 0.0194 AETC Y N 0.0155 AETC Y N 0.0111 AETC Y N 0.0072 AETC Y N 0.0081 AETC Y N 0.0084 AETC Y N 0.0084 AETC Y N 0.0084 AETC Y N 0.0035 AETC N N 0.0328 AETC N N 0.0328 AETC N N 0.0347 AETC N N 0.0347 AETC N N 0.0348 AETC N N 0.0348 AETC N N 0.0348 AETC N N 0.0348 AETC N N 0.0347 AETC N N 0.0348 AETC N N 0.0347 AETC N N 0.0345 AETC N N 0.0345 AETC N N 0.0345 AETC N N 0.0355 AETC N N 0.0343 AETC N N 0.0355 AETC N N 0.0355 AETC N N 0.0344 AETC Y N 0.0044 AETC Y N 0.0044 AETC Y N 0.0059 AETC Y N 0.0068 AETC Y N 0.0068 AETC Y N 0.0068 AETC Y N 0.0075 AETC Y N 0.0080 AETC N N 0.0074 AETC N N 0.0081 AETC Y N 0.0082 AETC N N 0.0000 AETC N
1745	18.000	94.000	384.00	6.0000	1434.0	0.0127 AETC Y N
1746	18.000	94.000	200.00	70.000	1434.0	0.0093 AETC Y N
1747	18.000	94.000	63.000	182.00	1434.0	0.0081 AETC Y N
1748	18.000	94.000	13.000	220.00	1434.0	0.0079 AETC Y N
1749	18.000	94.000	0.0000	441.00	1434.0	0.0064 AETC Y N

1761 1762 1763 1764 1765 1766 1767 1768 1776 1771 1772 1773 1777 1778 1777 1778 1779 1780 1781 1782 1783 1784 1785 1787 1788 1789 1790 1791 1792 1793 1794 1795 1796 1797 1798 1799 1800 1801 1802 1803 1814 1815 1816 1817 1818 1818 1818 1818 1818 1818	19.000 19.000 19.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 22.000 23.000	94.000 94.000	0.0000 0.0000 0.0000 4.0000 106.00 347.00 554.00 660.00 321.00 60.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 243.00 392.00 499.00 268.00 156.00 43.000 0.0000 0.	581.00 651.00 599.00 294.00 119.00 34.000 0.0000 18.000 26.000 146.00 227.00 464.00 479.00 489.00 332.00 184.00 39.000 1.0000 7.0000 41.000 175.00 324.00 486.00 495.00 524.00 0.0000 23.000 8.0000 23.000 82.000 139.00 252.00 26.000 27.000 82.000 139.00 27.000 82.000 139.00 27.000 82.000 139.00 27.000 82.000 139.00 297.00 515.00 637.00 592.00 346.00 12.000 7.0000 637.00 592.00 349.00 297.00 515.00 637.00 592.00 349.00 297.00 515.00 637.00 592.00 349.00 297.00 359.00 297.00 359.00 349.00 297.00 359.00 349.00 359.00	1803.0 1803.0 1803.0 1600.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 1660.0 16942.0 6942.0 6942.0 6942.0 6942.0 6942.0 8924.0	0.0091 AETC N N 0.0098 AETC N N 0.0089 AETC N N 0.0093 AETC N N 0.0093 AETC N N 0.0121 AETC N N 0.0121 AETC N N 0.0124 AETC N N 0.0129 AETC N N 0.0116 AETC N N 0.0105 AETC N N 0.0105 AETC N N 0.0127 AETC N N 0.0127 AETC N N 0.0127 AETC N N 0.0112 AETC N N 0.0112 AETC N N 0.0112 AETC N N 0.0113 AETC N N 0.0114 AETC N N 0.0116 AETC N N 0.0116 AETC N N 0.0019 AETC N N 0.0116 AETC N N 0.0116 AETC N N 0.0018 AETC N N 0.0116 AETC N N 0.0116 AETC N N 0.0117 AETC N N 0.0108 AETC N N 0.0108 AETC N N 0.0018 AETC N N 0.0019 AETC N N 0.0009 AETC N N 0.0009 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0052 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0055 AETC N N 0.0056 AETC N N 0.0051 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0057 AETC N N 0.0058 AETC N N 0.0059 AETC N N 0.0051 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0056 AETC N N 0.0057 AETC Y N 0.0060 AETC Y N 0.0060 AETC Y N 0.0060 AETC Y N 0.0051 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0056 AETC N N 0.0057 AETC Y N 0.0060 AETC Y N 0.0060 AETC Y N 0.0060 AETC Y N 0.0051 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0056 AETC N N 0.0051 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0056 AETC N N 0.0051 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0051 AETC N N 0.0051 AETC N N 0.0052 AETC N N 0.0054 AETC N N 0.0055 AETC N N 0.0056 AETC N N 0.0056 AETC N N 0.0051 AETC N
1813 1814 1815 1816 1817 1818 1819	24.000 24.000 24.000 24.000 24.000 24.000 24.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000	538.00 936.00 970.00 985.00 905.00 671.00 545.00	5.0000 0.0000 0.0000 0.0000 0.0000 0.0000	5152.0 5152.0 5152.0 5152.0 5152.0 5152.0 5152.0	0.0145 AETC N N 0.0206 AETC N N N 0.0218 AETC N N N 0.0211 AETC N N N 0.0202 AETC N N 0.0145 AETC N N 0.0123 AETC N N

1832 1833 1834 1835 1836 1837 1838 1839	25.000 25.000 25.000 25.000 25.000 26.000 26.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 0.0000 0.0000 0.0000 106.00 347.00 554.00	397.00 796.00 890.00 942.00 651.00 119.00 34.000	3048.0 3048.0 3048.0 3048.0 3048.0 4075.0 4075.0	0.0100 AETC Y N 0.0106 AETC Y N 0.0103 AETC Y N 0.0114 AETC Y N 0.0098 AETC Y N 0.0103 AETC N N 0.0141 AETC N N 0.0172 AETC N N
1840 1841 1842 1843 1844 1845 1846 1847	26.000 26.000 26.000 26.000 26.000 26.000 26.000 26.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	660.00 332.00 221.00 60.000 0.0000 0.0000 0.0000 0.0000	0.0000 18.000 26.000 146.00 227.00 464.00 489.00 489.00 332.00	4075.0 4075.0 4075.0 4075.0 4075.0 4075.0 4075.0 4075.0	0.0194 AETC N N 0.0144 AETC N N 0.0132 AETC N N 0.0107 AETC N N 0.0101 AETC N N 0.0103 AETC N N 0.0107 AETC N N 0.0110 AETC N N 0.0110 AETC N N
1849 1850 1851 1852 1853 1854 1855 1856	27.000 27.000 27.000 27.000 27.000 27.000 27.000 27.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	85.000 287.00 323.00 391.00 273.00 130.00 28.000	267.00 31.000 22.000 8.0000 34.000 102.00 183.00 357.00	3554.0 3554.0 3554.0 3554.0 3554.0 3554.0 3554.0	0.0094 AETC Y N 0.0119 AETC Y N 0.0116 AETC Y N 0.0128 AETC Y N 0.0108 AETC Y N 0.0101 AETC Y N 0.0081 AETC Y N 0.0087 AETC Y N
1857 1858 1859 1860 1861 1862 1863 1864	27.000 27.000 27.000 27.000 28.000 28.000 28.000 28.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 0.0000 0.0000 201.00 535.00 640.00	593.00 715.00 659.00 410.00 73.000 0.0000 0.0000	3554.0 3554.0 3554.0 3554.0 1395.0 1395.0	0.0092 AETC Y N 0.0083 AETC Y N 0.0101 AETC Y N 0.0080 AETC Y N 0.0104 AETC Y N 0.0171 AETC Y N 0.0020 AETC Y N
1865 1866 1867 1868 1869 1870 1871 1872	28.000 28.000 28.000 28.000 28.000 28.000 28.000 28.000 29.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	541.00 339.00 165.00 24.000 0.0000 0.0000 0.0000 9.0000 221.00	0.0000 14.000 71.000 242.00 568.00 581.00 511.00 291.00 72.000	1395.0 1395.0 1395.0 1395.0 1395.0 1395.0 1395.0 1395.0 6342.0	0.0172 AETC Y N 0.0158 AETC Y N 0.0105 AETC Y N 0.0077 AETC Y N 0.0086 AETC Y N 0.0090 AETC Y N 0.0081 AETC Y N 0.0075 AETC Y N 0.0067 AETC N N
1874 1875 1876 1877 1878 1879 1880 1881	29.000 29.000 29.000 29.000 29.000 29.000 29.000	94.000 94.000 94.000 94.000 94.000 94.000	540.00 615.00 766.00 656.00 342.00 149.00 44.000	3.0000 0.0000 0.0000 0.0000 28.000 73.000 168.00 523.00	6342.0 6342.0 6342.0 6342.0 6342.0 6342.0 6342.0 6342.0	0.0087 AETC N N 0.0087 AETC N N 0.0090 AETC N N 0.0112 AETC N N 0.0100 AETC N N 0.0068 AETC N N 0.0051 AETC N N 0.0055 AETC N N
1882 1883 1884 1885 1886 1887 1888 1889	29.000 29.000 29.000 30.000 30.000 30.000 30.000 30.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 19.000 27.000 165.00 396.00 454.00 198.00	545.00 576.00 312.00 220.00 55.000 1.0000 0.0000 23.000	6342.0 6342.0 6342.0 3589.0 3589.0 3589.0 3589.0	0.0050 AETC N N 0.0058 AETC N N 0.0038 AETC N N 0.0076 AETC Y N 0.0091 AETC Y N 0.0116 AETC Y N 0.0137 AETC Y N 0.0103 AETC Y N
1890 1891 1892 1893 1894 1895 1896 1897	30.000 30.000 30.000 30.000 30.000 30.000 30.000 31.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000	122.00 31.000 0.0000 0.0000 0.0000 0.0000 0.0000 256.00	53.000 158.00 283.00 426.00 459.00 454.00 364.00 37.000	3589.0 3589.0 3589.0 3589.0 3589.0 3589.0 3589.0	0.0086 AETC Y N 0.0079 AETC Y N 0.0079 AETC Y N 0.0085 AETC Y N 0.0088 AETC Y N 0.0084 AETC Y N 0.0091 AETC Y N 0.0089 AETC Y N
1898 1899 1900 1901 1902	31.000 31.000 31.000 31.000 31.000	94.000 94.000 94.000 94.000	672.00 751.00 971.00 803.00 413.00	0.0000 0.0000 0.0000 0.0000 19.000	1097.0 1097.0 1097.0 1097.0	0.0150 AETC Y N 0.0160 AETC Y N 0.0206 AETC Y N 0.0176 AETC Y N 0.0119 AETC Y N

1903 1904 1905 1906 1907 1908 1909 1910 1911 1912 1913 1914 1915 1916 1917 1918 1919 1920 1921	31.000 31.000 31.000 31.000 31.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000 32.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	205.00 59.000 0.0000 0.0000 33.000 100.00 298.00 370.00 284.00 137.00 56.000 12.000 0.0000 0.0000 0.0000 319.00	45.000 149.00 492.00 512.00 500.00 223.00 252.00 26.000 23.000 8.0000 27.000 82.000 139.00 297.00 515.00 637.00 592.00 359.00	1097.0 1097.0 1097.0 1097.0 1097.0 1097.0 1804.0 1804.0 1804.0 1804.0 1804.0 1804.0 1804.0 1804.0 1804.0	0.0102 AETC 0.0080 AETC 0.0085 AETC 0.0084 AETC 0.0091 AETC 0.0329 AETC 0.0328 AETC 0.0328 AETC 0.0311 AETC 0.0363 AETC 0.0284 AETC 0.0363 AETC 0.0476 AETC 0.0390 AETC 0.0386 AETC 0.0375 AETC 0.0343 AETC 0.0343 AETC	Y Y Y Y Y N N N N N N N N N N N N N N N	
1922	1.0000	94.000	567.00	9.0000	5898.0	0.0200 AMC	Y	N
1923	1.0000	94.000	914.00	0.0000	5898.0	0.0256 AMC	Y	N
1924	1.0000	94.000	1180.0	0.0000	5898.0	0.0312 AMC	Y	N
1925	1.0000	94.000	863.00	0.0000	5898.0	0.0297 AMC	Y	N
1926	1.0000	94.000	672.00	3.0000	5898.0	0.0272 AMC	Y	N
1927	1.0000	94.000	216.00	42.000	5898.0	0.0137 AMC	Y	N
1928	1.0000	94.000	209.00	39.000	5898.0	0.0081 AMC	Y	N
1929	1.0000	94.000	5.0000	322.00	5898.0	0.0095 AMC	Y	N
1930	1.0000	94.000	0.0000	452.00	5898.0	0.0108 AMC	Y	N
1931	1.0000	94.000	3.0000	241.00	5898.0	0.0103 AMC	Y	N
1932	1.0000	94.000	20.000	102.00	5898.0	0.0108 AMC	Y	N
1933	2.0000	94.000	49.000	127.00	2944.0	0.0087 AMC	Y	N
1934	2.0000	94.000	206.00	42.000	2944.0	0.0117 AMC	Y	N
1935 1936 1937	2.0000 2.0000 2.0000	94.000 94.000 94.000	504.00 568.00 327.00 152.00	0.0000 0.0000 7.0000	2944.0 2944.0 2944.0	0.0172 AMC 0.0192 AMC 0.0153 AMC	Y Y Y	N N N
1938 1939 1940 1941	2.0000 2.0000 2.0000 2.0000	94.000 94.000 94.000 94.000	30.000 11.000 0.0000	42.000 133.00 210.00 489.00	2944.0 2944.0 2944.0 2944.0	0.0130 AMC 0.0052 AMC 0.0056 AMC 0.0061 AMC	Y Y Y Y	N N N N
1942	2.0000	94.000	0.0000	537.00	2944.0	0.0072 AMC	Y	N
1943	2.0000	94.000	0.0000	473.00	2944.0	0.0064 AMC	Y	N
1944	2.0000	94.000	0.0000	327.00	2944.0	0.0044 AMC	Y	N
1945	3.0000	94.000	284.00	5.0000	3349.0	0.0111 AMC	Y	N
1946	3.0000	94.000	540.00	7.0000	3349.0	0.0170 AMC	Y	N
1947	3.0000	94.000	898.00	0.0000	3349.0	0.0237 AMC	Y	N
1948	3.0000	94.000	1145.0	0.0000	3349.0	0.0262 AMC	Y	N
1949 1950 1951	3.0000 3.0000 3.0000	94.000 94.000 94.000	872.00 690.00 234.00	0.0000 0.0000 21.000	3349.0 3349.0 3349.0	0.0227 AMC 0.0225 AMC	Y Y Y	N N
1952	3.0000	94.000	191.00	41.000	3349.0	0.0094 AMC	Y	N
1953	3.0000	94.000	5.0000	303.00	3349.0	0.0092 AMC	Y	N
1954	3.0000	94.000	0.0000	433.00	3349.0	0.0094 AMC	Y	N
1955	3.0000	94.000	0.0000	0.0000	3349.0	0.0095 AMC	Y	N
1956	3.0000	94.000	0.0000	0.0000	3349.0	0.0085 AMC	Y	N
1957	4.0000	94.000	535.00	0.0000	4394.0	0.0139 AMC	Y	N
1958	4.0000	94.000	1130.0	0.0000	4394.0	0.0219 AMC	Y	N
1959	4.0000	94.000	1116.0	0.0000	4394.0	0.0237 AMC	Y	N
1960	4.0000	94.000	965.00	0.0000	4394.0	0.0223 AMC	Y	N
1961	4.0000	94.000	1070.0	0.0000	4394.0	0.0222 AMC	Y	N
1962	4.0000	94.000	784.00	0.0000	4394.0	0.0187 AMC	Y	N
1963	4.0000	94.000	544.00	0.0000	4394.0	0.0144 AMC	Y	N
1964	4.0000	94.000	386.00	0.0000	4394.0	0.0105 AMC	Y	N
1965	4.0000	94.000	209.00	0.0000	4394.0	0.0070 AMC	Y	N
1966	4.0000	94.000	47.000	207.00	4394.0	0.0063 AMC	Y	N
1967	4.0000	94.000	53.000	106.00	4394.0	0.0067 AMC	Y	N
1968	4.0000	94.000	141.00	8.0000	4394.0	0.0079 AMC	Y	N
1969	5.0000	94.000	705.00	0.0000	3821.0	0.0231 AMC	Y	N
1970	5.0000	94.000	1283.0	0.0000	3821.0	0.0266 AMC	Y	N
1971	5.0000	94.000	1563.0	0.0000	3821.0	0.0324 AMC	Y	N
1972	5.0000	94.000	2198.0	0.0000	3821.0	0.0272 AMC	Y	N
1973	5.0000	94.000	1743.0		3821.0	0.0290 AMC	Y	N

1975 5.0000 94.000 652.00 0.0000 3821.0 0.0219 AMC 1976 5.0000 94.000 212.00 40.000 3821.0 0.0167 AMC 1977 5.0000 94.000 17.000 79.000 3821.0 0.0146 AMC 1978 5.0000 94.000 12.000 84.000 3821.0 0.0135 AMC 1979 5.0000 94.000 61.000 134.00 3821.0 0.0155 AMC 1980 5.0000 94.000 165.00 54.000 3821.0 0.0138 AMC 1981 6.0000 94.000 449.00 0.0000 2315.0 0.0178 AMC 1982 6.0000 94.000 766.00 0.0000 2315.0 0.0242 AMC 1983 6.0000 94.000 1104.0 0.0000 2315.0 0.0282 AMC	Y N Y N Y N Y N Y N Y N Y N Y N Y N Y N
1978 5.0000 94.000 12.000 84.000 3821.0 0.0135 AMC 1979 5.0000 94.000 61.000 134.00 3821.0 0.0155 AMC 1980 5.0000 94.000 165.00 54.000 3821.0 0.0138 AMC 1981 6.0000 94.000 449.00 0.0000 2315.0 0.0178 AMC 1982 6.0000 94.000 766.00 0.0000 2315.0 0.0242 AMC 1983 6.0000 94.000 1104.0 0.0000 2315.0 0.0282 AMC	Y N Y N Y N Y N Y N Y N Y N Y N Y N Y N
1980 5.0000 94.000 165.00 54.000 3821.0 0.0138 AMC 1981 6.0000 94.000 449.00 0.0000 2315.0 0.0178 AMC 1982 6.0000 94.000 766.00 0.0000 2315.0 0.0242 AMC 1983 6.0000 94.000 1104.0 0.0000 2315.0 0.0282 AMC	Y N Y N Y N Y N Y N Y N Y N Y N Y N Y N
1982 6.0000 94.000 766.00 0.0000 2315.0 0.0242 AMC 1983 6.0000 94.000 1104.0 0.0000 2315.0 0.0282 AMC	Y N Y N Y N Y N Y N Y N Y N Y N Y N
	Y N Y N Y N Y N Y N Y N Y N
1984 6.0000 94.000 1477.0 0.0000 2315.0 0.0291 AMC 1985 6.0000 94.000 1209.0 0.0000 2315.0 0.0270 AMC	$\begin{array}{ccc} Y & N \\ Y & N \end{array}$
1986 6.0000 94.000 1040.0 0.0000 2315.0 0.0266 AMC 1987 6.0000 94.000 393.00 22.000 2315.0 0.0189 AMC	Y N Y N Y N
1988 6.0000 94.000 197.00 63.000 2315.0 0.0139 AMC 1989 6.0000 94.000 18.000 266.00 2315.0 0.0120 AMC	Y N
1990 6.0000 94.000 0.0000 0.0000 2315.0 0.0000 AMC 1991 6.0000 94.000 0.0000 0.0000 2315.0 0.0000 AMC	
1992 6.0000 94.000 0.0000 0.0000 2315.0 0.0000 AMC 1993 7.0000 94.000 10.000 114.00 3719.0 0.0073 AMC	Y N Y N
1994 7.0000 94.000 178.00 10.000 3719.0 0.0084 AMC 1995 7.0000 94.000 367.00 0.0000 3719.0 0.0104 AMC	Y N Y N
1996 7.0000 94.000 289.00 0.0000 3719.0 0.0104 AMC 1997 7.0000 94.000 383.00 0.0000 3719.0 0.0107 AMC	Y N Y N
1998 7.0000 94.000 228.00 1.0000 3719.0 0.0092 AMC 1999 7.0000 94.000 178.00 25.000 3719.0 0.0081 AMC	Y N Y N
2000 7.0000 94.000 96.000 32.000 3719.0 0.0071 AMC 2001 7.0000 94.000 0.0000 319.00 3719.0 0.0075 AMC	Y N Y N
2002 7.0000 94.000 0.0000 366.00 3719.0 0.0087 AMC 2003 7.0000 94.000 0.0000 515.00 3719.0 0.0083 AMC	Y N Y N
2004 7.0000 94.000 1.0000 285.00 3719.0 0.0082 AMC 2005 8.0000 94.000 381.00 0.0000 3683.0 0.0082 AMC	Y N Y N
2006 8.0000 94.000 759.00 0.0000 3683.0 0.0123 AMC 2007 8.0000 94.000 757.00 0.0000 3683.0 0.0150 AMC	Y N Y N
2008 8.0000 94.000 663.00 0.0000 3683.0 0.0140 AMC 2009 8.0000 94.000 707.00 0.0000 3683.0 0.0141 AMC	Y N Y N
2010 8.0000 94.000 531.00 0.0000 3683.0 0.0134 AMC 2011 8.0000 94.000 417.00 0.0000 3683.0 0.0122 AMC	Y N Y N
2012 8.0000 94.000 277.00 0.0000 3683.0 0.0093 AMC 2013 8.0000 94.000 182.00 0.0000 3683.0 0.0092 AMC	Y N Y N
2014 8.0000 94.000 0.0000 0.0000 3683.0 0.0069 AMC 2015 8.0000 94.000 0.0000 0.0000 3683.0 0.0072 AMC	Y N Y N
2016 8.0000 94.000 0.0000 0.0000 3683.0 0.0075 AMC 2017 9.0000 94.000 295.00 32.000 2212.0 0.0084 AMC	Y N Y N
2018 9.0000 94.000 664.00 0.0000 2212.0 0.0178 AMC 2019 9.0000 94.000 751.00 0.0000 2212.0 0.0191 AMC	Y N Y N
2020 9.0000 94.000 1006.0 0.0000 2212.0 0.0227 AMC 2021 9.0000 94.000 861.00 0.0000 2212.0 0.0197 AMC	Y N Y N
2023 9.0000 94.000 316.00 29.000 2212.0 0.0128 AMC	Y N Y N
2024 9.0000 94.000 66.000 129.00 2212.0 0.0104 AMC 2025 9.0000 94.000 0.0000 409.00 2212.0 0.0088 AMC	Y N Y N
2026 9.0000 94.000 0.0000 355.00 2212.0 0.0079 AMC 2027 9.0000 94.000 0.0000 380.00 2212.0 0.0082 AMC	Y N Y N
2028 9.0000 94.000 32.000 237.00 2212.0 0.0077 AMC 2029 10.000 94.000 339.00 3.0000 4199.0 0.0124 AMC	Y N Y N
2030 10.000 94.000 593.00 4.0000 4199.0 0.0177 AMC 2031 10.000 94.000 908.00 0.0000 4199.0 0.0203 AMC	Y N Y N
2032 10.000 94.000 1214.0 0.0000 4199.0 0.0245 AMC 2033 10.000 94.000 992.00 0.0000 4199.0 0.0232 AMC	Y N Y N
2034 10.000 94.000 742.00 0.0000 4199.0 0.0254 AMC 2035 10.000 94.000 289.00 19.000 4199.0 0.0145 AMC	Y N Y N
2036 10.000 94.000 211.00 31.000 4199.0 0.0106 AMC 2037 10.000 94.000 6.0000 279.00 4199.0 0.0092 AMC	Y N Y N
2038 10.000 94.000 0.0000 0.0000 4199.0 0.0126 AMC 2039 10.000 94.000 0.0000 0.0000 4199.0 0.0122 AMC 2040 10.000 0.000 0.0000 4199.0 0.0115 AMC	Y N Y N
2040 10.000 94.000 0.0000 0.0000 4199.0 0.0115 AMC 2041 11.000 94.000 10.000 114.00 6069.0 0.0036 AMC	Y N Y N
2042 11.000 94.000 178.00 10.000 6069.0 0.0043 AMC 2043 11.000 94.000 367.00 0.0000 6069.0 0.0044 AMC 2044 11.000 94.000 289.00 0.0000 6069.0 0.0044 AMC	Y N Y N Y N

2045 2046 2047 2048 2049 2050	11.000 11.000 11.000 11.000 11.000	94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000	6069.0 6069.0 6069.0 6069.0 6069.0	0.0000 AMC 0.0000 AMC 0.0000 AMC 0.0000 AMC 0.0000 AMC	Y Y Y Y Y	N N N N N
2051 2052 2053 2054 2055 2056	11.000 11.000 12.000 12.000 12.000 12.000	94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 605.00 577.00 1325.0 1835.0	0.0000 0.0000 0.0000 0.0000 0.0000	6069.0 6069.0 2577.0 2577.0 2577.0	0.0000 AMC 0.0000 AMC 0.0132 AMC 0.0175 AMC 0.0266 AMC 0.0320 AMC	Y Y Y Y Y	N N N N N
2057 2058 2059 2060 2061 2062	12.000 12.000 12.000 12.000 12.000	94.000 94.000 94.000 94.000 94.000	1420.0 1089.0 620.00 344.00 51.000	0.0000 0.0000 0.0000 13.000 100.00 0.0000	2577.0 2577.0 2577.0 2577.0 2577.0	0.0280 AMC 0.0189 AMC 0.0217 AMC 0.0178 AMC 0.0074 AMC 0.0087 AMC	Y Y Y Y Y	N N N N N
2063 2064 2065 2066 2067 2068	12.000 12.000 13.000 13.000 13.000	94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 307.00 668.00 873.00 1198.0	0.0000 0.0000 11.000 0.0000 0.0000	2577.0 2577.0 3944.0 3944.0 3944.0	0.0070 AMC 0.0083 AMC 0.0117 AMC 0.0168 AMC 0.0181 AMC 0.0225 AMC	Y Y Y Y Y	N N N N N
2069 2070 2071 2072 2073 2074 2075	13.000 13.000 13.000 13.000 13.000 13.000	94.000 94.000 94.000 94.000 94.000 94.000	848.00 602.00 290.00 114.00 3.0000 0.0000	0.0000 0.0000 30.000 53.000 380.00 448.00 315.00	3944.0 3944.0 3944.0 3944.0 3944.0 3944.0	0.0180 AMC 0.0165 AMC 0.0135 AMC 0.0110 AMC 0.0135 AMC 0.0116 AMC 0.0151 AMC	Y Y Y Y Y Y	N N N N N
2076 2077 2078 2079 2080 2081	13.000 14.000 14.000 14.000 14.000	94.000 94.000 94.000 94.000 94.000 94.000	58.000 38.000 10.000 543.00 500.00 467.00	132.00 398.00 7.0000 0.0000 0.0000	3944.0 6635.0 6635.0 6635.0 6635.0	0.0137 AMC 0.0107 AMC 0.0058 AMC 0.0059 AMC 0.0109 AMC 0.0116 AMC 0.0099 AMC	Y Y Y Y Y Y	N N N N N
2082 2083 2084 2085 2086 2087	14.000 14.000 14.000 14.000 14.000	94.000 94.000 94.000 94.000 94.000 94.000	181.00 139.00 89.000 11.000 0.0000	5.0000 14.000 34.000 147.00 0.0000	6635.0 6635.0 6635.0 6635.0 6635.0	0.0129 AMC 0.0064 AMC 0.0055 AMC 0.0060 AMC 0.0059 AMC 0.0059 AMC	Y Y Y Y Y	N N N N N
2088 2089 2090 2091 2092	14.000 1.0000 1.0000 1.0000 1.0000	94.000 93.000 93.000 93.000 93.000 93.000	0.0000 358.00 530.00 828.00 899.00 906.00	0.0000 11.000 0.0000 0.0000 0.0000	6635.0 5786.0 5786.0 5786.0 5786.0 5786.0	0.0055 AMC 0.0110 AMC 0.0170 AMC 0.0259 AMC 0.0251 AMC 0.0260 AMC	Y Y Y Y Y	N N N N
2094 2095 2096 2097 2098 2099	1.0000 1.0000 1.0000 1.0000 1.0000	93.000 93.000 93.000 93.000 93.000 93.000	769.00 366.00 68.000 19.000 0.0000	0.0000 8.0000 60.000 284.00 476.00 333.00	5786.0 5786.0 5786.0 5786.0 5786.0 5786.0	0.0285 AMC 0.0108 AMC 0.0089 AMC 0.0084 AMC 0.0110 AMC 0.0077 AMC	Y Y Y Y Y	N N N N N
2100 2101 2102 2103 2104 2105	1.0000 2.0000 2.0000 2.0000 2.0000 2.0000	93.000 93.000 93.000 93.000 93.000 93.000	66.000 70.000 197.00 430.00 353.00 421.00	161.00 79.000 68.000 5.0000 7.0000	5786.0 2961.0 2961.0 2961.0 2961.0 2961.0	0.0168 AMC 0.0080 AMC 0.0119 AMC 0.0170 AMC 0.0166 AMC 0.0165 AMC	Y Y Y Y Y	N N N N N
2106 2107 2108 2109 2110 2111	2.0000 2.0000 2.0000 2.0000 2.0000 2.0000	93.000 93.000 93.000 93.000 93.000 93.000	279.00 132.00 1.0000 0.0000 0.0000	4.0000 37.000 241.00 440.00 644.00 536.00	2961.0 2961.0 2961.0 2961.0 2961.0 2961.0	0.0168 AMC 0.0100 AMC 0.0052 AMC 0.0061 AMC 0.0071 AMC 0.0064 AMC	Y Y Y Y Y	N N N N N
2112 2113 2114 2115	2.0000 3.0000 3.0000 3.0000	93.000 93.000 93.000 93.000	3.0000 348.00 514.00 788.00	410.00 11.000 0.0000	2961.0 3349.0 3349.0 3349.0	0.0040 AMC 0.0122 AMC 0.0183 AMC 0.0228 AMC	Y Y Y Y	N N N N

2116	3.0000	93.000	826.00	0.0000	3349.0	0.0236 AMC	Y	N
2117	3.0000	93.000	913.00	0.0000	3349.0	0.0263 AMC	Y	N
2118	3.0000	93.000	769.00	0.0000	3349.0	0.0236 AMC	Y	N
2119	3.0000	93.000	368.00	1.0000	3349.0	0.0173 AMC	Ү	N
2120	3.0000	93.000	88.000	60.000	3349.0	0.0092 AMC	Ү	N
2121	3.0000	93.000	16.000	250.00	3349.0	0.0092 AMC	Ү	N
2122	3.0000	93.000	0.0000	488.00	3349.0	0.0088 AMC	Ү	N
2123	3.0000	93.000	0.0000	339.00	3349.0	0.0102 AMC	Ү	N
2124	3.0000	93.000	57.000	165.00	3349.0	0.0094 AMC	Ү	N
2125	4.0000	93.000	0.0000	0.0000	4320.0	0.0139 AMC	Y	N
2126	4.0000	93.000	0.0000	0.0000	4320.0	0.0211 AMC	Y	N
2127	4.0000	93.000	0.0000	0.0000	4320.0	0.0263 AMC	Y	N
2128 2129	4.0000 4.0000	93.000 93.000	0.0000	0.0000	4320.0 4320.0	0.0268 AMC 0.0280 AMC	Y Y	N N
2130	4.0000	93.000	0.0000	0.0000	4320.0	0.0198 AMC	Ү	N
2131	4.0000	93.000	0.0000	0.0000	4320.0	0.0168 AMC	Ү	N
2132	4.0000	93.000	0.0000	0.0000	4320.0	0.0105 AMC	Ү	N
2133	4.0000	93.000	0.0000	0.0000	4320.0	0.0086 AMC	Y	N
2134	4.0000	93.000	0.0000	0.0000	4320.0	0.0075 AMC	Y	N
2135	4.0000	93.000	0.0000	0.0000	4320.0	0.0073 AMC	Y	N
2136	4.0000	93.000	0.0000	0.0000	4320.0	0.0078 AMC	Y	N
2137	5.0000	93.000	682.00	0.0000	3793.0	0.0249 AMC	Y	N
2138	5.0000	93.000	1178.0	0.0000	3793.0	0.0252 AMC	Y	N
2139	5.0000	93.000	1799.0	0.0000	3793.0	0.0312 AMC	У	N
2140	5.0000	93.000	1871.0	0.0000	3793.0	0.0342 AMC	У	N
2141	5.0000	93.000	1539.0	0.0000	3793.0	0.0308 AMC	У	N
2142	5.0000	93.000	1209.0	4.0000	3793.0	0.0268 AMC	Y	N
2143	5.0000	93.000	673.00	0.0000	3793.0	0.0229 AMC	Y	N
2144	5.0000	93.000	297.00	24.000	3793.0	0.0173 AMC	Y	N
2145	5.0000	93.000	130.00	63.000	3793.0	0.0167 AMC	Y	N
2146	5.0000	93.000	48.000	80.000	3793.0	0.0165 AMC	Y	N
2147	5.0000	93.000	37.000	116.00	3793.0	0.0180 AMC	Y	N
2148	5.0000	93.000	346.00	8.0000	3793.0	0.0156 AMC	Y	N
2149	6.0000	93.000	404.00	3.0000	2315.0	0.0165 AMC	Y	N
2150	6.0000	93.000	721.00	0.0000	2315.0	0.0245 AMC	Ү	N
2151	6.0000	93.000	1069.0	0.0000	2315.0	0.0309 AMC	Ү	N
2152	6.0000	93.000	1129.0	0.0000	2315.0	0.0407 AMC	Ү	N
2153	6.0000	93.000	1148.0	0.0000	2315.0	0.0314 AMC	Y	N
2154	6.0000	93.000	881.00	0.0000	2315.0	0.0279 AMC	Y	N
2155	6.0000	93.000	489.00	0.0000	2315.0	0.0217 AMC	Y	N
2156	6.0000	93.000	129.00	41.000	2315.0	0.0129 AMC	Y	N
2157	6.0000	93.000	50.000	160.00	2315.0	0.0145 AMC	Y	N
2158	6.0000	93.000	0.0000	314.00	2315.0	0.0131 AMC	Y	N
2159	6.0000	93.000	5.0000	263.00	2315.0	0.0127 AMC	Y	N
2160	6.0000	93.000	0.0000	26.000	2315.0	0.0119 AMC	Y	N
2161	7.0000	93.000	13.000	171.00	3382.0	0.0066 AMC	Y	N
2162 2163 2164	7.0000 7.0000 7.0000	93.000 93.000 93.000	202.00 460.00 369.00	2.0000 0.0000 0.0000	3382.0 3382.0 3382.0	0.0070 AMC 0.0107 AMC 0.0107 AMC	Y Y Y	N N
2165	7.0000	93.000	303.00	1.0000	3382.0	0.0093 AMC	Y	N
2166	7.0000	93.000	163.00	7.0000	3382.0	0.0078 AMC	Y	N
2167	7.0000	93.000	85.000	49.000	3382.0	0.0065 AMC	Y	N
2168	7.0000	93.000	7.0000	133.00	3382.0	0.0067 AMC	Y	N
2169	7.0000	93.000	17.000	305.00	3382.0	0.0067 AMC	Y	N
2170	7.0000	93.000	0.0000	268.00	3382.0	0.0081 AMC	Y	N
2171	7.0000	93.000	0.0000	352.00	3382.0	0.0073 AMC	Y	N
2172	7.0000	93.000	0.0000	312.00	3382.0	0.0081 AMC	Y	N
2173	8.0000	93.000	394.00	0.0000	3670.0	0.0105 AMC	Y	N
2174	8.0000	93.000	654.00	0.0000	3670.0	0.0126 AMC	Y	N
2175	8.0000	93.000	869.00	0.0000	3670.0	0.0156 AMC	Y	N
2176	8.0000	93.000	934.00	0.0000	3670.0	0.0173 AMC	Y	N
2177	8.0000	93.000	729.00	0.0000	3670.0	0.0146 AMC	Y	N
2178	8.0000	93.000	589.00		3670.0	0.0143 AMC	Y	N
2179	8.0000	93.000	460.00	0.0000	3670.0	0.0119 AMC	У	N
2180	8.0000	93.000	179.00	4.0000	3670.0	0.0098 AMC	У	N
2181	8.0000	93.000	149.00	5.0000	3670.0	0.0087 AMC	У	N
2182	8.0000	93.000	114.00	1.0000	3670.0	0.0078 AMC	Y	N
2183	8.0000	93.000	60.000	60.000	3670.0	0.0058 AMC	Y	N
2184	8.0000	93.000	170.00	23.000	3670.0	0.0077 AMC	Y	N
2185	9.0000	93.000	199.00	48.000	2170.0	0.0098 AMC	Y	N
2186	9.0000	93.000	677.00	0.0000	2170.0	0.0163 AMC	Y	N

2187 2188 2189	9.0000 9.0000 9.0000	93.000 93.000 93.000	896.00 1040.0 856.00	0.0000 0.0000 0.0000	2170.0 2170.0 2170.0	0.0198 AMC 0.0231 AMC 0.0185 AMC	Y	N N N
2190 2191 2192	9.0000 9.0000 9.0000	93.000 93.000 93.000	641.00 320.00 79.000	3.0000 2.0000 77.000	2170.0 2170.0 2170.0	0.0184 AMC 0.0131 AMC 0.0090 AMC	Y Y	N N N
2193 2194 2195	9.0000 9.0000 9.0000	93.000 93.000 93.000	9.0000 0.0000 0.0000	333.00 550.00 502.00	2170.0 2170.0 2170.0	0.0081 AMC 0.0082 AMC 0.0077 AMC	Y Y	N N N
2196 2197 2198	9.0000 10.000 10.000	93.000 93.000 93.000	57.000 399.00 550.00	132.00 5.0000 0.0000 0.0000	2170.0 4192.0 4192.0 4192.0	0.0062 AMC 0.0191 AMC 0.0221 AMC	Y Y	N N N
2199 2200 2201 2202	10.000 10.000 10.000 10.000	93.000 93.000 93.000 93.000	869.00 871.00 969.00 804.00	0.0000 0.0000 0.0000	4192.0 4192.0 4192.0	0.0225 AMC 0.0223 AMC 0.0238 AMC 0.0239 AMC	Y Y	N N N N
2202 2203 2204 2205	10.000 10.000 10.000	93.000 93.000 93.000	380.00 105.00 22.000	0.0000 46.000 208.00	4192.0 4192.0 4192.0	0.0185 AMC 0.0110 AMC 0.0089 AMC	Y Y	N N N
2206 2207 2208	10.000 10.000 10.000	93.000 93.000 93.000	0.0000 0.0000 85.000	404.00 312.00 141.00	4192.0 4192.0 4192.0	0.0123 AMC 0.0131 AMC 0.0118 AMC	Y Y	N N N
2209 2210 2211	11.000 11.000 11.000	93.000 93.000 93.000	14.000 196.00 468.00	143.00 6.0000 0.0000	6069.0 6069.0 6069.0	0.0054 AMO 0.0063 AMO 0.0088 AMO	Y Y	N N N
2212 2213 2214	11.000 11.000 11.000	93.000 93.000 93.000	410.00 328.00 140.00	0.0000 0.0000 4.0000	6069.0 6069.0 6069.0	0.0095 AMC 0.0076 AMC 0.0066 AMC	Y Y	N N N
2215 2216 2217	11.000 11.000 11.000	93.000 93.000 93.000	50.000 3.0000 18.000	47.000 139.00 310.00	6069.0 6069.0 6069.0	0.0052 AMC 0.0052 AMC 0.0052 AMC	Y Y	N N N
2218 2219 2220	11.000 11.000 11.000	93.000 93.000 93.000	0.0000 0.0000 0.0000	313.00 352.00 312.00	6069.0 6069.0	0.0050 AMC 0.0054 AMC 0.0044 AMC	Y Y	N N N
2221 2222 2223 2224	12.000 12.000 12.000 12.000	93.000 93.000 93.000 93.000	639.00 870.00 1177.0 1385.0	0.0000 0.0000 0.0000 0.0000	2650.0 2650.0 2650.0 2650.0	0.0190 AMC 0.0219 AMC 0.0276 AMC 0.0290 AMC	Y Y	N N N N
2225 2226 2227	12.000 12.000 12.000	93.000 93.000 93.000	1576.0 1217.0 631.00	0.0000 0.0000 0.0000	2650.0 2650.0 2650.0	0.0303 AMC 0.0296 AMC 0.0203 AMC	Y Y	N N N
2228 2229 2230	12.000 12.000 12.000	93.000 93.000 93.000	302.00 102.00 0.0000	1.0000 38.000 12.000	2650.0 2650.0 2650.0	0.0157 AMC 0.0064 AMC 0.0059 AMC	Y Y	N N N
2231 2232 2233	12.000 12.000 13.000	93.000 93.000 93.000	25.000 25.000 261.00	114.00 214.00 16.000	2650.0 2650.0 3825.0	0.0068 AMC 0.0066 AMC 0.0112 AMC	Y Y	N N N
2236	13.000 13.000 13.000	93.000 93.000 93.000	608.00 923.00 1091.0	0.0000 0.0000 0.0000	3825.0 3825.0 3825.0	0.0172 AMC 0.0202 AMC 0.0146 AMC	Y Y	N
2237 2238 2239 2240	13.000 13.000 13.000 13.000	93.000 93.000 93.000 93.000	970.00 740.00 372.00 75.000	0.0000 0.0000 5.0000 80.000	3825.0 3825.0 3825.0 3825.0	0.0133 AMC 0.0173 AMC 0.0134 AMC 0.0118 AMC	Y Y	N N N N
2241 2242 2243	13.000 13.000 13.000	93.000 93.000 93.000	13.000 0.0000 0.0000	291.00 500.00 427.00	3825.0 3825.0 3825.0	0.0126 AMC 0.0153 AMC 0.0131 AMC	Y Y	N N N
2244 2245 2246	13.000 14.000 14.000	93.000 93.000 93.000	69.000 7.0000 239.00	99.000 7.0000 16.000	3825.0 6635.0 6635.0	0.0111 AMC 0.0058 AMC 0.0065 AMC	Y Y	N N N
2247 2248 2249 2250	14.000 14.000 14.000 14.000	93.000 93.000 93.000 93.000	637.00 628.00 500.00 221.00	0.0000 20.000 0.0000 0.0000	6635.0 6635.0 6635.0 6635.0	0.0091 AMC 0.0133 AMC 0.0114 AMC 0.0098 AMC	Y Y	N N N N
2251 2252 2253	14.000 14.000 14.000	93.000 93.000 93.000	205.00 63.000 15.000	7.0000 44.000 266.00	6635.0 6635.0 6635.0	0.0056 AMC 0.0056 AMC	Y Y	N N N
2254 2255 2256	14.000 14.000 14.000	93.000 93.000 93.000	0.0000 0.0000 4.0000	232.00 259.00 185.00	6635.0 6635.0 6635.0	0.0061 AMC 0.0044 AMC 0.0055 AMC	Y Y	N N N
2257	1.0000	92.000	259.00	19.000	5665.0	0.0103 AMO	Y	N

2258 2259 2260 2261 2262 2263 2264 2265 2266 2267 2271 2272 2273 2274 2275 2276 2277 2278 2279 2280 2281 2282 2283 2284 2285	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 2.0000 3.0000 3.0000 3.0000	92.000 92.000	547.00 781.00 898.00 766.00 697.00 0.0000 0.0000 20.000 5.0000 41.000 281.00 349.00 473.00 293.00 234.00 119.00 28.000 0.0000 0.0000 0.0000 0.0000 3.0000 523.00 750.00 881.00 776.00	5.0000 0.0000 0.0000 0.0000 10.000 28.000 129.00 350.00 189.00 111.00 128.00 25.000 0.0000 7.0000 20.000 83.000 199.00 381.00 592.00 495.00 345.00 23.000 3.0000 0.0000 0.0000 0.0000	5665.0 5665.0 5665.0 5665.0 5665.0 5665.0 5665.0 5665.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 2954.0 3542.0 3542.0 3542.0	0.0185 AMC 0.0273 AMC 0.0293 AMC 0.0252 AMC 0.0245 AMC 0.0171 AMC 0.0099 AMC 0.0084 AMC 0.0061 AMC 0.0092 AMC 0.0138 AMC 0.0163 AMC 0.0169 AMC 0.0169 AMC 0.0166 AMC 0.0169 AMC 0.0164 AMC 0.0122 AMC 0.0164 AMC 0.0064 AMC 0.0054 AMC 0.0055 AMC 0.0065 AMC	Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1 1 Y 1	ии иии иии иии иии иии иии иии иии
2286 2287 2288 2289 2290 2291 2292 2293 2294 2295 2296 2297 2298 2300 2301 2302 2303 2304 2305 2306 2307 2308 2310 2311 2312 2313 2314 2315 2316 2317 2318 2319 2321 2322 2323 2324 2325 2326 2327 2328	3.0000 3.0000 3.0000 3.0000 3.0000 4.0000 4.0000 4.0000 4.0000 4.0000 4.0000 4.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000	92.000 92.000	709.00 407.00 208.00 13.000 0.0000 0.0000 612.00 962.00 1044.0 1080.0 798.00 636.00 87.000 88.000 87.000 1331.0 1478.0 1519.0 1291.0 1070.0 771.00 269.00 163.00 118.00 107.00 337.00 337.00 337.00 337.00 337.00 337.00 337.00 337.00 337.00 337.00 318.00 1101.0 841.00 791.00 498.00 200.00 5.0000 26.000 117.00	0.0000 7.0000 38.000 127.00 361.00 232.00 128.00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 122.00 94.000 158.00 4.0000 0.0000	3542.0 3542.0 3542.0 3542.0 3542.0 4460.0 4460.0 4460.0 4460.0 4460.0 4460.0 4460.0 4460.0 4460.0 3278.0	0.0212 AMC 0.0174 AMC 0.0095 AMC 0.0075 AMC 0.0082 AMC 0.0082 AMC 0.0082 AMC 0.0146 AMC 0.0222 AMC 0.0239 AMC 0.0183 AMC 0.0167 AMC 0.0128 AMC 0.0128 AMC 0.0067 AMC 0.0058 AMC 0.0067 AMC 0.0058 AMC 0.0058 AMC 0.0077 AMC 0.0058 AMC 0.0373 AMC 0.0374 AMC 0.0374 AMC 0.0375 AMC 0.0375 AMC 0.0376 AMC 0.0377 AMC 0.0377 AMC 0.0378 AMC 0.0378 AMC 0.0379 AMC 0.0381 AMC 0.0391 AMC 0.0187 AMC	Y 1 1 Y 1 Y 1 1 Y 1 Y 1 1 Y 1	

2329	7.0000	92.000	52.000	277.00	3214.0	0.0075 AMC	Y	N
2330	7.0000	92.000	144.00	50.000	3214.0	0.0078 AMC	Y	N
2331	7.0000	92.000	295.00	0.0000	3214.0	0.0097 AMC	Y	N
2332	7.0000	92.000	306.00	0.0000	3214.0	0.0111 AMC	Y	N
2333	7.0000	92.000	146.00	9.0000	3214.0	0.0091 AMC	Y	N
2334	7.0000	92.000	314.00	0.0000	3214.0	0.0093 AMC	Y	N
2335	7.0000	92.000	64.000	87.000	3214.0	0.0070 AMC	Y	N
2336	7.0000	92.000	0.0000	133.00	3214.0	0.0065 AMC	Y	N
2337	7.0000	92.000	4.0000	200.00	3214.0	0.0065 AMC	Y	N
2338	7.0000	92.000	0.0000	377.00	3214.0	0.0068 AMC	Y	N
2339	7.0000	92.000		529.00	3214.0	0.0069 AMC	Y	N
2340	7.0000	92.000	0.0000	468.00	3214.0	0.0073 AMC	Y	N
2341	8.0000	92.000	442.00	0.0000	3630.0	0.0090 AMC	Y	N
2342	8.0000	92.000	570.00	0.0000	3630.0	0.0116 AMC	Y	N
2343	8.0000	92.000	713.00	0.0000	3630.0	0.0152 AMC	Y	N
2344	8.0000	92.000	707.00	0.0000	3630.0	0.0155 AMC	Y	N
2345	8.0000	92.000	565.00	0.0000	3630.0	0.0143 AMC	Y	N
2346	8.0000	92.000	539.00	0.0000	3630.0	0.0129 AMC	Y	N
2347	8.0000	92.000	410.00	0.0000	3630.0	0.0117 AMC	Y	N
2348	8.0000	92.000	215.00	9.0000	3630.0	0.0093 AMC	Y	N
2349	8.0000	92.000	70.000	59.000	3630.0	0.0074 AMC	Y	N
2350	8.0000	92.000	32.000	59.000	3630.0	0.0072 AMC	Y	N
2351	8.0000	92.000	41.000	63.000	3630.0	0.0071 AMC	Y	N
2352	8.0000	92.000	191.00	6.0000	3630.0	0.0088 AMC	Y	N
2353	9.0000	92.000	224.00	100.00	2187.0	0.0086 AMC	Y	N
2354	9.0000	92.000	723.00	0.0000	2187.0	0.0188 AMC	Y	N
2355	9.0000	92.000	758.00	0.0000	2187.0	0.0183 AMC	Y	N
2356	9.0000	92.000	776.00	0.0000	2187.0	0.0185 AMC	Y	N
2357	9.0000	92.000	540.00	0.0000	2187.0	0.0146 AMC	Y	N
2358	9.0000	92.000	437.00	4.0000	2187.0	0.0140 AMC	Y	N
2359	9.0000	92.000	228.00	31.000	2187.0	0.0090 AMC	Y	N
2360	9.0000	92.000	90.000	95.000	2187.0	0.0071 AMC	Y	N
2361	9.0000	92.000	6.0000	215.00	2187.0	0.0073 AMC	Y	N
2362	9.0000	92.000	0.0000	463.00	2187.0	0.0076 AMC	Y	N
2363	9.0000	92.000	1.0000	276.00	2187.0	0.0075 AMC	Y	N
2364	9.0000	92.000	19.000	224.00	2187.0	0.0073 AMC	Y	N
2365	10.000	92.000	276.00	23.000	4193.0	0.0115 AMC	Y	N
2366	10.000	92.000	556.00	3.0000	4193.0	0.0181 AMC	Y	N
2367	10.000	92.000	766.00	0.0000	4193.0	0.0229 AMC	Y	N
2368	10.000	92.000	933.00	0.0000	4193.0	0.0247 AMC	Y	N
2369	10.000	92.000	835.00	0.0000	4193.0	0.0242 AMC	Y	N
2370	10.000	92.000	766.00	0.0000	4193.0	0.0230 AMC	Y	N
2371	10.000	92.000	461.00	6.0000	4193.0	0.0175 AMC	Y	N
2372	10.000	92.000	227.00	25.000	4193.0	0.0098 AMC	Y	N
2373	10.000	92.000	18.000	138.00	4193.0	0.0062 AMC	Y	N
2374	10.000	92.000	2.0000	287.00	4193.0	0.0010 AMC	Y	N
2375	10.000	92.000	1.0000	198.00	4193.0	0.0089 AMC	Y	N
2376	10.000	92.000	68.000	117.00	4193.0	0.0075 AMC	Y	N
2377	11.000	92.000	65.000	277.00	6071.0	0.0069 AMC	Y	N
2378	11.000	92.000	175.00	41.000	6071.0	0.0069 AMC	Y	N
2379	11.000	92.000	320.00	0.0000	6071.0	0.0091 AMC	Y	N
2380	11.000	92.000	335.00	0.0000	6071.0	0.0096 AMC	Y	N
2381	11.000	92.000	212.00	5.0000	6071.0	0.0084 AMC	Y	N
2382	11.000	92.000	238.00	0.0000	6071.0	0.0086 AMC	Y	N
2383	11.000	92.000	45.000	97.000	6071.0	0.0069 AMC	Y	N
2384	11.000	92.000	1.0000	184.00	6071.0	0.0058 AMC	Y	N
2385 2386 2387	11.000 11.000 11.000	92.000 92.000 92.000	3.0000 0.0000 0.0000	236.00 445.00 540.00	6071.0 6071.0 6071.0	0.0052 AMC 0.0062 AMC 0.0062 AMC	Y Y Y	N N
2388	11.000	92.000	0.0000	406.00	6071.0	0.0054 AMC	Ү	N
2389	12.000	92.000	507.00	0.0000	2650.0	0.0172 AMC	Ү	N
2390	12.000	92.000	908.00	0.0000	2650.0	0.0213 AMC	Ү	N
2391	12.000	92.000	1316.0	0.0000	2650.0	0.0236 AMC	Ү	N
2392	12.000	92.000	1494.0	0.0000	2650.0	0.0310 AMC	Ү	N
2393	12.000	92.000	1323.0	0.0000	2650.0	0.0299 AMC	Ү	N
2394	12.000	92.000	1229.0	0.0000	2650.0	0.0303 AMC	Y	N
2395	12.000	92.000	703.00	0.0000	2650.0	0.0224 AMC	Y	N
2396	12.000	92.000	327.00	11.000	2650.0	0.0180 AMC	Y	N
2397	12.000	92.000	103.00	0.0000	2650.0	0.0070 AMC	Ү	N
2398	12.000	92.000	66.000	0.0000	2650.0	0.0059 AMC	Ү	N
2399	12.000	92.000	54.000	0.0000	2650.0	0.0058 AMC	Ү	N

2400 2401	12.000	92.000 92.000	260.00 91.000	0.0000 241.00	2650.0 3952.0	0.0069 AMC 0.0133 AMC	Y Y	N N
2402	13.000	92.000	699.00	3.0000	3952.0	0.0179 AMC	. Y	N
2403	13.000	92.000	831.00	0.0000	3952.0	0.0197 AMC		N
2404	13.000	92.000	908.00	0.0000	3952.0	0.0177 AMC		N
2405 2406	13.000 13.000	92.000 92.000	670.00 561.00	0.0000 0.0000 30.000	3952.0 3952.0	0.0179 AMC 0.0168 AMC	. Y	N N
2407 2408 2409	13.000 13.000 13.000	92.000 92.000 92.000	291.00 115.00 10.000	77.000 220.00	3952.0 3952.0 3952.0	0.0130 AMC 0.0107 AMC 0.0113 AMC	. Y	N N N
2410 2411	13.000 13.000	92.000 92.000	0.0000	402.00 215.00	3952.0 3952.0	0.0115 AMC 0.0000 AMC	Y Y	N N
2412	13.000	92.000	69.000	149.00	3952.0	0.0107 AMC	. Y	N
2413	14.000	92.000	94.000	153.00	6474.0	0.0060 AMC		N
2414	14.000	92.000	307.00	0.0000	6474.0	0.0071 AMC		N
2415 2416	14.000 14.000	92.000 92.000	613.00 704.00	0.0000	6474.0 6474.0	0.0097 AMO	. Y	N N
2417	14.000	92.000	390.00	0.0000	6474.0	0.0108 AMC	. Y	N
2418	14.000	92.000	318.00	0.0000	6474.0	0.0089 AMC		N
2419	14.000	92.000	95.000	34.000	6474.0	0.0083 AMC		N
2420	14.000	92.000	4.0000	146.00	6474.0	0.0070 AMC	Y	N
2421	14.000	92.000	10.000	136.00	6474.0	0.0060 AMC	Y	N
2422	14.000	92.000	0.0000	320.00	6474.0	0.0063 AMC	Y Y	N
2423	14.000	92.000	65.000	335.00	6474.0	0.0060 AMC		N
2424	14.000	92.000	0.0000	278.00	6474.0	0.0550 AMC		N
2425 2426	1.0000	91.000 91.000	226.00 464.00	61.000 0.0000	5665.0 5665.0	0.0097 AMO	Y	N N
2427	1.0000	91.000	699.00	0.0000	5665.0	0.0240 AMC	Y	N
2428	1.0000	91.000	920.00	0.0000	5665.0	0.0302 AMC		N
2429	1.0000	91.000	684.00	0.0000	5665.0	0.0200 AMC		N
2430 2431	1.0000	91.000 91.000	570.00 298.00	2.0000 31.000	5665.0 5665.0	0.0244 AMC 0.0156 AMC	. Y	N N
2432	1.0000	91.000	65.000	190.00	5665.0	0.0110 AMC	. Y	N
2433	1.0000	91.000	22.000	235.00	5665.0	0.0094 AMC		N
2434	1.0000	91.000	0.0000	389.00	5665.0	0.0101 AMC		N
2435 2436 2437	1.0000	91.000 91.000 91.000	0.0000 70.000 65.000	344.00 122.00 238.00	5665.0 5665.0 2950.0	0.0064 AMC 0.0142 AMC	. Y	N N
2437 2438 2439	2.0000 2.0000 2.0000	91.000 91.000 91.000	152.00 280.00	24.000 21.000	2950.0 2950.0 2950.0	0.0088 AMC 0.0124 AMC 0.0158 AMC	. Y	N N N
2440	2.0000	91.000	432.00	0.0000	2950.0	0.0184 AMC	. Y	N
2441	2.0000	91.000	293.00	20.000	2950.0	0.0148 AMC		N
2442	2.0000	91.000	185.00	52.000	2950.0	0.0146 AMC		N
2443 2444	2.0000	91.000 91.000	34.000 0.0000	118.00 356.00	2950.0 2950.0 2950.0	0.0065 AMC 0.0065 AMC	Y Y	N N
2445	2.0000	91.000	0.0000	426.00	2950.0	0.0067 AMC	. Y	N
2446	2.0000	91.000	0.0000	584.00	2950.0	0.0069 AMC		N
2447	2.0000	91.000	0.0000	531.00	2950.0	0.0070 AMC		N
2448	2.0000	91.000	0.0000	379.00	2950.0	0.0052 AMC	Y	
2449	3.0000	91.000	186.00	84.000	3405.0	0.0117 AMC	Y	
2450	3.0000	91.000	461.00	0.0000	3405.0	0.0195 AMC	Y Y	N
2451	3.0000	91.000	669.00	0.0000	3405.0	0.0237 AMC		N
2452	3.0000	91.000	888.00	0.0000	3405.0	0.0308 AMC		N
2453	3.0000	91.000	687.00	0.0000	3405.0	0.0248 AMC	Y	N
2454	3.0000	91.000	585.00	1.0000	3405.0	0.0235 AMC	Y	N
2455	3.0000	91.000	322.00	22.000	3405.0	0.0161 AMC	. Y	N
2456	3.0000	91.000	74.000	187.00	3405.0	0.0086 AMC		N
2457	3.0000	91.000	10.000	153.00	3405.0	0.0091 AMC		N
2458	3.0000	91.000	0.0000	396.00	3405.0	0.0098 AMC	. Y	N
2459	3.0000	91.000	0.0000	365.00	3405.0	0.0097 AMC		N
2460	3.0000	91.000	59.000	132.00	3405.0	0.0085 AMC		N
2461	4.0000	91.000	673.00	0.0000	4460.0	0.0148 AMC	Y	N
2462	4.0000	91.000	834.00		4460.0	0.0212 AMC	Y	N
2463	4.0000	91.000	1421.0	0.0000	4460.0	0.0234 AMC	. Y	N
2464	4.0000	91.000	0.0000	0.0000	4460.0	0.0268 AMC		N
2465	4.0000	91.000	0.0000	0.0000	4460.0	0.0194 AMC		N
2466 2467	4.0000 4.0000	91.000 91.000	0.0000	0.0000	4460.0 4460.0	0.0200 AMC 0.0161 AMC	Y Y	N N
2468	4.0000	91.000	0.0000	0.0000	4460.0	0.0123 AMC	Y	N
2469	4.0000	91.000	277.00	1.0000	4460.0	0.0084 AMC		N
2470	4.0000	91.000	23.000	128.00	4460.0	0.0076 AMC		N

2471 24773 24774 24775 24776 24777 24778 24881 24884 24886 24887 24889 24993 24993 24993 24993 24993 24993 24996 25003 25505 25505 25511 25512 25513 25522 25523 25523 25523 2553 2553 25	4.0000 4.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 6.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 8.0000 9.0000	91.000 91.000	0.0000 0.0000 0.0000 0.0000 1099.0 1756.0 1881.0 1169.0 666.00 0.0000 12.000 17.000 294.00 309.00 605.00 1028.0 1243.0 887.00 739.00 335.00 168.00 2.0000 0.0000 1.0000 1.0000 1.49.00 425.00 352.00 154.00 403.00 149.00 89.000 0.000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 116.00 133.00 186.00 26.000 1.0000 0.0000 0.0000 0.0000 10.000 10.000 138.00 277.00 318.00 245.00 143.00 159.00 245.00 143.00 159.00 20.000 3.0000 0.0000	4460.0 4460.0 3302.0 3302.0 3302.0 3302.0 3302.0 3302.0 3302.0 3302.0 3302.0 3302.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 2088.0 3208.0 32	0.0077 AMC 0.0071 AMC 0.0294 AMC 0.0333 AMC 0.0436 AMC 0.0415 AMC 0.0349 AMC 0.0287 AMC 0.0287 AMC 0.0283 AMC 0.0211 AMC 0.0269 AMC 0.0269 AMC 0.0334 AMC 0.0334 AMC 0.0355 AMC 0.0375 AMC 0.0177 AMC 0.0177 AMC 0.0177 AMC 0.0112 AMC 0.0137 AMC 0.0139 AMC 0.0117 AMC 0.0139 AMC 0.0117 AMC 0.0139 AMC 0.0069 AMC 0.0067 AMC 0.0082 AMC 0.0175 AMC 0.0083 AMC 0.0139 AMC 0.0139 AMC 0.0139 AMC 0.0139 AMC 0.0149 AMC 0.0149 AMC 0.0149 AMC 0.0149 AMC 0.0155 AMC 0.0155 AMC 0.0155 AMC 0.0155 AMC 0.0067 AMC 0.0067 AMC 0.0067 AMC 0.0153 AMC 0.0155 AMC 0.0155 AMC 0.0075 AMC 0.0063 AMC 0.0155 AMC 0.0075 AMC 0.0067 AMC 0.0063 AMC 0.0075 AMC 0.0067 AMC 0.0063 AMC 0.0155 AMC 0.0075 AMC 0.0063 AMC 0.0155 AMC 0.0075 AMC 0.0063 AMC 0.0144 AMC 0.0224 AMC 0.0248 AMC 0.0248 AMC	λ	
2531	9.0000	91.000	0.0000	489.00	2766.0	0.0063 AMC	Y	N
2532	9.0000	91.000	65.000	233.00	2766.0	0.0055 AMC	Y	N
2533	10.000	91.000	217.00	85.000	4193.0	0.0078 AMC	Y	N
2534	10.000	91.000	486.00	1.0000	4193.0	0.0146 AMC	Y	N

2542 2543 2544 2545 2546 2547 2548	10.000 10.000 10.000 11.000 11.000 11.000	91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 90.000 2.0000 173.00 447.00 324.00	357.00 232.00 126.00 165.00 17.000 0.0000	4193.0 4193.0 4193.0 5914.0 5914.0 5914.0	0.0083 AMC 0.0068 AMC 0.0099 AMC 0.0063 AMC 0.0066 AMC 0.0100 AMC 0.01098 AMC	Y Y Y Y Y Y	N N N N N
2549 2550 2551 2552 2553 2554 2555 2556	11.000 11.000 11.000 11.000 11.000 11.000 11.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	140.00 372.00 134.00 81.000 0.0000 0.0000 0.0000	5.0000 0.0000 14.000 59.000 154.00 369.00 420.00 383.00	5914.0 5914.0 5914.0 5914.0 5914.0 5914.0 5914.0	0.0078 AMC 0.0088 AMC 0.0068 AMC 0.0059 AMC 0.0056 AMC 0.0066 AMC 0.0064 AMC 0.0068 AMC	Y Y Y Y Y Y Y	N N N N N N
2557 2558 2559 2560 2561 2562 2563 2564	12.000 12.000 12.000 12.000 12.000 12.000 12.000 12.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	508.00 786.00 1144.0 990.00 538.00 243.00 41.000 3.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 101.00 182.00	2641.0 2641.0 2641.0 2641.0 2641.0 2641.0 2641.0	0.0187 AMC 0.0234 AMC 0.0281 AMC 0.0264 AMC 0.0246 AMC 0.0159 AMC 0.0067 AMC 0.0066 AMC	Y Y Y Y Y Y Y	N N N N N N
2565 2566 2567 2568 2569 2570 2571	12.000 12.000 13.000 13.000 13.000 13.000 13.000	91.000 91.000 91.000 91.000 91.000 91.000	22.000 290.00 307.00 428.00 946.00 1131.0 695.00	0.0000 0.0000 17.000 5.0000 0.0000 0.0000	2641.0 2641.0 2641.0 3911.0 3911.0 3911.0	0.0056 AMC 0.0071 AMC 0.0120 AMC 0.0169 AMC 0.0206 AMC 0.0230 AMC 0.0191 AMC	Y Y Y Y Y Y	N N N N N
2572 2573 2574 2575 2576 2577 2578 2579	13.000 13.000 13.000 13.000 13.000 13.000 13.000 14.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	505.00 179.00 35.000 0.0000 0.0000 0.0000 91.000 35.000	10.000 34.000 232.00 383.00 419.00 383.00 241.00 57.000	3911.0 3911.0 3911.0 3911.0 3911.0 3911.0 3911.0	0.0169 AMC 0.0128 AMC 0.0134 AMC 0.0154 AMC 0.0155 AMC 0.0149 AMC 0.0138 AMC 0.0056 AMC	Y Y Y Y Y Y Y	N N N N N N
2580 2581 2582 2583 2584 2585 2586 2587	14.000 14.000 14.000 14.000 14.000 14.000 14.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000	344.00 770.00 556.00 287.00 459.00 244.00 185.00 46.000	0.0000 0.0000 0.0000 0.0000 1.0000 14.000 66.000	3911.0 6474.0 6474.0 6474.0 6474.0 6474.0 6474.0 6474.0	0.0060 AMC 0.0109 AMC 0.0125 AMC 0.0098 AMC 0.0095 AMC 0.0101 AMC 0.0081 AMC 0.0074 AMC	Y Y Y Y Y Y Y	N N N N N N
2588 2589 2590 2591 2592 2593 2594 2595	14.000 14.000 14.000 81.000 81.000 81.000 81.000	91.000 91.000 91.000 94.000 94.000 94.000 94.000	0.0000 0.0000 3.0000 679.00 969.00 1011.0 1059.0 941.00	248.00 205.00 224.00 0.0000 0.0000 0.0000 0.0000	6474.0 6474.0 6474.0 5735.0 5735.0 5735.0 5735.0	0.0060 AMC 0.0058 AMC 0.0062 AMC 0.0146 AFA 0.0181 AFA 0.0185 AFA 0.0185 AFA 0.0181 AFA	Y Y Y N N N	N N
2596 2597 2598 2599 2600 2601 2602	81.000 81.000 81.000 81.000 81.000 81.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000	808.00 651.00 291.00 5.0000 34.000 32.000 197.00	0.0000 0.0000 0.0000 137.00 80.000 118.00 13.000	5735.0 5735.0 5735.0 5735.0 5735.0 5735.0 5735.0	0.0167 AFA 0.0157 AFA 0.0120 AFA 0.0067 AFA 0.0084 AFA 0.0079 AFA 0.0092 AFA	N N N N N	N N N N N
2603 2604 2605 2606 2607 2608 2609 2610 2611	81.000 81.000 81.000 81.000 81.000 81.000 81.000 81.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	421.00 958.00 1034.0 1185.0 1019.0 889.00 677.00 407.00	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	5813.0 5813.0 5813.0 5813.0 5813.0 5813.0 5813.0 5813.0 5813.0	0.0130 AFA 0.0168 AFA 0.0196 AFA 0.0196 AFA 0.0178 AFA 0.0177 AFA 0.0147 AFA 0.0124 AFA 0.0076 AFA	N N N N N N N	N N N N N N N
2612	81.000	93.000	14.000	93.000	5813.0	0.0073 AFA	N	N

2613 2614	81.000 81.000	93.000 93.000	82.000 339.00	28.000	5813.0 5813.0	0.0078		N	N
2615	81.000	92.000	650.00	0.0000	5682.0	0.0144	AFA	N N	N N
2616 2617	81.000 81.000	92.000 92.000	1054.0 1142.0	0.0000	5682.0 5682.0	0.0184	AFA	N N	N N
2618 2619	81.000 81.000	92.000 92.000	1148.0 939.00	0.0000	5682.0 5682.0	0.0195		N N	N N
2620	81.000	92.000	930.00	0.0000	5682.0	0.0169	AFA	N	N
2621 2622	81.000 81.000	92.000 92.000	569.00 446.00	0.0000	5682.0 5682.0	0.0140		N N	N N
2623 2624	81.000 81.000	92.000 92.000	271.00 83.000	0.0000 53.000	5682.0 5682.0	0.0088		N N	N N
2625	81.000	92.000	79.000	71.000	5682.0 5682.0	0.0086	AFA	N	N
2626 2627	81.000 81.000	92.000 91.000	148.00 621.00	23.000	5572.0	0.0098 0.0144	AFA	N N	N N
2628 2629	81.000 81.000	91.000 91.000	783.00 1333.0	0.0000	5572.0 5572.0	0.0158 0.0194		N N	N N
2630	81.000	91.000	1269.0	0.0000	5572.0	0.0207	AFA	N	N
2631 2632	81.000 81.000	91.000 91.000	921.00 991.00	0.0000	5572.0 5572.0	0.0158 0.0169		N N	N N
2633 2634	81.000 81.000	91.000 91.000	821.00 487.00	0.0000	5572.0 5572.0	0.0150		N N	N N
2635	81.000	91.000	39.000	29.000	5572.0	0.0065	AFA	N	N
2636 2637	81.000 81.000	91.000 91.000	100.00 105.00	43.000 9.0000	5572.0 5572.0	0.0077 0.0081	AFA	N N	N N
2638 2639	81.000 82.000	91.000 94.000	340.00 0.0000	0.0000	5572.0 1804.0	0.0104 0.0096		N N	N N
2640	82.000	94.000	0.0000	0.0000	1804.0	0.0128	AFDW	N	N
2641 2642	82.000 82.000	94.000 94.000	0.0000	0.0000	1804.0 1804.0	0.0168			N N
2643 2644	82.000 82.000	94.000 94.000	0.0000	0.0000	1804.0 1804.0	0.0173			N N
2645 2646	82.000 82.000	94.000	0.0000	0.0000	1804.0	0.0129	AFDW	N	N
2647	82.000	94.000 94.000	0.0000	0.0000	1804.0 1804.0	0.0109	AFDW	N	N N
2648 2649	82.000 82.000	94.000 94.000	0.0000	0.0000	1804.0 1804.0	0.0119			N N
2650 2651	82.000 82.000	94.000 93.000	0.0000	0.0000	1804.0 2911.0	0.0102 0.0110	AFDW	N	N N
2652	82.000	93.000	0.0000	0.0000	2911.0	0.0144	AFDW	N	N
2653 2654	82.000 82.000	93.000 93.000	0.0000	0.0000	2911.0 2911.0	0.0166			N N
2655 2656	82.000 82.000	93.000 93.000	0.0000	0.0000	2911.0 2911.0	0.0154 0.0150			N N
2657	82.000	93.000	0.0000	0.0000	2911.0	0.0122	AFDW	N	N
2658 2659	82.000 82.000	93.000 93.000	0.0000	0.0000	2911.0 2911.0	0.0098 0.0107			N N
2660 2661	82.000 82.000	93.000 93.000	0.0000	0.0000	2911.0 2911.0	0.0115			N N
2662	82.000	93.000	0.0000	0.0000	2911.0	0.0111	AFDW	N	N
2663 2664	82.000 82.000	92.000 92.000	0.0000	0.0000	2911.0 2911.0	0.0106 0.0133			N N
2665 2666	82.000 82.000	92.000 92.000	0.0000	0.0000	2911.0 2911.0	0.0176 0.0177			N N
2667	82.000	92.000	0.0000	0.0000	2911.0	0.0170	AFDW	N	N
2668 2669	82.000 82.000	92.000 92.000	0.0000	0.0000	2911.0 2911.0	0.0157 0.0127	AFDW	N	N N
2670 2671	82.000 82.000	92.000 92.000	0.0000	0.0000	2911.0 2911.0	0.0099			N N
2672	82.000 82.000	92.000	0.0000	0.0000	2911.0	0.0102	AFDW	N	N
2673 2674	82.000	92.000 92.000	0.0000	0.0000	2911.0 2911.0	0.0099	AFDW	N	N N
2675 2676	82.000 82.000	91.000 91.000	0.0000	0.0000	2911.0 2911.0	0.0101			N N
2677 2678	82.000 82.000	91.000 91.000	0.0000	0.0000	2911.0 2911.0	0.0160 0.0187			N
2679	82.000	91.000	0.0000	0.0000	2911.0	0.0170	AFDW	N	N N
2680 2681	82.000 82.000	91.000 91.000	0.0000	0.0000	2911.0 2911.0	0.0157 0.0111			N N
2682 2683	82.000 82.000	91.000 91.000	0.0000	0.0000	2911.0 2911.0	0.0103 0.0123	AFDW	N	N N
								-	

2684 2685 2687 2688 2689 2690 2691 2692 2693 2694 2699 2700 2701 2702 2703 2704 2705 2706 2707 2708 2707 2718 2714 2715 2716 2717 2718 2719 2721 2722 2723 2724 2725 2726 2737 2738 2738 2739 2731 2722 2733 2740 2733 2740 2735 2736 2737 2738 2739 2730 2731 2732 2733 2740 2736 2737 2738 2738 2739 2739 2730 2731 2732 2733 2740 2741 2742 2738 2739 2740 2741 2742 2743 2744 2745 2746 2747 2748 2749 2748 2749 2749 2749 2749 2749 2749 2749 2749 2749 2749 2749 2749 2749 2740 2741 2742 2743 2744 2745 2746 2747 2748 2749 2749 2749 2749 2744 2745 2746 2747 2748 2749 2749 2749 2749 2749 2749 2749 2749 2740 2741 2742 2743 2744 2745 2746 2747 2748 2749 2749 2749 2749 2749 2749 2749 2749 2740 2741 2742 2743 2744 2744 2745 2746 2747 2748 2749	82.000 82.000 83.000	91.000 91.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 93.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 0.0000 37.000 198.00 280.00 474.00 251.00 166.000 1.0000 0.0000	0.0000 0.0000 170.00 41.000 0.0000 170.00 41.000 0.0000 18.000 110.00 264.00 464.00 453.00 464.00 0.0000	2911.0 2911.0 2911.0 2772.0 2772.0 2772.0 2772.0 2772.0 2772.0 2772.0 2772.0 2772.0 2772.0 2630.0 2650.0	0.0110 AFDW N N 0.0102 AFDW N N 0.0102 AFDW N N 0.0104 AFDW N N 0.0074 SOC Y N 0.0085 SOC Y N 0.0101 SOC Y N 0.0117 SOC Y N 0.0087 SOC Y N 0.0087 SOC Y N 0.0094 SOC Y N 0.00994 SOC Y N 0.00991 SOC Y N 0.00992 SOC Y N 0.0091 SOC Y N 0.0092 SOC Y N 0.0095 SOC Y N 0.0065 SOC Y N 0.0075 SOC Y N 0.0088 SOC Y N 0.0088 SOC Y N 0.0088 SOC Y N 0.0085 SOC Y N 0.0085 SOC Y N 0.0085 SOC Y N 0.0085 SOC Y N 0.0086 SOC Y N 0.0087 SOC Y N 0.0088 SOC Y N 0.0088 SOC Y N 0.0089 SOC Y N 0.0080 SOC Y N 0.0081 SOC Y N 0.0082 SOC Y N 0.0083 SOC Y N 0.0085 SOC Y N 0.0086 SOC Y N 0.0086 SOC Y N 0.0087 SOC Y N 0.0088 SOC Y N 0.0089 SOC Y N 0.0080 SOC Y N 0.0081 SOC Y N 0.0085 SOC Y N 0.0085 SOC Y N 0.0086 SOC Y N 0.0071 SOC Y N 0.0069 SOC Y N 0.0069 SOC Y N 0.0065 SOC Y N 0.0071 SOC Y N 0.0065 SOC Y N 0.0000 SOC Y N 0.01131 SPC N N 0.1291 AFMC N N
2745	67.000	94.000	0.0000	243.00	2652.0	0.0897 AFMC N N
2746	67.000	94.000	0.0000	242.00	2652.0	0.1291 AFMC N N
2747	67.000	94.000	0.0000	230.00	2652.0	0.1166 AFMC N N
2748	67.000	94.000	49.000	79.000	2652.0	0.0814 AFMC N N

2784 70.000 94.000 0.0000 339.00 8366.0 0.0114 AFMC Y N N 2785 71.000 94.000 114.00 61.000 12890.0 0.0156 AFMC Y Y Y 2786 71.000 94.000 450.00 7.0000 12890.0 0.0246 AFMC Y Y Y 2787 71.000 94.000 0.0000 0.0000 12890.0 0.0269 AFMC Y Y Y 2788 71.000 94.000 0.0000 0.0000 12890.0 0.0258 AFMC Y Y Y 2799 71.000 94.000 0.0000 0.0000 12890.0 0.0237 AFMC Y Y Y 2791 71.000 94.000 0.0000 0.0000 12890.0 0.0162 AFMC Y Y Y 2792 71.000 94.000 0.0000 0.0000 12890.0 0.0162 AFMC Y Y Y 2793 71.000 94.000 29.000 220.00 12890.0 0.0087 AFMC Y Y	2784 70.000 94.000 0.0000 339.00 8366.0 0.0114 AFMC Y N N 2785 71.000 94.000 114.00 61.000 12890.0 0.0156 AFMC Y Y Y 2786 71.000 94.000 450.00 7.0000 12890.0 0.0246 AFMC Y Y Y 2787 71.000 94.000 0.0000 0.0000 12890.0 0.0258 AFMC Y Y Y 2788 71.000 94.000 0.0000 0.0000 12890.0 0.0258 AFMC Y Y Y 2789 71.000 94.000 0.0000 0.0000 12890.0 0.0237 AFMC Y Y Y 2790 71.000 94.000 0.0000 0.0000 12890.0 0.0212 AFMC Y Y Y 2791 71.000 94.000 0.0000 0.0000 12890.0 0.0162 AFMC Y Y Y 2793 71.000 94.000 29.000 220.00 12890.0 0.0109 AFMC Y Y Y 2794 71.000 94.000 8.0000 406.00 12890.0 0.0086 AFMC Y Y Y 2795 71.000	2784 70.000 94.000 0.0000 339.00 8366.0 0.0114 AFMC Y N N 2785 71.000 94.000 114.00 61.000 12890.0 0.0156 AFMC Y Y Y 2786 71.000 94.000 450.00 7.0000 12890.0 0.0246 AFMC Y Y Y 2787 71.000 94.000 0.0000 0.0000 12890.0 0.0269 AFMC Y Y Y 2788 71.000 94.000 0.0000 0.0000 12890.0 0.0258 AFMC Y Y Y 2790 71.000 94.000 0.0000 0.0000 12890.0 0.0237 AFMC Y Y Y 2791 71.000 94.000 0.0000 0.0000 12890.0 0.0212 AFMC Y Y Y 2792 71.000 94.000 0.0000 0.0000 12890.0 0.0162 AFMC Y Y Y 2793 71.000 94.000 0.0000 0.0000 12890.0 0.0162 AFMC Y Y Y 2794 71.000 94.000 8.0000 406.00 12890.0 0.0086 AFMC Y Y Y 2795 71.000	2755 2756 2757 2758 2759 2760 2761 2762 2763 2764 2765 2766 2767 2768 2770 2771 2772 2773 2774 2775 2776 2777 2778 2777 2778 2779 2780 2781 2782 2783	68.000 68.000 68.000 68.000 68.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000 70.000 70.000 70.000 70.000 70.000 70.000	94.000 94.000	28.000 10.000 0.0000 0.0000 0.0000 95.000 384.00 582.00 591.00 541.00 239.00 154.00 65.000 3.0000 0.0000 0.0000 49.000 259.00 463.00 529.00 242.00 179.00 36.000 0.0000 0.0000 0.0000	183.00 593.00 715.00 659.00 410.00 40.000 0.0000 0.0000 0.0000 0.0000 60.000 144.00 444.00 444.00 453.00 252.00 155.00 40.000 0.0000 10.000 31.000 140.00 277.00 442.00 443.00 443.00 442.00 4453.00	2081.0 2081.0 2081.0 2081.0 2081.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 8366.0 8366.0 8366.0 8366.0 8366.0 8366.0 8366.0 8366.0 8366.0 8366.0	0.0132 0.0141 0.0133 0.0128 0.0143 0.0121 0.0070 0.0119 0.0241 0.0177 0.0146 0.0124 0.0105 0.0101 0.0114 0.0103 0.0097 0.0121 0.0151 0.0151 0.0163 0.0151 0.0163 0.0151 0.0126 0.0106 0.0119 0.0112	AFMC N AFMC N AFMC N AFMC Y	
	2795 71.000 94.000 0.0000 395.00 12890.0 0.0089 AFMC Y Y Y 2796 71.000 94.000 41.000 147.00 12890.0 0.0080 AFMC Y Y Y 2797 72.000 94.000 98.000 245.00 16376.0 0.0080 AFMC N Y Y 2798 72.000 94.000 298.00 26.000 16376.0 0.0104 AFMC N Y Y 2800 72.000 94.000 370.00 8.0000 16376.0 0.0109 AFMC N Y Y 2801 72.000 94.000 284.00 27.000 16376.0 0.0125 AFMC N Y Y 2802 72.000 94.000 137.00 82.000 16376.0 0.0108 AFMC N Y 2803 72.000 94.000 137.00 82.000 16376.0 0.0108 AFMC N Y 2804 72.000 94.000 297.00 16376.0 0.0085 AFMC N Y	2795 71.000 94.000 0.0000 395.00 12890.0 0.0089 AFMC Y Y Y 2796 71.000 94.000 41.000 147.00 12890.0 0.0080 AFMC Y Y Y 2797 72.000 94.000 98.000 245.00 16376.0 0.0080 AFMC N Y Y 2798 72.000 94.000 298.00 26.000 16376.0 0.0104 AFMC N Y Y 2799 72.000 94.000 300.00 23.000 16376.0 0.0109 AFMC N Y Y 2800 72.000 94.000 370.00 8.0000 16376.0 0.0109 AFMC N Y Y 2800 72.000 94.000 370.00 8.0000 16376.0 0.0125 AFMC N Y Y 2800 72.000 94.000 284.00 27.000 16376.0 0.0125 AFMC N Y Y 2800 72.000 94.000 137.00 82.000 16376.0 0.0125 AFMC N Y Y 2803 72.000 94.000 137.00 82.000 16376.0 0.0101 AFMC N Y Y 2803 72.000 94.000 12.000 297.00 16376.0 0.0085 AFMC N Y Y 2803 72.000 94.000 12.000 297.00 16376.0 0.0085 AFMC N Y Y 2805 72.000 94.000 0.0000 515.00 16376.0 0.0085 AFMC N Y Y 2805 72.000 94.000 0.0000	2785 2786 2787 2788 2789 2790 2791 2792 2793	71.000 71.000 71.000 71.000 71.000 71.000 71.000 71.000 71.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	114.00 450.00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 29.000	61.000 7.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 220.00	12890.0 12890.0 12890.0 12890.0 12890.0 12890.0 12890.0 12890.0	0.0156 0.0246 0.0269 0.0258 0.0237 0.0212 0.0162 0.0109 0.0087	AFMC Y	Y Y Y Y Y Y Y

2886 79.000 94.000 382.00 22.000 14979.0 0.0157 AFMC N Y 2887 79.000 94.000 188.00 66.000 14979.0 0.0166 AFMC N Y	2826 2827 2828 2832 2833 2833 2833 2833 2833	74.000 74.000 74.000 74.000 74.000 74.000 74.000 75.000 75.000 75.000 75.000 75.000 75.000 75.000 75.000 76.000 76.000 76.000 76.000 76.000 76.000 77.000	94.000 94.000	989.00 580.00 377.00 53.000 0.0000 6.0000 0.0000	0.0000 0.0000 123.00 404.00 187.00 30.000 0.0000	3484.0 3484.0 3484.0 3484.0 3484.0 3484.0 3484.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0 1796.0 11796.0	0.0315 AFMC N N 0.0260 AFMC N N 0.0194 AFMC N N 0.0182 AFMC N N 0.0184 AFMC N N 0.0183 AFMC N N 0.0175 AFMC N N 0.0076 AFMC N N 0.0077 AFMC N N 0.0095 AFMC N N 0.0095 AFMC N N 0.0096 AFMC N N 0.0095 AFMC N N 0.0071 AFMC N N 0.0071 AFMC N N 0.0072 AFMC N N 0.0071 AFMC N Y 0.0068 AFMC N Y 0.0078 AFMC N Y 0.0132 AFMC N Y 0.0089 AFMC N Y 0.0082 AFMC N Y 0.0078 AFMC N Y 0.0078 AFMC N N 0.0237 AFMC N N 0.0238 AFMC N N 0.0244 AFMC N N 0.0255 AFMC N N 0.0279 AFMC N N 0.0279 AFMC N N 0.0279 AFMC N N 0.0270 AFMC N N 0.0271 AFMC N N 0.0221 AFMC N N 0.02221 AFMC N Y 0.0222 AFMC N Y 0.0231 AFMC N Y
	2878 2879 2880 2881 2882 2883 2884 2885	78.000 78.000 78.000 79.000 79.000 79.000 79.000 79.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 0.0000 245.00 559.00 670.00 889.00 0.0000	441.00 436.00 254.00 42.000 0.0000 0.0000 0.0000	11555.0 11555.0 11555.0 14979.0 14979.0 14979.0 14979.0	0.0103 AFMC N N 0.0097 AFMC N N 0.0089 AFMC N N 0.0143 AFMC N Y 0.0202 AFMC N Y 0.0231 AFMC N Y 0.2310 AFMC N Y 0.0157 AFMC N Y

2897 2898 2899 2900 2901 2902 2903 2904 2905 2906 2907 2908 2909 2910 2911 2912	80.000 80.000 80.000 80.000 80.000 80.000 80.000 67.000 67.000 67.000 67.000 67.000 67.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	1023.0 792.00 338.00 259.00 14.000 0.0000 0.0000 108.00 398.00 625.00 633.00 701.00 545.00 253.00 43.000	0.0000 0.0000 16.000 35.000 265.00 252.00 0.0000 21.000 3.0000 0.0000 0.0000 4.0000 4.0000 113.00	14689.0 14689.0 14689.0 14689.0 14689.0 14689.0 14689.0 2574.0 2574.0 2574.0 2574.0 2574.0 2574.0 2574.0	0.0314 AFM 0.0291 AFM 0.0211 AFM 0.0133 AFM 0.0129 AFM 0.0122 AFM 0.0122 AFM 0.1024 AFM 0.1024 AFM 0.1027 AFM 0.1027 AFM 0.0859 AFM 0.0759 AFM 0.0855 AFM 0.0865 AFM 0.1031 AFM	
2913 2914 2915 2916 2917 2918 2919 2920 2921 2922 2923 2924 2925 2926 2927	67.000 67.000 67.000 68.000 68.000 68.000 68.000 68.000 68.000 68.000 68.000 68.000 68.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	8.0000 0.0000 0.0000 53.000 0.0000 260.00 287.00 421.00 269.00 147.00 42.000 0.0000 0.0000 0.0000	256.00 441.00 389.00 115.00 267.00 34.000 24.000 1.0000 7.0000 45.000 117.00 283.00 503.00 660.00 698.00	2574.0 2574.0 2574.0 2574.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0	0.1090 AFM 0.0869 AFM 0.0823 AFM 0.1013 AFM 0.0140 AFM 0.0169 AFM 0.0182 AFM 0.0179 AFM 0.0160 AFM 0.0158 AFM 0.0158 AFM 0.0164 AFM 0.0162 AFM 0.0162 AFM	
2928 2929 2930 2931 2933 2933 2934 2935 2936 2937 2938 2939 2941	68.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	0.0000 52.000 423.00 669.00 653.00 484.00 212.00 14.000 21.000 0.0000 0.0000	503.00 53.000 0.0000 0.0000 0.0000 0.0000 22.000 131.00 315.00 404.00 478.00 243.00	1730.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0 6542.0	0.0143 AFM 0.0091 AFM 0.0128 AFM 0.0190 AFM 0.0207 AFM 0.0171 AFM 0.0149 AFM 0.0112 AFM 0.0106 AFM 0.0091 AFM 0.0099 AFM 0.0085 AFM 0.0084 AFM	
2941 2942 2943 2944 2945 2946 2947 2948 2949 2950 2951 2953 2953	70.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000 71.000 71.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	14.000 228.00 288.00 229.00 323.00 251.00 91.000 0.0000 0.0000 0.0000 0.0000 0.0000 317.00 969.00	98.000 33.000 11.000 6.0000 2.0000 8.0000 25.000 219.00 438.00 551.00 547.00 398.00 11.000 0.0000	7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 7812.0 12930.0	0.0117 AFM 0.0132 AFM 0.0162 AFM 0.0155 AFM 0.0158 AFM 0.0127 AFM 0.0127 AFM 0.0124 AFM 0.0128 AFM 0.0147 AFM 0.0142 AFM 0.0142 AFM 0.0142 AFM 0.0132 AFM	N N N N N N N N N N Y Y
2955 2956 2957 2958 2959 2960 2961 2962 2963 2964 2965 2966 2967	71.000 71.000 71.000 71.000 71.000 71.000 71.000 71.000 71.000 71.000 72.000 72.000 72.000	93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000 93.000	1200.0 1270.0 707.00 734.00 566.00 178.00 45.000 4.0000 114.00 1.0000 275.00 307.00	0.0000 0.0000 0.0000 0.0000 0.0000 70.000 56.000 117.00 179.00 61.000 225.00 29.000 24.000	12930.0 12930.0 12930.0 12930.0 12930.0 12930.0 12930.0 12930.0 12930.0 12930.0 16108.0 16108.0	0.0285 AFM 0.0296 AFM 0.0258 AFM 0.0232 AFM 0.0192 AFM 0.0124 AFM 0.0087 AFM 0.0081 AFM 0.0081 AFM 0.0082 AFM 0.0082 AFM 0.0076 AFM 0.0101 AFM	Y Y Y Y Y Y Y Y Y Y

2968 2970 2971 2977 2977 2977 2977 2977 2977 2977	72.000 72.000 72.000 72.000 72.000 72.000 72.000 72.000 73.000 73.000 73.000 73.000 73.000 73.000 73.000 73.000 74.000 74.000 74.000 74.000 74.000 74.000 74.000 75.000	93.000 93.000	431.00 270.00 158.00 43.000 0.0000 0.0000 0.0000 0.0000 128.00 752.00 991.00 778.00 624.00 496.00 238.00 69.000 3.0000 0.0000 15.000 401.00 664.00 974.00 1023.0 1083.0 871.00 444.00 112.00 35.000 0.0000	1.0000 9.0000 34.000 98.000 263.00 488.00 574.00 622.00 0.0000 5.0000 0.0000	16108.0 16108.0 16108.0 16108.0 16108.0 16108.0 16108.0 16108.0 16108.0 16108.0 6806.0 6806.0 6806.0 6806.0 6806.0 6806.0 6806.0 6806.0 3656.0	0.0133 AFMC N Y 0.0116 AFMC N Y 0.0107 AFMC N Y 0.0083 AFMC N Y 0.0083 AFMC N Y 0.0086 AFMC N Y 0.0081 AFMC N Y 0.0081 AFMC N Y 0.0081 AFMC N Y 0.0081 AFMC N N 0.0140 AFMC N N 0.0140 AFMC N N 0.0142 AFMC N N 0.0149 AFMC N N 0.0123 AFMC N N 0.0083 AFMC N N 0.0084 AFMC N N 0.0087 AFMC N N 0.0087 AFMC N N 0.0087 AFMC N N 0.0088 AFMC N N 0.0029 AFMC N N 0.0298 AFMC N N 0.0291 AFMC N N 0.0150 AFMC N N 0.0150 AFMC N N 0.0150 AFMC N N 0.0154 AFMC N N 0.0155 AFMC N N 0.0077 AFMC N N 0.0077 AFMC N Y 0.0083 AFMC N Y 0.0077 AFMC N Y 0.0084 AFMC N Y 0.0077 AFMC N N 0.0077 AFMC N Y 0.0077 AFMC N Y 0.0077 AFMC N Y 0.0077 AFMC N N 0.0077 AFMC N
3021	76.000	93.000	14.000	320.00	11431.0	0.0077 AFMC N Y 0.0082 AFMC N Y 0.0080 AFMC N Y 0.0070 AFMC N Y 0.0243 AFMC N N 0.0225 AFMC N N 0.0270 AFMC N N
3022	76.000	93.000	0.0000	418.00	11431.0	
3023	76.000	93.000	0.0000	377.00	11431.0	
3024	76.000	93.000	0.0000	302.00	11431.0	
3025	77.000	93.000	403.00	2.0000	868.00	
3026	77.000	93.000	600.00	0.0000	868.00	

3039 3040 3041 3042 3044 3044 3044 3045 3047 3055 3055 3055 3055 3055 3055 3055 3066 3066	78.000 78.000 78.000 78.000 78.000 78.000 78.000 78.000 78.000 79.000 79.000 79.000 79.000 79.000 79.000 79.000 80.000 80.000 80.000 80.000 80.000 80.000 80.000 80.000 67.000	93.000 93.000	514.00 421.00 460.00 330.00 139.00 6.0000 0.0000 0.0000 0.0000 117.00 573.00 780.00 892.00 736.00 540.00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 1103.0 826.00 444.00 990.00 1103.0 826.00 444.00 97.000 40.000 0.0000	0.0000 0.0000 0.0000 13.000 27.000 230.00 460.00 640.00 640.00 0.0000 0.	12107.0 12107.0 12107.0 12107.0 12107.0 12107.0 12107.0 12107.0 12107.0 13890.0 13890.0 13890.0 13890.0 13890.0 13890.0 13890.0 13890.0 14689.0 1699.0 1730.0	0.0191 AFMC N Y 0.0175 AFMC N Y 0.0172 AFMC N Y 0.0172 AFMC N Y 0.0110 AFMC N Y 0.01010 AFMC N Y 0.0102 AFMC N Y 0.0102 AFMC N Y 0.0105 AFMC N Y 0.0105 AFMC N Y 0.0107 AFMC N Y 0.0157 AFMC N Y 0.0230 AFMC N Y 0.0230 AFMC N Y 0.0279 AFMC N Y 0.0253 AFMC N Y 0.0253 AFMC N Y 0.0159 AFMC N N 0.0165 AFMC N Y 0.0166 AFMC N Y 0.0176 AFMC N N 0.0176 AFMC N N 0.0250 AFMC N N 0.0250 AFMC N N 0.0290 AFMC N N 0.0290 AFMC N N 0.0290 AFMC N N 0.0290 AFMC N N 0.0317 AFMC N N 0.0131 AFMC N N 0.0132 AFMC N N 0.0133 AFMC N N 0.0134 AFMC N N 0.0135 AFMC N N 0.0135 AFMC N N 0.0152 AFMC N N 0.0152 AFMC N N 0.0152 AFMC N N 0.0153 AFMC N N 0.0154 AFMC N N 0.0154 AFMC N N 0.0155 AFMC N N 0.0154 AFMC N N 0.0154 AFMC N N 0.0155 AFMC N N 0.0156 AFMC N N 0.0157 AFMC N N 0.0158 AFMC N N 0.0140 AFMC N N 0.0158 AFMC N N 0.0159 AFMC N N 0.0162 AFMC N N 0.0163 AFMC N N 0.0164 AFMC N N 0.0164 AFMC N N 0.0165 AFMC N N 0.0165 AFMC N N 0.0165 AFMC N N 0.0166 AFMC N N 0.0167 AFMC N N 0.0168 AFMC N N 0.0168 AFMC N N 0.0169 AFMC N N 0.0160 AFMC N N 0.0161 AFMC N N 0.0162 AFMC N N 0.0162 AFMC N N 0.0163 AFMC N N 0.0164 AFMC N N 0.0164 AFMC N N 0.0165 AFMC N N 0.0165 AFMC N N 0.0167 AFMC N N 0.0168 AFMC N N 0.0168 AFMC N N 0.0169 AFMC N N 0.0169 AFMC N N 0.0160 AFMC N N 0.0161 AFMC N N 0.0162 AFMC N N 0.0162 AFMC N N 0.0164 AFMC N N 0.0165 AFMC N N 0.0164 AFMC N N 0.0165 AFMC N N 0.0166 AFMC N N 0.0167 AFMC N N 0.0168 AFMC N N 0.0168 AFMC N N 0.0169 AFMC N
3093 3094 3095 3096 3097 3098	68.000 68.000 68.000 68.000 69.000	92.000 92.000 92.000 92.000 92.000 92.000	0.0000 0.0000 0.0000 0.0000 188.00 382.00	531.00 618.00 542.00 508.00 119.00 0.0000	1730.0 1730.0 1730.0 1730.0 6399.0 6399.0	0.0162 AFMC N N 0.0152 AFMC N N 0.0148 AFMC N N 0.0159 AFMC N N 0.0091 AFMC Y N 0.0109 AFMC Y N

3110 70.0 3111 70.0 3111 70.0 3112 70.0 3113 70.0 3114 70.0 3115 70.0 3116 70.0 3117 70.0 3118 70.0 3120 70.0 3121 71.0 3122 71.0 3123 71.0 3124 71.0 3125 71.0 3126 71.0 3127 71.0 3128 71.0 3129 71.0 3129 71.0 3130 71.0 3131 71.0	00 92.000 00 92.000	291.00 295.00 437.00 239.00 174.00 71.000 18.000 0.0000 0.0000 0.0000 392.00 823.00 1154.0 1211.0 797.00 562.00 299.00 103.00 60.000 25.000 25.000	22.000 16.000 6.0000 9.0000 14.000 85.000 217.00 415.00 527.00 439.00 359.00 1.0000 0.0000 0.0000 0.0000 11.000 46.000 154.00 31.000	7742.0 7742.0 7742.0 7742.0 7742.0 7742.0 7742.0 7742.0 7742.0 13134.0 13134.0 13134.0 13134.0 13134.0 13134.0	0.0161 AFMC Y N 0.0153 AFMC Y N 0.0170 AFMC Y N 0.0147 AFMC Y N 0.0150 AFMC Y N 0.0133 AFMC Y N 0.0131 AFMC Y N 0.0133 AFMC Y N 0.0134 AFMC Y N 0.0144 AFMC Y N 0.0126 AFMC Y N 0.0131 AFMC Y N 0.0131 AFMC Y N 0.0133 AFMC Y Y 0.0286 AFMC Y Y 0.0288 AFMC Y Y 0.0198 AFMC Y Y 0.0198 AFMC Y Y 0.0198 AFMC Y Y 0.0090 AFMC Y Y 0.0082 AFMC Y Y 0.0083 AFMC Y Y 0.0083 AFMC Y Y
3132 71.0 3133 72.0 3134 72.0 3135 72.0 3136 72.0 3137 72.0 3138 72.0 3139 72.0 3140 72.0 3141 72.0 3142 72.0 3143 72.0 3144 72.0 3145 73.0 3146 73.0 3147 73.0 3148 73.0 3148 73.0 3149 73.0 3150 73.0 3151 73.0	00 92.000 00 92.000	65.000 29.000 269.00 309.00 449.00 201.00 108.00 37.000 4.0000 0.0000 0.0000 0.0000 188.00 645.00 851.00 994.00 651.00 473.00 170.00	58.000 292.00 50.000 16.000 0.0000 12.000 39.000 123.00 252.00 501.00 592.00 505.00 463.00 25.000 0.0000 0.0000 0.0000 0.0000 27.000	13134.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0 6341.0 6341.0 6341.0 6341.0 6341.0	0.0083 AFMC Y Y 0.0102 AFMC N Y 0.0129 AFMC N Y 0.0132 AFMC N Y 0.0132 AFMC N Y 0.0164 AFMC N Y 0.0123 AFMC N Y 0.0112 AFMC N Y 0.0099 AFMC N Y 0.0099 AFMC N Y 0.0092 AFMC N Y 0.0097 AFMC N Y 0.0097 AFMC N Y 0.0091 AFMC N N 0.0079 AFMC N N 0.0182 AFMC N N 0.0182 AFMC N N 0.0183 AFMC N N 0.0142 AFMC N N 0.0142 AFMC N N 0.0142 AFMC N N 0.01099 AFMC N N 0.01099 AFMC N N
3152 73.0 3153 73.0 3154 73.0 3155 73.0 3156 73.0 3157 74.0 3158 74.0 3160 74.0 3161 74.0 3162 74.0 3163 74.0 3165 74.0 3166 74.0 3166 74.0 3167 74.0 3167 74.0 3170 75.0 3171 75.0 3172 75.0 3173 75.0 3174 75.0 3175 75.0 3177 75.0 3177 75.0 3177 75.0	00 92.000 00 92.000	53.000 5.0000 0.0000 0.0000 8.0000 274.00 576.00 885.00 1011.0 900.00 847.00 478.00 200.00 16.000 14.000 29.000 190.00 29.000 130.00 172.00 25.000 0.0000 3.0000	49.000 235.00 354.00 318.00 171.00 0.0000 0.0000 0.0000 0.0000 10.000 52.000 161.00 210.00 199.00 78.000 107.00 37.000 2.0000 5.0000 14.000 0.0000 5.0000 14.000 0.0000	6341.0 6341.0 6341.0 6341.0 6341.0 3391.0 3391.0 3391.0 3391.0 3391.0 3391.0 3391.0 3391.0 3391.0 1618.0 1618.0 1618.0 1618.0 1618.0 1618.0	0.0064 AFMC N N 0.0090 AFMC N N 0.0070 AFMC N N 0.0073 AFMC N N 0.0078 AFMC N N 0.0182 AFMC N N 0.0182 AFMC N N 0.0243 AFMC N N 0.0323 AFMC N N 0.0376 AFMC N N 0.0306 AFMC N N 0.0306 AFMC N N 0.0308 AFMC N N 0.0399 AFMC N N 0.0150 AFMC N N 0.0152 AFMC N N 0.0153 AFMC N N 0.0153 AFMC N N 0.0154 AFMC N N 0.0155 AFMC N N 0.0155 AFMC N N 0.0158 AFMC N N 0.0075 AFMC N N 0.0075 AFMC N N 0.0089 AFMC N N 0.0109 AFMC N N 0.0109 AFMC N N 0.0109 AFMC N N 0.0070 AFMC N N 0.0071 AFMC N N 0.0072 AFMC N N

3181 3182 3183 3184 3185 3186 3187 3188 3190 3191 3192 3193 3194 3195 3196 3197 3198 3199 3200 3201 3202 3203 3204 3205 3206 3207 3208 3207 3208 3211 3212 3213 3214 3215 3216 3217 3218 3219 3221 3222 3223 3224 3225 3226 3227 3228	76.000 76.000 76.000 76.000 76.000 76.000 76.000 76.000 76.000 76.000 77.000	92.000 92.000	71.000 226.00 510.00 610.00 253.00 204.00 64.000 0.0000 0.0000 0.0000 0.0000 296.00 714.00 878.00 1011.0 814.00 747.00 402.00 190.00 35.000 0.0000 8.0000 101.00 0.0000 355.00 0.0000 519.00 328.00 227.00 140.00 32.000 0.0000 519.00 328.00 0.0000 519.00 328.00 0.0000 519.00 328.00 0.0000 519.00 328.00 0.0000 519.00 328.00 0.0000 519.00 328.00 0.0000	252.00 1.0000 0.0000 0.0000 1.0000 45.000 305.00 297.00 457.00 457.00 23.000 0.0000 0.0000 0.0000 0.0000 15.00 272.00 152.00 99.000 115.00 272.00 152.00 99.000 101.00 23.000 0.0000 13.000 272.00 152.00 99.000 101.00 23.000 0.0000 0.0000 13.000 152.00 99.000 101.00 23.000 0.0000 23.000 0.0000 0.0000 14.000 23.000 0.0000 0.0000 0.0000 24.000 23.000 0.0000 0.0000 0.0000 0.0000 24.000 23.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 24.000 23.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 24.000 23.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 24.000 23.000 0.0000	11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 11431.0 868.00 868.00 868.00 868.00 868.00 868.00 868.00 868.00 11373.0	0.0080 0.0070 0.0156 0.0144 0.0129 0.0128 0.0088 0.0079 0.0073 0.0073 0.00250 0.0250 0.0251 0.0252 0.0252 0.0234 0.0242 0.0232 0.0100 0.0150 0.0181 0.0197 0.0164 0.0148 0.0118 0.0097 0.0103 0.0121 0.0105 0.0103 0.0121 0.0103 0.0242 0.0234 0.0100 0.0150 0.0164 0.0175 0.0103 0.0121 0.0105 0.0103 0.0242 0.0242 0.0242 0.0103 0.0121 0.0105 0.0103 0.0121 0.0105 0.0103 0.0121 0.0105 0.0103 0.0121 0.0105 0.0103 0.01242 0.0242 0.0243 0.0242 0.0243 0.0243 0.0105 0.0103 0.0121 0.0105 0.0103 0.0121 0.0105 0.0103 0.0121 0.0105 0.0103 0.0124 0.0242 0.0243 0.0242 0.0243 0.0246 0.0167 0.0167 0.0167 0.0168	AFMC I AF		
3219	79.000	92.000	549.00	0.0000	13678.0	0.0243	AFMC I	N Y	Z
3221	79.000	92.000	373.00	0.0000	13678.0	0.0230	AFMC I	Y Y	7
3224	79.000	92.000	63.000	127.00	13678.0	0.0167	AFMC I	N Y	Z
3226	79.000	92.000	0.0000	446.00	13678.0	0.0192	AFMC 1	N Y	Z
				203.00			AFMC I	N Y	
3230 3231	80.000	92.000 92.000 92.000	740.00 906.00	0.0000	14689.0 14689.0	0.0244 0.0292	AFMC I	N N	1
3232 3233	80.000	92.000 92.000	1060.0 814.00	0.0000	14689.0 14689.0	0.0316	AFMC I	N N	1
3234 3235	80.000	92.000 92.000	735.00 432.00	0.0000 12.000	14689.0 14689.0	0.0270 0.0231	AFMC I	N N	
3236 3237	80.000	92.000 92.000	237.00 65.000	29.000 63.000	14689.0 14689.0	0.0166	AFMC I	N N	1
3238 3239 3240	80.000 80.000 80.000	92.000 92.000 92.000	4.0000 17.000 136.00	257.00 257.00 67.000	14689.0 14689.0 14689.0	0.0138 0.0130 0.0124	AFMC I	N N	1
3241 3242	67.000 67.000	91.000 91.000	254.00 381.00	33.000 4.0000	2658.0 2658.0	0.0865	AFMC I	N N	1
3243 3244	67.000 67.000	91.000 91.000	608.00 769.00	4.0000	2658.0 2658.0	0.0717 0.0782	AFMC I	N N	
3245 3246 3247	67.000 67.000	91.000 91.000 91.000	701.00 432.00	0.0000 16.000 14.000	2658.0 2658.0	0.0557	AFMC I	N N	1
3248 3249	67.000 67.000 67.000	91.000 91.000 91.000	100.00 6.0000 0.0000	293.00 0.0000	2658.0 2658.0 2658.0	0.0745 0.0592 0.0528	AFMC I	N N	1
3250 3251	67.000 67.000	91.000 91.000	0.0000 7.0000	426.00 372.00	2658.0 2658.0	0.0451	AFMC I	N N	1

3252 3253 3254 3255 3256 3257 3258 3259 3260 3261	67.000 68.000 68.000 68.000 68.000 68.000 68.000 68.000 68.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	51.000 50.000 142.00 422.00 494.00 240.00 96.000 7.0000 0.0000	236.00 192.00 91.000 23.000 0.0000 10.000 70.000 234.00 402.00 541.00	2658.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0 1730.0	0.0448 AFMC N N 0.0127 AFMC N N 0.0152 AFMC N N 0.0178 AFMC N N 0.0178 AFMC N N 0.0156 AFMC N N 0.0151 AFMC N N 0.0163 AFMC N N 0.0152 AFMC N N 0.0143 AFMC N N	
3262 3263 3264 3265 3266 3267 3268 3269 3270 3271 3272 3273	68.000 68.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000 69.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 5.0000 74.000 385.00 867.00 686.00 379.00 507.00 260.00 134.00 0.0000	612.00 654.00 396.00 69.000 0.0000 0.0000 0.0000 0.0000 3.0000 64.000 279.00	1730.0 1730.0 1730.0 6352.0 6352.0 6352.0 6352.0 6352.0 6352.0 6352.0 6352.0	0.0147 AFMC N N 0.0143 AFMC N N 0.0130 AFMC N N 0.0096 AFMC Y N 0.0108 AFMC Y N 0.0197 AFMC Y N 0.0203 AFMC Y N 0.0176 AFMC Y N 0.0152 AFMC Y N 0.0157 AFMC Y N 0.0157 AFMC Y N 0.0121 AFMC Y N 0.0100 AFMC Y N	
3274 3275 3276 3277 3278 3279 3280 3281 3282 3283 3284	69.000 69.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 39.000 110.00 244.00 396.00 213.00 119.00 8.0000	0.0000 480.00 338.00 223.00 31.000 39.000 0.0000 10.000 46.000 197.00 394.00 0.0000	6352.0 6352.0 7686.0 7686.0 7686.0 7686.0 7686.0 7686.0 7686.0 7686.0 7686.0	0.0099 AFMC Y N 0.0086 AFMC Y N 0.0104 AFMC Y N 0.0120 AFMC Y N 0.0121 AFMC Y N 0.0150 AFMC Y N 0.0154 AFMC Y N 0.0138 AFMC Y N 0.0142 AFMC Y N 0.0114 AFMC Y N	
3285 3286 3287 3288 3289 3290 3291 3292 3293 3294 3295 3296	70.000 70.000 70.000 70.000 71.000 71.000 71.000 71.000 71.000 71.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 0.0000 332.00 714.00 1376.0 1255.0 806.00 762.00 592.00 350.00	0.0000 0.0000 408.00 9.0000 0.0000 0.0000 0.0000 0.0000 0.0000	7686.0 7686.0 7686.0 13222.0 13222.0 13222.0 13222.0 13222.0 13222.0	0.0134 AFMC Y N 0.0123 AFMC Y N 0.0133 AFMC Y N 0.0139 AFMC Y N 0.0137 AFMC Y Y 0.0217 AFMC Y Y 0.0291 AFMC Y Y 0.0301 AFMC Y Y 0.0222 AFMC Y Y 0.0230 AFMC Y Y 0.0130 AFMC Y Y 0.0154 AFMC Y Y	
3297 3298 3299 3300 3301 3302 3303 3304 3305 3306 3307	71.000 71.000 71.000 71.000 72.000 72.000 72.000 72.000 72.000 72.000 72.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	41.000 0.0000 0.0000 49.000 34.000 164.00 442.00 510.00 256.00 106.00 9.0000	106.00 385.00 353.00	13222.0 13222.0 13222.0 13222.0 14456.0 14456.0 14456.0 14456.0 14456.0 14456.0	0.0081 AFMC Y Y 0.0081 AFMC Y Y 0.0082 AFMC Y Y 0.0083 AFMC Y Y 0.0105 AFMC N Y 0.0117 AFMC N Y 0.0138 AFMC N Y 0.0165 AFMC N Y 0.0165 AFMC N Y 0.0131 AFMC N Y 0.0131 AFMC N Y 0.0100 AFMC N Y	
3308 3309 3310 3311 3312 3313 3314 3315 3316 3317 3318	72.000 72.000 72.000 72.000 72.000 73.000 73.000 73.000 73.000 73.000 73.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000	0.0000 0.0000 0.0000 0.0000 6.0000 202.00 811.00 1013.0 903.00 563.00 581.00	376.00 523.00 579.00 631.00 372.00 0.0000 0.0000 0.0000 0.0000 0.0000	14456.0 14456.0 14456.0 14456.0 14456.0 6341.0 6341.0 6341.0 6341.0 6341.0	0.0094 AFMC N Y 0.0099 AFMC N Y 0.0097 AFMC N Y 0.0099 AFMC N Y 0.0094 AFMC N Y 0.0073 AFMC N N 0.0150 AFMC N N 0.0150 AFMC N N 0.01218 AFMC N N 0.0173 AFMC N N 0.01740 AFMC N N	
3319 3320 3321 3322	73.000 73.000 73.000 73.000	91.000 91.000 91.000 91.000	263.00 60.000 12.000 0.0000	0.0000 87.000 269.00 375.00	6341.0 6341.0 6341.0 6341.0	0.0121 AFMC N N 0.0077 AFMC N N 0.0066 AFMC N N 0.0069 AFMC N N	ſ

3323 3324	73.000 73.000	91.000 91.000	0.0000	331.00 120.00	6341.0 6341.0	0.0070 AFMC N N 0.0082 AFMC N N
3325	74.000	91.000	255.00	30.000	3391.0	0.0002 AFMC N N
3326	74.000	91.000	540.00	7.0000	3391.0	0.0236 AFMC N N
3327 3328	74.000 74.000	91.000 91.000	806.00 1105.0	0.0000	3391.0 3391.0	0.0264 AFMC N N 0.0338 AFMC N N
3329	74.000	91.000	805.00	0.0000	3391.0	0.0262 AFMC N N
3330 3331	74.000 74.000	91.000 91.000	703.00 374.00	0.0000 12.000	3391.0 3391.0	0.0256 AFMC N N 0.0215 AFMC N N
3332	74.000	91.000	96.000	89.000	3391.0	0.0215 AFMC N N
3333	74.000	91.000	35.000	168.00	3391.0	0.0152 AFMC N N
3334 3335	74.000 74.000	91.000 91.000	0.0000	283.00 272.00	3391.0 3391.0	0.0155 AFMC N N 0.0142 AFMC N N
3336	74.000	91.000	124.00	75.000	3391.0	0.0142 AFMC N N
3337	75.000	91.000	1.0000	147.00	1619.0	0.0082 AFMC N N
3338 3339	75.000 75.000	91.000 91.000	62.000 261.00	43.000 13.000	1619.0 1619.0	0.0071 AFMC N N 0.0092 AFMC N N
3340	75.000	91.000	236.00	1.0000	1619.0	0.0124 AFMC N N
3341 3342	75.000 75.000	91.000 91.000	145.00 303.00	4.0000	1619.0 1619.0	0.0099 AFMC N N 0.0109 AFMC N N
3343	75.000	91.000	130.00	17.000	1619.0	0.0109 AFMC N N
3344	75.000	91.000	145.00	9.0000	1619.0	0.0083 AFMC N N
3345 3346	75.000 75.000	91.000 91.000	41.000 0.0000	13.000 70.000	1619.0 1619.0	0.0065 AFMC N N 0.0069 AFMC N N
3347	75.000	91.000	0.0000	129.00	1619.0	0.0009 AFMC N N
3348	75.000	91.000	0.0000	92.000	1619.0	0.0074 AFMC N N
3349 3350	76.000 76.000	91.000 91.000	37.000 348.00	87.000 0.0000	11422.0 11422.0	0.0077 AFMC N Y 0.0119 AFMC N Y
3351	76.000	91.000	707.00	0.0000	11422.0	0.0158 AFMC N Y
3352 3353	76.000 76.000	91.000 91.000	532.00 259.00	0.0000	11422.0 11422.0	0.0139 AFMC N Y 0.0123 AFMC N Y
3354	76.000	91.000	400.00	0.0000	11422.0	0.0123 AFMC N 1
3355	76.000	91.000	189.00	3.0000	11422.0	0.0096 AFMC N Y
3356 3357	76.000 76.000	91.000 91.000	104.00 7.0000	40.000 161.00	11422.0 11422.0	0.0083 AFMC N Y 0.0082 AFMC N Y
3358	76.000	91.000	0.0000	372.00	11422.0	0.0086 AFMC N Y
3359	76.000	91.000	4.0000	232.00	11422.0	0.0080 AFMC N Y
3360 3361	76.000 77.000	91.000 91.000	0.0000 310.00	392.00 9.0000	11422.0 864.00	0.0079 AFMC N Y 0.0270 AFMC N N
3362	77.000	91.000	558.00	3.0000	864.00	0.0241 AFMC N N
3363 3364	77.000 77.000	91.000 91.000	850.00 1089.0	0.0000	864.00 864.00	0.0279 AFMC N N 0.0315 AFMC N N
3365	77.000	91.000	817.00	0.0000	864.00	0.0268 AFMC N N
3366	77.000	91.000	649.00	0.0000	864.00	0.0279 AFMC N N
3367 3368	77.000 77.000	91.000 91.000	292.00 42.000	21.000 232.00	864.00 864.00	0.0271 AFMC N N 0.0256 AFMC N N
3369	77.000	91.000	0.0000	307.00	864.00	0.0232 AFMC N N
3370 3371	77.000 77.000	91.000 91.000	0.0000	402.00 317.00	864.00 864.00	0.0190 AFMC N N 0.0256 AFMC N N
3371	77.000	91.000	105.00	147.00	864.00	0.0241 AFMC N N
3373	78.000	91.000	90.000	147.00	11778.0	0.0099 AFMC N Y
3374 3375	78.000 78.000	91.000 91.000	235.00 375.00	8.0000 9.0000	11778.0 11778.0	0.0114 AFMC N Y 0.0156 AFMC N Y
3376	78.000	91.000	501.00	0.0000	11778.0	0.0168 AFMC N Y
3377 3378	78.000 78.000	91.000 91.000	314.00 0.0000	6.0000 46.000	11778.0 11778.0	0.0141 AFMC N Y 0.0119 AFMC N Y
3379	78.000	91.000	29.000	139.00	11778.0	0.0119 AFMC N 1
3380	78.000	91.000	0.0000	342.00	11778.0	0.0101 AFMC N Y
3381 3382	78.000 78.000	91.000 91.000	0.0000	405.00 552.00	11778.0 11778.0	0.0106 AFMC N Y 0.0101 AFMC N Y
3383	78.000	91.000	0.0000	489.00	11778.0	0.0114 AFMC N Y
3384	78.000 79.000	91.000	0.0000	331.00	11778.0	0.0103 AFMC N Y
3385 3386	79.000	91.000 91.000	139.00 834.00	65.000 0.0000	13272.0 13272.0	0.0117 AFMC N Y 0.0218 AFMC N Y
3387	79.000	91.000	834.00	0.0000	13272.0	0.0262 AFMC N Y
3388 3389	79.000 79.000	91.000 91.000	844.00 396.00	0.0000	13272.0 13272.0	0.0288 AFMC N Y 0.0227 AFMC N Y
3390	79.000	91.000	285.00	34.000	13272.0	0.0229 AFMC N Y
3391 3392	79.000 79.000	91.000 91.000	71.000 18.000	81.000 306.00	13272.0 13272.0	0.0164 AFMC N Y 0.0167 AFMC N Y
3393	79.000	91.000	0.0000	476.00	13272.0	0.0167 AFMC N 1

3394 33956 33967 33997 33990 34001 34007 34007 34007 34112 34112 34112 34112 34112 34112 34112 34112 34112 34112 34112 34112 34112 3412 34	79.000 79.000 80.000 80.000 80.000 80.000 80.000 80.000 80.000 80.000 80.000 56.000 56.000 56.000 56.000 56.000 56.000 57.000	91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 91.000 94.000	0.0000 0.0000 346.00 540.00 892.00 1117.0 826.00 673.00 3.17.00 62.000 3.0000 0.0000 107.00 9.0000 42.000 158.00 66.000 48.000 0.0000	599.00 294.00 0.0000 0.0000 0.0000	13272.0 13272.0 13272.0 14689.0 14689.0 14689.0 14689.0 14689.0 14689.0 14689.0 14689.0 14689.0 3583.0 322.00 329.70 2897.0 2897.0 2897.0 2897.0 2897.0 2897.0	0.0177 AFN 0.0179 AFN 0.0166 AFN 0.0166 AFN 0.0223 AFN 0.0275 AFN 0.0263 AFN 0.0263 AFN 0.0205 AFN 0.0157 AFN 0.0157 AFN 0.0157 AFN 0.0157 AFN 0.0157 AFN 0.0148 AFN 0.0132 AFN 0.0132 AFN 0.0132 AFN 0.0132 AFN 0.0136 SPC 0.0176 SPC 0.0176 SPC 0.0176 SPC 0.0176 SPC 0.0180 SPC 0.0176 SPC 0.0189 SPC 0.0768 SPC		ע מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ
3442 3443 3444 3445 3446 3447 3448 3449 3450	58.000 58.000 58.000 59.000 59.000 59.000 59.000 59.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	0.0000 0.0000 4.0000 642.00 0.0000 1059.0 1097.0 0.0000	651.00 599.00 294.00 0.0000 0.0000 0.0000 0.0000 0.0000	115.00 115.00 115.00 2897.0 2897.0 2897.0 2897.0 2897.0 2897.0	0.0421 SPC 0.0484 SPC 0.0414 SPC 0.0141 SPC 0.0212 SPC 0.0262 SPC 0.0234 SPC 0.0214 SPC 0.0184 SPC	N N N N N N N N N N N N N N N N N N N	N N N N N N N
3451 3452 3453 3454 3455 3456 3457 3458 3459 3460 3461 3462 3463 3464	59.000 59.000 59.000 59.000 59.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000	94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000 94.000	809.00 644.00 249.00 43.000 0.0000 16.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 3.0000 91.000 0.0000 156.00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	2897.0 2897.0 2897.0 2897.0 2897.0 1464.0 1464.0 1464.0 1464.0 1464.0 1464.0	0.0205 SPC 0.0114 SPC 0.0090 SPC 0.0079 SPC 0.0069 SPC 0.0092 SPC 0.0229 SPC 0.0229 SPC 0.0241 SPC 0.0240 SPC 0.0212 SPC 0.0215 SPC 0.0202 SPC 0.0202 SPC		N N N N N N N N N

3465	60.000	94.000	0.0000	0.0000	1464.0	0.0180 SPC	N	N
3466	60.000	94.000	0.0000	0.0000	1464.0	0.0100 SPC 0.0173 SPC	N	N
3467	60.000	94.000	0.0000	0.0000	1464.0	0.0173 SPC 0.0174 SPC	N	N
3468	60.000	94.000	0.0000	0.0000	1464.0	0.0174 SPC 0.0167 SPC	N	N
3469	61.000	94.000	483.00	0.0000	2938.0	0.0165 SPC	Y	N
3470	61.000	94.000	1002.0	0.0000	2938.0	0.0271 SPC	Y	N
3471	61.000	94.000	887.00	0.0000	2938.0	0.0202 SPC	Y	N
3472	61.000	94.000	1099.0	0.0000	2938.0	0.0301 SPC	Y	N
3473	61.000	94.000	1264.0	0.0000	2938.0	0.0307 SPC	Y	N
3474	61.000	94.000	694.00	0.0000	2938.0	0.0183 SPC	Y	Ν
3475	61.000	94.000	538.00	2.0000	2938.0	0.0163 SPC	Y	Ν
3476	61.000	94.000	226.00	8.0000	2938.0	0.0156 SPC	Y	Ν
3477	61.000	94.000	111.00	75.000	2938.0	0.0065 SPC	Y	Ν
3478	61.000	94.000	23.000	226.00	2938.0	0.0070 SPC	Y	Ν
3479	61.000	94.000	21.000	222.00	2938.0	0.0078 SPC	Y	N
3480	61.000	94.000	81.000	59.000	2938.0	0.0083 SPC	Y	N
3481	62.000	94.000	0.0000	0.0000	119.00	0.0596 SPC	N	N
3482	62.000	94.000	0.0000	0.0000	119.00	0.0597 SPC	N	N
3483	62.000	94.000	0.0000	0.0000	119.00	0.0563 SPC	N	N
3484	62.000	94.000	0.0000	0.0000	119.00	0.1957 SPC	N	N
3485	62.000	94.000	0.0000	0.0000	119.00	0.1349 SPC	N	N
3486	62.000	94.000	0.0000	0.0000	119.00	0.1408 SPC	N	N
3487	62.000	94.000	0.0000	0.0000	119.00	0.0302 SPC	N	N
3488	62.000	94.000	0.0000	0.0000	119.00	0.0193 SPC	N	N
3489	62.000	94.000	0.0000	0.0000	119.00	0.0222 SPC	N	N
3490	62.000	94.000	0.0000	0.0000	119.00	0.0233 SPC	N	N
3491	62.000	94.000	0.0000	0.0000	119.00	0.0207 SPC	N	N
3492	62.000	94.000	0.0000	0.0000	119.00	0.0290 SPC	N	N
3493	63.000	94.000	0.0000	0.0000	497.00	0.1283 SPC	N	N
3494	63.000	94.000	0.0000	0.0000	497.00	0.1265 SPC	N	N
3495	63.000	94.000	0.0000	0.0000	497.00	0.1259 SPC	N	N
3496	63.000	94.000	0.0000	0.0000	497.00	0.1380 SPC	N	N
3497	63.000	94.000	0.0000	0.0000	497.00	0.1421 SPC	N	N
3498	63.000	94.000	0.0000	0.0000	497.00	0.1428 SPC	N	N
3499	63.000	94.000	0.0000	0.0000	497.00	0.1263 SPC	N	N
3500	63.000	94.000	0.0000	0.0000	497.00	0.1264 SPC	N	N
3501	63.000	94.000	0.0000	0.0000	497.00	0.1359 SPC	N	N
3502	63.000	94.000	0.0000	0.0000	497.00	0.1315 SPC	N	N
3503	63.000	94.000	0.0000	0.0000	497.00	0.1395 SPC	N	N
3504	63.000	94.000	0.0000	0.0000	497.00	0.1320 SPC	N	N
3505	64.000	94.000	1.0000	455.00	3433.0	0.0079 SPC	N	N
3506	64.000	94.000	26.000	227.00	3433.0	0.0059 SPC	N	N
3507	64.000	94.000	109.00	36.000	3433.0	0.0078 SPC	N	N
3508	64.000	94.000	17.000	11.000	3433.0	0.0071 SPC	N	N
3509	64.000	94.000	5.0000	22.000	3433.0	0.0063 SPC	N	Ν
3510	64.000	94.000	31.000	144.00	3433.0	0.0073 SPC	N	Ν
3511	64.000	94.000	0.0000	0.0000	3433.0	0.0070 SPC	N	Ν
3512	64.000	94.000	0.0000	0.0000	3433.0	0.0066 SPC	N	Ν
3513	64.000	94.000	0.0000	0.0000	3433.0	0.0078 SPC	N	N
3514	64.000	94.000	0.0000	0.0000	3433.0	0.0083 SPC	N	N
3515	64.000	94.000	0.0000	0.0000	3433.0	0.0071 SPC	N	Ν
3516	64.000	94.000	0.0000	0.0000	3433.0	0.0078 SPC	N	N
3517	65.000	94.000	519.00	1.0000	2483.0	0.0132 SPC	N	N
3518	65.000	94.000	972.00	0.0000	2483.0	0.0178 SPC	N	N
3519	65.000	94.000	1008.0	0.0000	2483.0	0.0163 SPC	N	N
3520	65.000	94.000	1032.0	0.0000	2483.0	0.1890 SPC	N	N
3521	65.000	94.000	926.00	0.0000	2483.0	0.1600 SPC	N	N
3522	65.000	94.000	749.00	0.0000	2483.0	0.0143 SPC	N	N
3523	65.000	94.000	576.00	0.0000	2483.0	0.0129 SPC	N	N
3524	65.000	94.000	223.00	5.0000	2483.0	0.0105 SPC	N	N
3525	65.000	94.000	14.000	143.00	2483.0	0.0070 SPC	N	N
3526	65.000	94.000	10.000	165.00	2483.0	0.0070 SPC	N	N
3527	65.000	94.000	14.000	182.00	2483.0	0.0089 SPC	N	N
3528	65.000	94.000	0.0000	0.0000	2483.0	0.0054 SPC	N	N
3529 3530	66.000	94.000	0.0000	0.0000	6916.0	0.0106 SPC	N	N
3530	66.000 66.000	94.000 94.000	0.0000 175.00	0.0000 6.0000	6916.0 6916.0	0.0114 SPC 0.0141 SPC	N N	N N
3531	66.000	94.000	0.0000	0.0000	6916.0	0.0141 SPC 0.0168 SPC	N	N
3532	66.000	94.000	0.0000	0.0000	6916.0	0.0100 SPC 0.0137 SPC	N	N
3534	66.000	94.000	0.0000	0.0000	6916.0	0.0137 SPC 0.0137 SPC	N	N
3535	66.000	94.000	0.0000	0.0000	6916.0	0.0137 SPC 0.0105 SPC	N	N
5555	55.555	71.000	3.000	3.000	3710.0	J. J. L. J. DE.C	TA	Τ4

3536	66.000	94.000	240.00	0.0000	6916.0	0.0140 SPC	N	N
3537	66.000	94.000	291.00		6916.0	0.0128 SPC	N	N
3538	66.000	94.000	229.00	0.0000	6916.0	0.0103 SPC	N	N
3539	66.000	94.000	162.00	2.0000	6916.0	0.0116 SPC	N	N
3540	66.000	94.000	0.0000	0.0000	6916.0	0.1150 SPC	N	N
3541	56.000	93.000	0.0000	271.00	3583.0	0.0178 SPC	N	N
3542	56.000	93.000	44.000	211.00	3583.0	0.0186 SPC	N	N
3543	56.000	93.000	99.000	49.000	3583.0	0.0163 SPC	N	N
3544	56.000	93.000	73.000	106.00	3583.0	0.0163 SPC	N	N
3545	56.000	93.000	178.00	11.000	3583.0	0.0155 SPC	N	N
3546 3547 3548	56.000 56.000 56.000	93.000 93.000 93.000	85.000 25.000	74.000 85.000 281.00	3583.0 3583.0 3583.0	0.0156 SPC 0.0176 SPC	N N	N N
3549 3550	56.000 56.000	93.000 93.000 93.000	0.0000 0.0000 0.0000	452.00 560.00	3583.0 3583.0	0.0180 SPC 0.0178 SPC 0.0209 SPC	N N N	N N N
3551	56.000	93.000	0.0000	538.00	3583.0	0.0203 SPC	N	N
3552	56.000	93.000	0.0000	486.00	3583.0	0.0194 SPC	N	N
3553	57.000	93.000	0.0000	0.0000	388.00	0.0780 SPC	N	N
3554 3555	57.000 57.000	93.000 93.000	0.0000	0.0000	388.00 388.00	0.0636 SPC 0.0675 SPC	N N	N N
3556	57.000	93.000	0.0000	0.0000	388.00	0.0767 SPC	N	N
3557	57.000	93.000	0.0000	0.0000	388.00	0.0751 SPC	N	N
3558	57.000	93.000	0.0000	0.0000	388.00	0.0797 SPC	N	N
3559 3560	57.000 57.000	93.000 93.000	0.0000	0.0000	388.00 388.00	0.0801 SPC 0.0875 SPC	N N	N N
3561	57.000	93.000	0.0000	0.0000	388.00	0.0844 SPC	N	N
3562	57.000	93.000	0.0000	0.0000	388.00	0.0873 SPC	N	N
3563	57.000	93.000	0.0000	0.0000	388.00	0.0795 SPC	N	N
3564	57.000	93.000	0.0000	0.0000	388.00	0.0773 SPC	N	N
3565	58.000	93.000	27.000	134.00	115.00	0.0402 SPC	N	N
3566	58.000	93.000	370.00	16.000	115.00	0.0378 SPC	N	N
3567	58.000	93.000	473.00	3.0000	115.00	0.0444 SPC	N	N
3568	58.000	93.000	619.00	0.0000	115.00	0.0468 SPC	N	N
3569	58.000	93.000	434.00	0.0000	115.00	0.0406 SPC	N	N
3570	58.000	93.000	0.0000	0.0000	115.00	0.0472 SPC	N	N
3571	58.000	93.000	434.00	0.0000	115.00	0.0422 SPC	N	N
3572 3573	58.000 58.000	93.000 93.000	0.0000	0.0000	115.00 115.00	0.0415 SPC 0.0383 SPC	N N	N N
3574	58.000	93.000	0.0000	0.0000	115.00	0.0535 SPC	N	N
3575	58.000	93.000	0.0000	0.0000	115.00	0.0343 SPC	N	N
3576	58.000	93.000	0.0000	283.00	115.00	0.0397 SPC	N	N
3577	59.000	93.000	484.00	0.0000	3584.0	0.0131 SPC	N	N
3578	59.000	93.000	1014.0	0.0000	3584.0	0.0155 SPC	N	N
3579	59.000	93.000	1216.0	0.0000	3584.0	0.0206 SPC	N	N
3580	59.000	93.000	1198.0	0.0000	3584.0	0.0184 SPC	N	N
3581	59.000	93.000	8.0000		3584.0	0.0156 SPC	N	N
3582	59.000	93.000	856.00	0.0000	3584.0	0.0108 SPC	N	N
3583	59.000	93.000	680.00	0.0000	3584.0	0.0120 SPC	N	N
3584	59.000	93.000	0.0000	0.0000	3584.0	0.0088 SPC	N	N
3585 3586 3587	59.000 59.000 59.000	93.000 93.000 93.000	0.0000 45.000 0.0000	0.0000 89.000 0.0000	3584.0 3584.0 3584.0	0.0063 SPC 0.0136 SPC 0.0080 SPC	N N	N N
3588 3589	59.000 60.000	93.000 93.000	0.0000	0.0000	3584.0 1457.0	0.0068 SPC 0.0180 SPC	N N N	N N N
3590	60.000	93.000	990.00	0.0000	1457.0	0.0186 SPC	N	N
3591	60.000	93.000	1101.0	0.0000	1457.0	0.0247 SPC	N	N
3592	60.000	93.000	0.0000	0.0000	1457.0	0.0216 SPC	N	N
3593 3594	60.000	93.000 93.000	990.00 776.00	0.0000	1457.0 1457.0	0.0208 SPC 0.0255 SPC	N N	N N
3595	60.000	93.000	558.00	0.0000	1457.0	0.0245 SPC	N	N
3596	60.000	93.000	0.0000	0.0000	1457.0	0.0196 SPC	N	N
3597	60.000	93.000	0.0000	0.0000	1457.0	0.0172 SPC	N	N
3598	60.000	93.000	0.0000	0.0000	1457.0	0.0171 SPC	N	N
3599	60.000	93.000	0.0000	0.0000	1457.0	0.0173 SPC	N	N
3600	60.000	93.000	0.0000	0.0000	1457.0	0.0178 SPC	N	N
3601	61.000	93.000	463.00	16.000	2977.0	0.0163 SPC	Y	N
3602	61.000	93.000	800.00	0.0000	2977.0	0.0221 SPC	Y	N
3603	61.000	93.000	1367.0	0.0000	2977.0	0.0284 SPC	Y	N
3604	61.000	93.000	1494.0	0.0000	2977.0	0.0291 SPC	Y	N
3605	61.000	93.000	1205.0	0.0000	2977.0	0.0265 SPC	Y	N
3606	61.000	93.000	770.00	0.0000	2977.0	0.0225 SPC	Y	N

3607	61.000	93.000	540.00	0.0000	2977.0	0.0218 SPC	Y	N
3608	61.000	93.000	199.00	13.000	2977.0	0.0156 SPC	Y	N
3609	61.000	93.000	189.00	33.000	2977.0	0.0087 SPC	Y	N
3610	61.000	93.000	141.00	24.000	2977.0	0.0082 SPC	Y	N
3611	61.000	93.000	57.000	91.000	2977.0	0.0104 SPC	Y	N
3612	61.000	93.000	11.000	286.00	2977.0	0.0102 SPC	Y	N
3613	62.000	93.000	0.0000	0.0000	119.00	0.0263 SPC	N	N
3614	62.000	93.000	0.0000	0.0000	119.00	0.0334 SPC	N	N
3615	62.000	93.000	0.0000	0.0000	119.00	0.0377 SPC	N	N
3616	62.000	93.000	0.0000	0.0000	119.00	0.0359 SPC	N	N
3617	62.000	93.000	0.0000	0.0000	119.00	0.0371 SPC	N	N
3618	62.000	93.000	0.0000	0.0000	119.00	0.0311 SPC	N	N
3619	62.000	93.000	0.0000	0.0000	119.00	0.0300 SPC	N	N
3620	62.000	93.000	0.0000	0.0000	119.00	0.0214 SPC	N	N
3621	62.000	93.000	0.0000	0.0000	119.00	0.0212 SPC	N	N
3622	62.000	93.000	0.0000	0.0000	119.00	0.0224 SPC	N	N
3623	62.000	93.000	0.0000	0.0000	119.00	0.0199 SPC	N	N
3624	62.000	93.000	0.0000	0.0000	119.00	0.0233 SPC	N	N
3625 3626 3627 3628	63.000 63.000 63.000 63.000	93.000 93.000 93.000 93.000	0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000	497.00 497.00 497.00 497.00	0.1214 SPC 0.1303 SPC 0.1250 SPC 0.1254 SPC	N N N	N N N
3629 3630 3631	63.000 63.000 63.000	93.000 93.000 93.000	0.0000 0.0000 0.0000	0.0000 0.0000 0.0000	497.00 497.00 497.00	0.1290 SPC 0.1210 SPC 0.1324 SPC	N N N	N N N N
3632	63.000	93.000	0.0000	0.0000	497.00	0.1346 SPC	N	N
3633	63.000	93.000	0.0000	0.0000	497.00	0.1285 SPC	N	N
3634	63.000	93.000	0.0000	0.0000	497.00	0.1284 SPC	N	N
3635	63.000	93.000	0.0000	0.0000	497.00	0.1389 SPC	N	N
3636 3637 3638 3639	63.000 64.000 64.000	93.000 93.000 93.000	0.0000 0.0000 30.000	0.0000 31.000 249.00 95.000	497.00 3433.0 3433.0	0.1300 SPC 0.0056 SPC 0.0068 SPC	N N N	N N N
3640 3641 3642	64.000 64.000 64.000	93.000 93.000 93.000 93.000	38.000 28.000 76.000 43.000	148.00 33.000 116.00	3433.0 3433.0 3433.0 3433.0	0.0046 SPC 0.0074 SPC 0.0052 SPC 0.0062 SPC	N N N N	N N N N
3643	64.000	93.000	2.0000	178.00	3433.0	0.0068 SPC	N	N
3644	64.000	93.000	0.0000	376.00	3433.0	0.0064 SPC	N	N
3645	64.000	93.000	0.0000	503.00	3433.0	0.0067 SPC	N	N
3646	64.000	93.000	0.0000	593.00	3433.0	0.0075 SPC	N	N
3647	64.000	93.000	0.0000	579.00	3433.0	0.0073 SPC	N	N
3648	64.000	93.000	0.0000	579.00	3433.0	0.0065 SPC	N	N
3649	65.000	93.000	383.00	0.0000	2529.0	0.0132 SPC	N	N
3650	65.000	93.000	990.00	0.0000	2529.0	0.0128 SPC	N	N
3651	65.000	93.000	1101.0	0.0000	2529.0	0.0157 SPC	N	N
3652	65.000	93.000	1179.0	0.0000	2529.0	0.0155 SPC	N	N
3653	65.000	93.000	990.00	0.0000	2529.0	0.0160 SPC	N	N
3654	65.000	93.000	776.00	0.0000	2529.0	0.0134 SPC	N	N
3655	65.000	93.000	558.00	0.0000	2529.0	0.0105 SPC	N	N
3656	65.000	93.000	286.00	2.0000	2529.0	0.0079 SPC	N	N
3657	65.000	93.000	84.000	89.000	2529.0	0.0064 SPC	N	N
3658	65.000	93.000	0.0000	183.00	2529.0	0.0063 SPC	N	N
3659	65.000	93.000	0.0000	0.0000	2529.0	0.0072 SPC	N	N
3660	65.000	93.000	212.00	11.000	2529.0	0.0032 SPC	N	N
3661	66.000	93.000	0.0000	0.0000	7050.0	0.0169 SPC	N	N
3662 3663 3664 3665	66.000 66.000 66.000	93.000 93.000 93.000 93.000	0.0000 0.0000 366.00 344.00	0.0000 0.0000 0.0000 0.0000	7050.0 7050.0 7050.0 7050.0	0.0146 SPC 0.0138 SPC 0.0154 SPC 0.0141 SPC	N N N	N N N
3666	66.000	93.000	266.00	0.0000	7050.0	0.0137 SPC	N	N
3667	66.000	93.000	0.0000	0.0000	7050.0	0.0143 SPC	N	N
3668	66.000	93.000	0.0000	240.00	7050.0	0.0144 SPC	N	N
3669 3670 3671 3672	66.000 66.000 66.000	93.000 93.000 93.000 93.000	5.0000 0.0000 0.0000 0.0000	266.00 150.00 120.00 0.0000	7050.0 7050.0 7050.0 7050.0	0.0135 SPC 0.0129 SPC 0.0118 SPC 0.0120 SPC	N N N N	N N N N
3673	56.000	92.000	0.0000	301.00	3504.0	0.0192 SPC	N	N
3674	56.000	92.000	84.000	119.00	3504.0	0.0201 SPC	N	N
3675	56.000	92.000	78.000	94.000	3504.0	0.0183 SPC	N	N
3676	56.000	92.000	232.00	17.000	3504.0	0.0172 SPC	N	N
3677	56.000	92.000	113.00	63.000	3504.0	0.0171 SPC	N	N

3678 3679 3681 3682 3688 3688 3688 3688 3699 3699 3699 3699	56.000 56.000 56.000 56.000 56.000 56.000 57.000 57.000 57.000 57.000 57.000 57.000 57.000 57.000 57.000 58.000	92.000 92.000	83.000 37.000 14.000 0.0000	78.000 137.00 245.00 444.00 546.00 487.00 0.0000	3504.0 3504.0 3504.0 3504.0 3504.0 3504.0 322.00	0.0172 SPC 0.0183 SPC 0.0213 SPC 0.0214 SPC 0.0227 SPC 0.0227 SPC 0.0232 SPC 0.0210 SPC 0.1435 SPC 0.0709 SPC 0.0538 SPC 0.0915 SPC 0.0724 SPC 0.0724 SPC 0.0750 SPC 0.0849 SPC 0.0852 SPC 0.0852 SPC 0.0854 SPC 0.0857 SPC 0.0857 SPC 0.0495 SPC		
3720 3721 3722 3723 3724 3726 3727 3728 3729 3730 3731 3732 3733 3733 3735 3736 3737 3740 3741 3742 3743 3744 3745 3746 3747 3748	59.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 61.000 61.000 61.000 61.000 61.000 61.000 61.000 62.000 62.000 62.000	92.000 92.000	161.00 453.00 954.00 1048.0 998.00 0.0000 717.00 383.00 219.00 96.000 12.000 0.0000 91.000 925.00 992.00 9925.00 935.00 819.00 670.00 454.00 231.00 128.00 130.00 171.00 260.00 0.0000 0.0000 0.0000 0.0000	16.000 4.0000 0.0000 0.0000 0.0000 0.0000 4.0000 3.0000 28.000 131.00 0.0000 0.0000 0.0000 0.0000 0.0000 7.0000 70.000 113.00 21.000 70.000 113.00 21.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	3584.0 1347.0 1347.0 1347.0 1347.0 1347.0 1347.0 1347.0 1347.0 1347.0 1347.0 3067.0	0.0093 SPC 0.0236 SPC 0.0237 SPC 0.0285 SPC 0.0225 SPC 0.0211 SPC 0.0227 SPC 0.0247 SPC 0.0189 SPC 0.0170 SPC 0.0166 SPC 0.0183 SPC 0.0192 SPC 0.0216 SPC 0.0220 SPC 0.0220 SPC 0.0229 SPC 0.0229 SPC 0.0229 SPC 0.0171 SPC 0.0192 SPC 0.0192 SPC 0.0193 SPC 0.0193 SPC 0.0194 SPC 0.0195 SPC 0.0195 SPC 0.0197 SPC 0.0198 SPC 0.0199 SPC 0.0199 SPC 0.0190 SPC 0.0276 SPC 0.0281 SPC 0.0327 SPC 0.0400 SPC	N N N N N N N N N N N N N N N N N N N	N N N N N N N N N N N N N N N N N N N

3798 3799 3800 3801 3802 3803 3804 3805 3806 3807 3808 3809 3810 3811	62.000 62.000 62.000 62.000 62.000 62.000 63.000 63.000 63.000 63.000 63.000 63.000 63.000 63.000 64.000 64.000 64.000 64.000 64.000 64.000 64.000 65.000 65.000 66.000	92.000 92.000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 293.00 7.0000 19.000 82.000 92.000 104.00 77.000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 155.00 148.00 41.000 155.00 148.00 41.000 194.00 296.00 475.00 556.00 513.00 543.00 0.0000	119.00 119.00 119.00 119.00 119.00 119.00 119.00 497.00 497.00 497.00 497.00 497.00 497.00 497.00 497.00 3392.0 3434.0 2434.0 3447.0 3447.0 3447.0 3447.0 3447.0 3447.0 3447.0	0.0117 SPC 0.0133 SPC 0.0133 SPC 0.0110 SPC 0.0128 SPC 0.0127 SPC 0.0124 SPC 0.0192 SPC 0.0195 SPC 0.0195 SPC 0.0158 SPC 0.0173 SPC 0.0177 SPC 0.0180 SPC 0.0181 SPC		
3806 3807 3808 3809 3810	56.000 56.000 56.000 56.000	91.000 91.000 91.000 91.000 91.000	19.000 82.000 92.000 104.00 77.000	158.00 122.00 103.00 57.000 120.00	3447.0 3447.0 3447.0 3447.0 3447.0	0.0195 SPC 0.0158 SPC 0.0173 SPC 0.0177 SPC 0.0180 SPC	N N N N	N N N N

3820 3821	57.000 57.000	91.000 91.000	0.0000	0.0000	309.00 309.00	0.1127 SPC 0.0711 SPC	N N	N N
3822	57.000	91.000	0.0000	0.0000	309.00	0.1119 SPC	N	N
3823	57.000	91.000	0.0000	0.0000	309.00	0.0924 SPC	N	N
3824	57.000	91.000	0.0000	0.0000	309.00	0.1053 SPC	N	N
3825 3826	57.000 57.000	91.000 91.000	0.0000	0.0000	309.00 309.00	0.1126 SPC 0.1064 SPC	N N	N N
3827	57.000	91.000	0.0000	0.0000	309.00	0.1002 SPC	N	N
3828	57.000	91.000	0.0000	0.0000	309.00	0.0793 SPC	N	N
3829	58.000	91.000	124.00	88.000	115.00	0.0432 SPC	N	N
3830	58.000	91.000	257.00	26.000	115.00	0.0383 SPC	N	N
3831	58.000	91.000	610.00	0.0000	115.00	0.0446 SPC	N	N
3832	58.000	91.000	651.00	0.0000	115.00	0.0368 SPC	N	N
3833	58.000	91.000	364.00	0.0000	115.00	0.0365 SPC	N	N
3834	58.000	91.000	214.00	30.000	115.00	0.0367 SPC	N	N
3835 3836	58.000 58.000	91.000 91.000 91.000	38.000 8.0000	98.000 371.00	115.00 115.00 115.00	0.0307 SPC 0.0412 SPC 0.0377 SPC	N N	N N
3837	58.000	91.000	0.0000	413.00	115.00	0.0468 SPC	N	N
3838	58.000	91.000		517.00	115.00	0.0404 SPC	N	N
3839	58.000	91.000	0.0000	581.00	115.00	0.0393 SPC	N	N
3840	58.000	91.000	33.000	248.00	115.00	0.0428 SPC	N	N
3841	59.000	91.000	558.00	0.0000	2976.0	0.0135 SPC	N	N
3842	59.000	91.000	784.00	0.0000	2976.0	0.0179 SPC	N	N
3843	59.000	91.000	1364.0		2976.0	0.0254 SPC	N	N
3844	59.000	91.000	1231.0	0.0000	2976.0	0.0237 SPC	N	N
3845	59.000	91.000	799.00	0.0000	2976.0	0.0202 SPC	N	N
3846	59.000	91.000	879.00	0.0000	2976.0	0.0128 SPC	N	N
3847	59.000	91.000	712.00	0.0000	2976.0	0.0157 SPC	N	N
3848	59.000	91.000	385.00		2976.0	0.0121 SPC	N	N
3849	59.000	91.000	95.000	28.000	2976.0	0.0074 SPC	N	N
3850	59.000	91.000	40.000	111.00	2976.0	0.0082 SPC	N	N
3851	59.000	91.000	0.0000	0.0000	2976.0	0.0067 SPC	N	N
3852	59.000	91.000	0.0000	0.0000	2976.0	0.0080 SPC	N	N
3853	60.000	91.000	473.00		1343.0	0.0198 SPC	N	N
3854	60.000	91.000	663.00	0.0000	1343.0	0.0225 SPC	N	N
3855	60.000	91.000	1258.0	0.0000	1343.0	0.0230 SPC	N	N
3856	60.000	91.000	1142.0	0.0000	1343.0	0.0230 SPC	N	N
3857 3858	60.000	91.000 91.000 91.000	750.00 773.00	0.0000	1343.0 1343.0	0.0230 SPC 0.0192 SPC 0.0212 SPC	N N	N N
3859	60.000	91.000	568.00	0.0000	1343.0	0.0161 SPC	N	N
3860	60.000	91.000	219.00	8.0000	1343.0	0.0189 SPC	N	N
3861	60.000	91.000	33.000	101.00	1343.0	0.0196 SPC	N	N
3862 3863	60.000	91.000 91.000	16.000 16.000	161.00 161.00 120.00	1343.0 1343.0	0.0163 SPC 0.0163 SPC	N N	N N
3864	60.000	91.000	0.0000	0.0000	1343.0	0.0159 SPC	N	N
3865	61.000	91.000	460.00	0.0000	3539.0	0.0186 SPC	Y	N
3866	61.000	91.000	711.00	0.0000	3539.0	0.0172 SPC	Y	N
3867 3868	61.000 61.000	91.000 91.000 91.000	0.0000	0.0000	3539.0 3539.0 3539.0	0.0354 SPC 0.0250 SPC	Y Y	N
3869	61.000	91.000	647.00	0.0000	3539.0	0.0217 SPC	Y	N
3870	61.000	91.000	848.00	0.0000	3539.0	0.0211 SPC	Y	N
3871	61.000	91.000	0.0000	0.0000	3539.0	0.0191 SPC	Y	N
3872	61.000	91.000	0.0000	0.0000	3539.0	0.0177 SPC	Y	N
3873	61.000	91.000	16.000	12.000	3539.0	0.0129 SPC	Y	N
3874	61.000	91.000	4.0000	226.00	3539.0	0.0088 SPC	Y	N
3875	61.000	91.000	0.0000	0.0000	3539.0	0.0093 SPC	Y	N
3876	61.000	91.000	0.0000	0.0000	3539.0	0.0110 SPC	Y	N
3877 3878	62.000 62.000	91.000 91.000	0.0000	0.0000	119.00 119.00	0.0236 SPC 0.0321 SPC	N N	N N
3879	62.000	91.000	0.0000	0.0000	119.00	0.0332 SPC	N	N
3880	62.000	91.000	0.0000	0.0000	119.00	0.0396 SPC	N	N
3881	62.000	91.000	0.0000	0.0000	119.00	0.0319 SPC	N	N
3882 3883	62.000 62.000	91.000 91.000	0.0000	0.0000	119.00 119.00	0.0372 SPC 0.0288 SPC	N N	N N
3884	62.000	91.000	0.0000	0.0000	119.00	0.0261 SPC	N	N
3885	62.000	91.000	0.0000	0.0000	119.00	0.0231 SPC	N	N
3886	62.000	91.000	0.0000	0.0000	119.00	0.0225 SPC	N	N
3887 3888	62.000 62.000	91.000 91.000	0.0000	0.0000	119.00 119.00	0.0227 SPC 0.0237 SPC	N N	N N
3889 3890	63.000 63.000	91.000 91.000	0.0000	0.0000	497.00 497.00	0.1501 SPC 0.1395 SPC	N N	N N

3891	63.000	91.000	0.0000	0.0000	497.00	0.1441 SPC	N	N
3892	63.000	91.000	0.0000	0.0000	497.00	0.1513 SPC	N	N
3893	63.000	91.000	0.0000	0.0000	497.00	0.1394 SPC	N	N
3894	63.000	91.000	0.0000	0.0000	497.00	0.1449 SPC	N	N
3895	63.000	91.000	0.0000	0.0000	497.00	0.1488 SPC	N	N
3896	63.000	91.000	0.0000	0.0000	497.00	0.1320 SPC	N	N
3897	63.000	91.000	0.0000	0.0000	497.00	0.1328 SPC	N	N
3898	63.000	91.000	0.0000	0.0000	497.00	0.1489 SPC	N	N
3899 3900	63.000	91.000	0.0000	0.0000	497.00	0.1388 SPC	N	N
3900	63.000 64.000	91.000 91.000	0.0000 5.0000	0.0000 423.00	497.00 3420.0	0.1439 SPC 0.0047 SPC	N N	N N
3901	64.000	91.000	3.0000	215.00	3420.0	0.0047 SPC 0.0046 SPC	N	N
3903	64.000	91.000	36.000	159.00	3420.0	0.0040 SFC	N	N
3904	64.000	91.000	55.000	149.00	3420.0	0.0018 SPC	N	N
3905	64.000	91.000	69.000	97.000	3420.0	0.0067 SPC	N	N
3906	64.000	91.000	34.000	149.00	3420.0	0.0064 SPC	N	N
3907	64.000	91.000	2.0000	319.00	3420.0	0.0057 SPC	N	N
3908	64.000	91.000	0.0000	469.00	3420.0	0.0064 SPC	N	N
3909	64.000	91.000	0.0000	503.00	3420.0	0.0070 SPC	N	N
3910	64.000	91.000	0.0000	535.00	3420.0	0.0070 SPC	N	N
3911	64.000	91.000	0.0000	558.00	3420.0	0.0076 SPC	N	N
3912	64.000	91.000	0.0000	542.00	3420.0	0.0071 SPC	N	N
3913	65.000	91.000	473.00	0.0000	2434.0	0.0150 SPC	N	N
3914	65.000	91.000	663.00	0.0000	2434.0	0.0114 SPC	N	N
3915 3916	65.000	91.000 91.000	1258.0 1142.0	0.0000	2434.0 2434.0	0.0180 SPC	N	N
3910	65.000 65.000	91.000	750.00	0.0000	2434.0	0.0179 SPC 0.0145 SPC	N N	N N
3917	65.000	91.000	773.00	0.0000	2434.0	0.0145 SPC 0.0149 SPC	N	N
3919	65.000	91.000	568.00	0.0000	2434.0	0.0149 SPC	N	N
3920	65.000	91.000	219.00	8.0000	2434.0	0.0085 SPC	N	N
3921	65.000	91.000	33.000	101.00	2434.0	0.0063 SPC	N	N
3922	65.000	91.000	16.000	161.00	2434.0	0.0051 SPC	N	N
3923	65.000	91.000	16.000	120.00	2434.0	0.0070 SPC	N	N
3924	65.000	91.000	145.00	15.000	2434.0	0.0022 SPC	N	N
3925	66.000	91.000	180.00	6.0000	7037.0	0.0129 SPC	N	N
3926	66.000	91.000	257.00	5.0000	7037.0	0.0142 SPC	N	N
3927	66.000	91.000	485.00	0.0000	7037.0	0.0168 SPC	N	N
3928	66.000	91.000	397.00	0.0000	7037.0	0.0180 SPC	N	N
3929	66.000	91.000	313.00	0.0000	7037.0	0.0179 SPC	N	N
3930 3931	66.000 66.000	91.000 91.000	452.00 0.0000	0.0000	7037.0 7037.0	0.0179 SPC 0.0155 SPC	N	N
3931	66.000	91.000	0.0000	0.0000	7037.0	0.0155 SPC 0.0154 SPC	N N	N N
3932	66.000	91.000	0.0000	0.0000	7037.0	0.0134 SPC 0.0146 SPC	N	N
3934	66.000	91.000	0.0000	0.0000	7037.0	0.0146 SPC 0.0139 SPC	N	N
3935	66.000	91.000	0.0000	0.0000	7037.0	0.0139 SPC 0.0138 SPC	N	N
3936	66.000	91.000	0.0000	0.0000	7037.0	0.0130 SPC	N	N

Appendix B

STATISTIX 4.1 CH3DATA, 10/07/95, 11:18

VIEW DATA

				F				
CASE	BASE	CDD	CMD	L Y	FY	HDD	MBTU	SQFT
1	1	3	AMC	Y	94	319	0.0106	5898.0
2	1	9	AMC	Y	94	567	0.0200	5898.0
3	1	0	AMC	Y	94	914	0.0256	5898.0
4	1	0	AMC	Y	94	1180	0.0312	5898.0
5	1	0	AMC	Y	94	863	0.0297	5898.0
6	1	3	AMC	Y	94	672	0.0272	5898.0
7	1	42	AMC	Y	94	216	0.0137	5898.0
8	1	39	AMC	Y	94	209	0.0081	5898.0
9	1	322	AMC	Y	94	5	0.0095	5898.0
10	1	452	AMC	Y	94	0	0.0108	5898.0
11	1	241	AMC	Y	94	3	0.0103	5898.0
12	1		AMC	Y	94	20	0.0108	5898.0
13	2		AMC	Y	94	49	0.0087	2944.0
14	2		AMC	Y	94	206	0.0117	2944.0
15	2	0	AMC	Y	94	504	0.0172	2944.0
16	2	0	AMC	Y	94	568	0.0192	2944.0
17	2	7	AMC	Y	94	327	0.0153	2944.0
18	2	42	AMC	Y	94	152	0.0130	2944.0
19	2		AMC	Y	94	30	0.0052	2944.0
20	2	210	AMC	Y	94	11	0.0056	2944.0
21	2	489	AMC	Y	94	0	0.0061	2944.0
22	2		AMC	Y	94	0	0.0072	2944.0
23	2		AMC	Y	94	0	0.0064	2944.0
24	2	327	AMC	Y	94	0	0.0044	2944.0
25 26	3 3	5 7	AMC	Y	94	284	0.0111	3349.0
26 27	3		AMC	Y	94	540	0.0170	3349.0
27 28	3	0	AMC	Y Y	94 94	898	0.0237 0.0262	3349.0
26 29	3	0	AMC AMC	Y	94	1145 872	0.0262	3349.0 3349.0
30	3	0	AMC	Y	94	690	0.0227	3349.0
31	3	21	AMC	Y	94	234	0.0225	3349.0
32	3		AMC	Y	94	191	0.0094	3349.0
33	3	303	AMC	Y	94	5	0.0091	3349.0
34	3		AMC	Y	94	0	0.0094	3349.0
37	4	0	AMC	Y	94	535	0.0139	4394.0
38	4	0	AMC	Y	94	1130	0.0219	4394.0
39	4	0	AMC	Y	94	1116	0.0237	4394.0
40	4	_	AMC	Y	94	965	0.0223	4394.0
41	4	0	AMC	Y	94	1070	0.0222	4394.0
42	4	0	AMC	Y	94	784	0.0187	4394.0
43	4	0	AMC	Y	94	544	0.0144	4394.0
44	4	0	AMC	Y	94	386	0.0105	4394.0
45	4	0	AMC	Y	94	209	0.0070	4394.0
46	4	207	AMC	Y	94	47	0.0063	4394.0
47	4	106	AMC	Y	94	53	0.0067	4394.0

48	4	8	AMC	Y	94	141	0.0079	4394.0
49	5	0	AMC	Y	94	705	0.0231	3821.0
50	5	0	AMC	Y	94	1283	0.0266	3821.0
51	5	0	AMC	Y	94	1563	0.0324	3821.0
52	5	0	AMC	Y	94	2198	0.0272	3821.0
53	5	0	AMC	Y	94	1743	0.0290	3821.0
54	5	0	AMC	Y	94	1051	0.0243	3821.0
55	5	0	AMC	Y	94	652	0.0219	3821.0
56	5	40	AMC	Y	94	212	0.0167	3821.0
57	5	79	AMC	Y	94	17	0.0146	3821.0
58	5	84	AMC	Y	94	12	0.0135	3821.0
59	5	134	AMC	Y	94	61	0.0155	3821.0
60	5	54	AMC	Y	94	165	0.0138	3821.0
61	6	0	AMC	Y	94	449	0.0178	2315.0
62	6	0	AMC	Y	94	766	0.0242	2315.0
63	6	0	AMC	Y	94	1104	0.0282	2315.0
64	6	0	AMC	Y	94	1477	0.0291	2315.0
65	6	0	AMC	Y	94	1209	0.0270	2315.0
66	6	0	AMC	Y	94	1040	0.0266	2315.0
67	6	22	AMC	Y	94	393	0.0189	2315.0
68	6	63	AMC	Y	94	197	0.0139	2315.0
69	6	266	AMC	Y	94	18	0.0120	2315.0
73	7	114	AMC	Y	94	10	0.0073	3719.0
74	7	10	AMC	Y	94	178	0.0084	3719.0
75	7	0	AMC	Y	94	367	0.0104	3719.0
76	7	0	AMC	Y	94	289	0.0104	3719.0
77	7	0	AMC	Y	94	383	0.0107	3719.0
78	7	1	AMC	Y	94	228	0.0092	3719.0
79	7	25	AMC	Y	94	178	0.0081	3719.0
80	7	32	AMC	Y	94	96	0.0071	3719.0
81	7	319	AMC	Y	94	0	0.0075	3719.0
82	7	366	AMC	Y	94	0	0.0087	3719.0
83	7	515	AMC	Y	94	0	0.0083	3719.0
84	7	285	AMC	Y	94	1	0.0082	3719.0

Appendix C

STATISTIX 4.1 , 09/26/95, 10:17

VIEW DATA

CASE	BASE	FY	AGE	SFMAINT	SQFT	MAINT
25	35.000	94.000	24.000	1880.0	2339.0	0.8038
26	35.000	94.000	24.000	1880.0	2339.0	0.8038
27	35.000	94.000	24.000	1880.0	2339.0	0.8038
28	35.000	94.000	24.000	1880.0	2339.0	0.8038
29	35.000	94.000	24.000	1880.0	2339.0	0.8038
30	35.000	94.000	24.000	1880.0	2339.0	0.8038
31	35.000	94.000	24.000	1880.0	2339.0	0.8038
32	35.000	94.000	24.000	1880.0	2339.0	0.8038
33	35.000	94.000	24.000	1880.0	2339.0	0.8038
34	35.000	94.000	24.000	1880.0	2339.0	0.8038
35	35.000	94.000	24.000	1880.0	2339.0	0.8038
36	35.000	94.000	24.000	1880.0	2339.0	0.8038
97	41.000	94.000	24.000	1590.0	4624.0	0.3439
98 99	41.000 41.000	94.000	24.000 24.000	1590.0 1590.0	4624.0 4624.0	0.3439
100	41.000	94.000 94.000	24.000	1590.0	4624.0	0.3439
101	41.000	94.000	24.000	1590.0	4624.0	0.3439
101	41.000	94.000	24.000	1590.0	4624.0	0.3439
102	41.000	94.000	24.000	1590.0	4624.0	0.3439
104	41.000	94.000	24.000	1590.0	4624.0	0.3439
105	41.000	94.000	24.000	1590.0	4624.0	0.3439
106	41.000	94.000	24.000	1590.0	4624.0	0.3439
107	41.000	94.000	24.000	1590.0	4624.0	0.3439
108	41.000	94.000	24.000	1590.0	4624.0	0.3439
133	44.000	94.000	29.000	945.00	3160.0	0.2991
134	44.000	94.000	29.000	945.00	3160.0	0.2991
135	44.000	94.000	29.000	945.00	3160.0	0.2991
136	44.000	94.000	29.000	945.00	3160.0	0.2991
137	44.000	94.000	29.000	945.00	3160.0	0.2991
138	44.000	94.000	29.000	945.00	3160.0	0.2991
139	44.000	94.000	29.000	945.00	3160.0	0.2991
140	44.000	94.000	29.000	945.00	3160.0	0.2991
141	44.000	94.000	29.000	945.00	3160.0	0.2991
142	44.000	94.000	29.000	945.00	3160.0	0.2991
143	44.000	94.000	29.000	945.00	3160.0	0.2991
144	44.000	94.000	29.000	945.00	3160.0	0.2991
157	46.000	94.000	28.000	934.00	3867.0	0.2415
158	46.000	94.000	28.000	934.00	3867.0	0.2415
159 160	46.000 46.000	94.000 94.000	28.000 28.000	934.00 934.00	3867.0 3867.0	0.2415 0.2415
161	46.000	94.000	28.000	934.00	3867.0	0.2415
162	46.000	94.000	28.000	934.00	3867.0	0.2415
163	46.000	94.000	28.000	934.00	3867.0	0.2415
164	46.000	94.000	28.000	934.00	3867.0	0.2415
165	46.000	94.000	28.000	934.00	3867.0	0.2415
166	46.000	94.000	28.000	934.00	3867.0	0.2415
167	46.000	94.000	28.000	934.00	3867.0	0.2415
168	46.000	94.000	28.000	934.00	3867.0	0.2415
181	48.000	94.000	23.000	682.00	1847.0	0.3692
182	48.000	94.000	23.000	682.00	1847.0	0.3692
183	48.000	94.000	23.000	682.00	1847.0	0.3692
185	48.000	94.000	23.000	682.00	1847.0	0.3692
187	48.000	94.000	23.000	682.00	1847.0	0.3692
188	48.000	94.000	23.000	682.00	1847.0	0.3692
190	48.000	94.000	23.000	682.00	1847.0	0.3692
191	48.000	94.000	23.000	682.00	1847.0	0.3692
192	48.000	94.000	23.000	682.00	1847.0	0.3692
193	49.000	94.000	26.000	796.00	2478.0	0.3212

194	49.000	94.000	26.000	796.00	2478.0	0.3212
195	49.000	94.000	26.000	796.00	2478.0	0.3212
196	49.000	94.000	26.000	796.00	2478.0	0.3212
197	49.000	94.000	26.000	796.00	2478.0	
198	49.000	94.000	26.000	796.00	2478.0	0.3212
199	49.000	94.000	26.000	796.00	2478.0	0.3212
200	49.000	94.000	26.000	796.00	2478.0	0.3212
201	49.000	94.000	26.000	796.00	2478.0	
202	49.000 49.000	94.000 94.000	26.000	796.00 796.00	2478.0 2478.0	0.3212
204	49.000	94.000	26.000 26.000	796.00	2478.0	0.3212
217 218	51.000	94.000	34.000	1343.0 1343.0	5779.0 5779.0	0.2324
219	51.000	94.000	34.000	1343.0	5779.0	0.2324
220	51.000	94.000	34.000	1343.0	5779.0	0.2324
221	51.000	94.000	34.000	1343.0	5779.0	0.2324
222	51.000	94.000	34.000	1343.0	5779.0	0.2324
223	51.000	94.000	34.000	1343.0	5779.0	0.2324
224	51.000	94.000	34.000	1343.0	5779.0	0.2324
225	51.000	94.000	34.000	1343.0	5779.0	0.2324
241	53.000	94.000	25.000	896.00	2708.0	
242	53.000	94.000	25.000	896.00	2708.0	0.3309
243	53.000	94.000	25.000	896.00	2708.0	
244	53.000	94.000	25.000	896.00	2708.0	0.3309
245	53.000	94.000	25.000	896.00	2708.0	
246 247	53.000 53.000	94.000 94.000	25.000 25.000 25.000	896.00 896.00	2708.0 2708.0	0.3309
248	53.000	94.000	25.000	896.00	2708.0	0.3309
249	53.000	94.000	25.000	896.00	2708.0	0.3309
250	53.000	94.000	25.000	896.00	2708.0	
251	53.000	94.000	25.000	896.00	2708.0	0.3309
252	53.000	94.000	25.000	896.00	2708.0	
253	54.000	94.000	25.000	920.00	2910.0	0.3162
254	54.000	94.000	25.000	920.00	2910.0	0.3162
255	54.000	94.000	25.000	920.00	2910.0	0.3162
256	54.000	94.000	25.000	920.00	2910.0	0.3162
257	54.000	94.000	25.000	920.00	2910.0	0.3162
258	54.000	94.000	25.000	920.00	2910.0	0.3162
259	54.000	94.000	25.000	920.00	2910.0	0.3162
260	54.000	94.000	25.000	920.00	2910.0	0.3162
261	54.000	94.000	25.000	920.00	2910.0	0.3162
262	54.000	94.000	25.000	920.00	2910.0	0.3162
263	54.000	94.000	25.000	920.00	2910.0	0.3162
264	54.000	94.000	25.000	920.00	2910.0	0.3162
301	35.000 35.000	93.000	23.000	1880.0	2295.0	0.8192
302 303	35.000	93.000 93.000	23.000	1880.0 1880.0	2295.0 2295.0	0.8192
304	35.000	93.000	23.000	1880.0	2295.0	0.8192
305	35.000	93.000	23.000	1880.0	2295.0	0.8192
306 307	35.000 35.000	93.000	23.000	1880.0 1880.0	2295.0 2295.0	0.8192 0.8192
308	35.000	93.000	23.000	1880.0	2295.0	0.8192
309	35.000	93.000	23.000	1880.0	2295.0	0.8192
310	35.000	93.000	23.000	1880.0	2295.0	0.8192
311	35.000	93.000	23.000	1880.0	2295.0	0.8192
312	35.000	93.000	23.000	1880.0	2295.0	0.8192
373	41.000	93.000	22.000	1590.0	4479.0	0.3550
374	41.000	93.000	22.000	1590.0	4479.0	0.3550
375	41.000	93.000	22.000	1590.0	4479.0	0.3550
376	41.000	93.000	22.000	1590.0	4479.0	0.3550
377	41.000	93.000	22.000	1590.0	4479.0	0.3550
378	41.000	93.000	22.000	1590.0	4479.0	0.3550
381	41.000	93.000	22.000	1590.0	4479.0	0.3550
382 383	41.000 41.000	93.000 93.000	22.000	1590.0 1590.0	4479.0 4479.0	0.3550
384 409	41.000 41.000 44.000	93.000 93.000 93.000	22.000	1590.0 1590.0 945.00	4479.0 3121.0	0.3550
		22.000	_0.000		5-21.0	0.5020

410	44.000	93.000	28.000	945.00	3121.0	0.3028
411	44.000	93.000	28.000	945.00	3121.0	0.3028
412	44.000	93.000	28.000	945.00	3121.0	0.3028
413	44.000	93.000	28.000	945.00	3121.0	0.3028
414	44.000	93.000	28.000	945.00	3121.0	0.3028
415	44.000	93.000	28.000	945.00	3121.0	0.3028
416	44.000	93.000	28.000	945.00	3121.0	0.3028
417	44.000	93.000	28.000	945.00	3121.0	0.3028
418	44.000	93.000	28.000	945.00	3121.0	0.3028
419	44.000	93.000	28.000	945.00	3121.0	0.3028
420	44.000	93.000	28.000	945.00	3121.0	0.3028
433	46.000	93.000	27.000	934.00	3831.0	0.2438
434	46.000	93.000	27.000	934.00	3831.0	0.2438
435	46.000	93.000	27.000	934.00	3831.0	0.2438
436	46.000	93.000	27.000	934.00	3831.0	0.2438
437	46.000	93.000	27.000	934.00	3831.0	0.2438
438	46.000	93.000	27.000	934.00	3831.0	0.2438
439	46.000	93.000	27.000	934.00	3831.0	0.2438
440		93.000		934.00	3831.0	0.2438
	46.000		27.000			
441	46.000	93.000	27.000	934.00	3831.0	0.2438
442	46.000	93.000	27.000	934.00	3831.0	0.2438
443	46.000	93.000	27.000	934.00	3831.0	0.2438
444	46.000	93.000	27.000	934.00	3831.0	0.2438
457	48.000	93.000	22.000	681.00	1826.0	0.3729
458	48.000	93.000	22.000	681.00	1826.0	0.3729
459	48.000	93.000	22.000	681.00	1826.0	0.3729
460	48.000	93.000	22.000	681.00	1826.0	0.3729
461	48.000	93.000	22.000	681.00	1826.0	0.3729
462	48.000	93.000	22.000	681.00	1826.0	0.3729
463	48.000	93.000	22.000	681.00	1826.0	0.3729
464	48.000	93.000	22.000	681.00	1826.0	0.3729
465	48.000	93.000	22.000	681.00	1826.0	0.3729
466	48.000	93.000	22.000	681.00	1826.0	0.3729
467	48.000	93.000	22.000	681.00	1826.0	0.3729
468	48.000	93.000	22.000	681.00	1826.0	0.3729
469	49.000	93.000	25.000	796.00	2462.0	0.3233
470	49.000	93.000	25.000	796.00	2462.0	0.3233
471	49.000	93.000	25.000	796.00	2462.0	0.3233
472	49.000	93.000	25.000	796.00	2462.0	0.3233
473	49.000	93.000	25.000	796.00	2462.0	0.3233
474	49.000	93.000	25.000	796.00	2462.0	0.3233
475	49.000	93.000	25.000	796.00	2462.0	0.3233
476	49.000	93.000	25.000	796.00	2462.0	0.3233
477	49.000	93.000	25.000	796.00	2462.0	0.3233
478	49.000	93.000	25.000	796.00	2462.0	0.3233
479	49.000	93.000	25.000	796.00	2462.0	0.3233
480	49.000	93.000	25.000	796.00	2462.0	0.3233
493	51.000	93.000	33.000	1343.0	6015.0	0.2233
494	51.000	93.000	33.000	1343.0	6015.0	0.2233
495	51.000	93.000	33.000	1343.0	6015.0	0.2233
496	51.000	93.000	33.000	1343.0	6015.0	0.2233
497	51.000	93.000	33.000	1343.0	6015.0	0.2233
498	51.000	93.000	33.000	1343.0	6015.0	0.2233
499	51.000	93.000	33.000	1343.0	6015.0	0.2233
500	51.000	93.000	33.000	1343.0	6015.0	0.2233
501	51.000	93.000	33.000	1343.0	6015.0	0.2233
502	51.000	93.000	33.000	1343.0	6015.0	0.2233
503	51.000	93.000	33.000	1343.0	6015.0	0.2233
504	51.000	93.000	33.000	1343.0	6015.0	0.2233
517	53.000	93.000	24.000	896.00	2684.0	0.3338
518	53.000	93.000	24.000	896.00	2684.0	0.3338
519	53.000	93.000	24.000	896.00	2684.0	0.3338
520	53.000	93.000	24.000	896.00	2684.0	0.3338
521	53.000	93.000	24.000	896.00	2684.0	0.3338
522	53.000	93.000	24.000	896.00	2684.0	0.3338
523	53.000	93.000	24.000	896.00	2684.0	0.3338
524	53.000	93.000	24.000	896.00	2684.0	0.3338

526 53.000 93.000 24.000 896.00 2684.0 0.3338 527 53.000 93.000 24.000 896.00 2684.0 0.3338 528 53.000 93.000 24.000 896.00 2684.0 0.3338 529 54.000 93.000 24.000 920.00 2910.0 0.3162 531 54.000 93.000 24.000 920.00 2910.0 0.3162 534 54.000 93.000 24.000 920.00 2910.0 0.3162 535 54.000 93.000 24.000 920.00 2910.0 0.3162 536 54.000 93.000 24.000 920.00 2910.0 0.3162 537 54.000 93.000 24.000 920.00 2910.0 0.3162 538 54.000 93.000 24.000 920.00 2910.0 0.3162 577 35.000 92.000 22.000 1880.0 2129.0 0.830	525	53.000	93.000	24.000	896.00	2684.0	0.3338
528 53.000 93.000 24.000 896.00 2684.00 0.3162 531 54.000 93.000 24.000 920.00 2910.0 0.3162 532 54.000 93.000 24.000 920.00 2910.0 0.3162 534 54.000 93.000 24.000 920.00 2910.0 0.3162 535 54.000 93.000 24.000 920.00 2910.0 0.3162 536 54.000 93.000 24.000 920.00 2910.0 0.3162 537 54.000 93.000 24.000 920.00 2910.0 0.3162 538 54.000 93.000 24.000 920.00 2910.0 0.3162 577 35.000 92.000 22.000 1880.0 2129.0 0.8830 578 35.000 92.000 22.000 1880.0 2129.0 0.8830 580 35.000 92.000 22.000 1880.0 2129.0 0.8830 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>							
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532 54,000 93,000 24,000 920,00 2910,0 0.3162 535 54,000 93,000 24,000 920,00 2910,0 0.3162 536 54,000 93,000 24,000 920,00 2910,0 0.3162 537 54,000 93,000 24,000 920,00 2910,0 0.3162 538 54,000 93,000 24,000 920,00 2910,0 0.3162 540 54,000 93,000 24,000 920,00 2910,0 0.3162 540 54,000 93,000 24,000 920,00 2910,0 0.3162 577 35,000 92,000 22,000 1880,0 2129,0 0.8830 579 35,000 92,000 22,000 1880,0 2129,0 0.8830 581 35,000 92,000 22,000 1880,0 2129,0 0.8830 581 35,000 92,000 22,000 1880,0 2129,0 0.8830 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>							
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696 44.000 92.000 27.000 945.00 2875.0 0.3287 709 46.000 92.000 26.000 934.00 3773.0 0.2475 710 46.000 92.000 26.000 934.00 3773.0 0.2475 711 46.000 92.000 26.000 934.00 3773.0 0.2475 712 46.000 92.000 26.000 934.00 3773.0 0.2475 713 46.000 92.000 26.000 934.00 3773.0 0.2475 714 46.000 92.000 26.000 934.00 3773.0 0.2475 715 46.000 92.000 26.000 934.00 3773.0 0.2475 716 46.000 92.000 26.000 934.00 3773.0 0.2475 718 46.000 92.000 26.000 934.00 3773.0 0.2475 719 46.000 92.000 26.000 934.00 3773.0 0.2475 720 46.000 92.000 26.000 934.00 3773.0 0.2475							
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717 46.000 92.000 26.000 934.00 3773.0 0.2475 718 46.000 92.000 26.000 934.00 3773.0 0.2475 719 46.000 92.000 26.000 934.00 3773.0 0.2475 720 46.000 92.000 26.000 934.00 3773.0 0.2475 733 48.000 92.000 21.000 682.00 1774.0 0.3844 734 48.000 92.000 21.000 682.00 1774.0 0.3844 735 48.000 92.000 21.000 682.00 1774.0 0.3844 736 48.000 92.000 21.000 682.00 1774.0 0.3844 737 48.000 92.000 21.000 682.00 1774.0 0.3844							
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737 48.000 92.000 21.000 682.00 1774.0 0.3844	735	48.000	92.000	21.000	682.00	1774.0	0.3844

739	48.000	92.000	21.000	682.00	1774.0	0.3844
740	48.000	92.000	21.000	682.00	1774.0	0.3844
741	48.000	92.000	21.000	682.00	1774.0	0.3844
742	48.000	92.000	21.000	682.00	1774.0	0.3844
743	48.000	92.000	21.000	682.00	1774.0	0.3844
744	48.000	92.000	21.000	682.00	1774.0	0.3844
745	49.000	92.000	24.000	796.00	2329.0	0.3418
746	49.000	92.000	24.000	796.00	2329.0	0.3418
747	49.000	92.000	24.000	796.00	2329.0	0.3418
748	49.000	92.000	24.000	796.00	2329.0	0.3418
749	49.000		24.000		2329.0	
		92.000		796.00		0.3418
750	49.000	92.000	24.000	796.00	2329.0	0.3418
751	49.000	92.000	24.000	796.00	2329.0	0.3418
752	49.000	92.000	24.000	796.00	2329.0	0.3418
753	49.000	92.000	24.000	796.00	2329.0	0.3418
754	49.000	92.000	24.000	796.00	2329.0	0.3418
755	49.000	92.000	24.000	796.00	2329.0	0.3418
756	49.000	92.000	24.000	796.00	2329.0	0.3418
769	51.000	92.000	23.000	1343.0	6015.0	0.2233
770	51.000	92.000	23.000	1343.0	6015.0	0.2233
771	51.000	92.000	23.000	1343.0	6015.0	0.2233
772	51.000	92.000	23.000	1343.0	6015.0	0.2233
773	51.000	92.000	23.000	1343.0	6015.0	0.2233
774	51.000	92.000	23.000	1343.0	6015.0	0.2233
775	51.000	92.000	23.000	1343.0	6015.0	0.2233
776	51.000	92.000	23.000	1343.0	6015.0	0.2233
777	51.000	92.000	23.000	1343.0	6015.0	0.2233
778		92.000	23.000	1343.0	6015.0	0.2233
	51.000					
779	51.000	92.000	23.000	1343.0	6015.0	0.2233
780	51.000	92.000	23.000	1343.0	6015.0	0.2233
793	53.000	92.000	23.000	896.00	2639.0	0.3395
794	53.000	92.000	23.000	896.00	2639.0	0.3395
795	53.000	92.000	23.000	896.00	2639.0	0.3395
796	53.000	92.000	23.000	896.00	2639.0	0.3395
797	53.000	92.000	23.000	896.00	2639.0	0.3395
798	53.000	92.000	23.000	896.00	2639.0	0.3395
799	53.000	92.000	23.000	896.00	2639.0	0.3395
800	53.000	92.000	23.000	896.00	2639.0	0.3395
801	53.000	92.000	23.000	896.00	2639.0	0.3395
802	53.000	92.000	23.000	896.00	2639.0	0.3395
803	53.000	92.000	23.000	896.00	2639.0	0.3395
804	53.000	92.000	23.000	896.00	2639.0	0.3395
805	54.000	92.000	23.000	920.00	2834.0	0.3246
806	54.000	92.000	23.000	920.00	2834.0	0.3246
807	54.000	92.000	23.000	920.00	2834.0	0.3246
809	54.000	92.000	23.000	920.00	2834.0	0.3246
810	54.000	92.000	23.000	920.00	2834.0	0.3246
			23.000			
811	54.000	92.000	23.000	920.00	2834.0	0.3246
812	54.000	92.000	23.000	920.00	2834.0	0.3246
813	54.000	92.000	23.000	920.00	2834.0	0.3246
	54.000	92.000		920.00		0.3246
814			23.000		2834.0	
815	54.000	92.000	23.000	920.00	2834.0	0.3246
816	54.000	92.000	23.000	920.00	2834.0	0.3246
853	35.000	91.000	21.000	1880.0	2129.0	0.8830
854	35.000	91.000	21.000	1880.0	2129.0	0.8830
855	35.000	91.000	21.000	1880.0	2129.0	0.8830
856	35.000	91.000	21.000	1880.0	2129.0	0.8830
857	35.000	91.000	21.000	1880.0	2129.0	0.8830
858	35.000	91.000	21.000	1880.0	2129.0	0.8830
859	35.000	91.000	21.000	1880.0	2129.0	0.8830
860	35.000	91.000	21.000	1880.0	2129.0	0.8830
861	35.000	91.000	21.000	1880.0	2129.0	0.8830
862	35.000	91.000	21.000	1880.0	2129.0	0.8830
863	35.000	91.000	21.000	1880.0	2129.0	0.8830
864	35.000	91.000	21.000	1880.0	2129.0	0.8830
925	41.000	91.000	20.000	1590.0	3994.0	0.3981
926	41.000	91.000	20.000	1590.0	3994.0	0.3981

927	41.000	91.000	20.000	1590.0	3994.0	0.3981
928 929	41.000 41.000	91.000 91.000	20.000 20.000	1590.0 1590.0	3994.0 3994.0	0.3981 0.3981
930	41.000	91.000	20.000	1590.0	3994.0	0.3981
931 932	41.000 41.000	91.000 91.000	20.000 20.000	1590.0 1590.0	3994.0 3994.0	0.3981 0.3981
933	41.000	91.000	20.000	1590.0	3994.0	0.3981
934 935	41.000 41.000	91.000 91.000	20.000 20.000	1590.0 1590.0	3994.0 3994.0	0.3981 0.3981
936	41.000	91.000	20.000	1590.0	3994.0	0.3981
961 962	44.000	91.000 91.000	26.000	945.00	2800.0	0.3375
963	44.000 44.000	91.000	26.000 26.000	945.00 945.00	2800.0 2800.0	0.3375 0.3375
964	44.000	91.000	26.000	945.00	2800.0	0.3375
965 966	44.000 44.000	91.000 91.000	26.000 26.000	945.00 945.00	2800.0 2800.0	0.3375 0.3375
967	44.000	91.000	26.000	945.00	2800.0	0.3375
968 969	44.000 44.000	91.000 91.000	26.000 26.000	945.00 945.00	2800.0 2800.0	0.3375 0.3375
970	44.000	91.000	26.000	945.00	2800.0	0.3375
971 972	44.000 44.000	91.000 91.000	26.000 26.000	945.00 945.00	2800.0 2800.0	0.3375 0.3375
985	46.000	91.000	25.000	934.00	3773.0	0.2475
986 987	46.000 46.000	91.000 91.000	25.000 25.000	934.00 934.00	3773.0 3773.0	0.2475 0.2475
988	46.000	91.000	25.000	934.00	3773.0	0.2475
989 990	46.000 46.000	91.000 91.000	25.000 25.000	934.00 934.00	3773.0 3773.0	0.2475 0.2475
991	46.000	91.000	25.000	934.00	3773.0	0.2475
992 993	46.000 46.000	91.000 91.000	25.000 25.000	934.00 934.00	3773.0 3773.0	0.2475 0.2475
994	46.000	91.000	25.000	934.00	3773.0	0.2475
995 996	46.000	91.000	25.000	934.00 934.00	3773.0 3773.0	0.2475 0.2475
1009	46.000 48.000	91.000 91.000	25.000 20.000	682.00	1780.0	0.3831
1010	48.000	91.000	20.000	682.00	1780.0	0.3831
1011 1012	48.000 48.000	91.000 91.000	20.000 20.000	682.00 682.00	1780.0 1780.0	0.3831
1013	48.000	91.000	20.000	682.00	1780.0	0.3831
1014 1015	48.000 48.000	91.000 91.000	20.000 20.000	682.00 682.00	1780.0 1780.0	0.3831
1016	48.000	91.000	20.000	682.00	1780.0	0.3831
1017 1018	48.000 48.000	91.000 91.000	20.000 20.000	682.00 682.00	1780.0 1780.0	0.3831 0.3831
1019	48.000	91.000	20.000	682.00	1780.0	0.3831
1020 1021	48.000 49.000	91.000 91.000	20.000 23.000	682.00 796.00	1780.0 2516.0	0.3831 0.3164
1022	49.000	91.000	23.000	796.00	2516.0	0.3164
1023 1024	49.000 49.000	91.000 91.000	23.000 23.000	796.00 796.00	2516.0 2516.0	0.3164 0.3164
1025	49.000	91.000	23.000	796.00	2516.0	0.3164
1026 1027	49.000 49.000	91.000 91.000	23.000 23.000	796.00 796.00	2516.0 2516.0	0.3164 0.3164
1028	49.000	91.000	23.000	796.00	2516.0	0.3164
1029 1030	49.000 49.000	91.000 91.000	23.000 23.000	796.00 796.00	2516.0 2516.0	0.3164 0.3164
1030	49.000	91.000	23.000	796.00	2516.0	0.3164
1032	49.000	91.000	23.000	796.00	2516.0	0.3164
1045 1046	51.000 51.000	91.000 91.000	31.000 31.000	1343.0 1343.0	6015.0 6015.0	0.2233
1047	51.000	91.000	31.000	1343.0	6015.0	0.2233
1048 1049	51.000 51.000	91.000 91.000	31.000 31.000	1343.0 1343.0	6015.0 6015.0	0.2233
1050	51.000	91.000	31.000	1343.0	6015.0	0.2233
1051 1052	51.000 51.000	91.000 91.000	31.000 31.000	1343.0 1343.0	6015.0 6015.0	0.2233
1053	51.000	91.000	31.000	1343.0	6015.0	0.2233

1054 1055	51.000 51.000	91.000 91.000	31.000 31.000	1343.0 1343.0	6015.0 6015.0	0.2233 0.2233
1056	51.000	91.000	31.000	1343.0	6015.0	0.2233
1069	53.000	91.000	22.000	896.00	2639.0	0.3395
1070	53.000	91.000	22.000	896.00	2639.0	0.3395
1071	53.000	91.000	22.000	896.00	2639.0	0.3395
1072	53.000	91.000	22.000	896.00	2639.0	0.3395
1073	53.000	91.000	22.000	896.00	2639.0	0.3395
1074	53.000	91.000	22.000	896.00	2639.0	0.3395
1075	53.000	91.000	22.000	896.00	2639.0	0.3395
1076	53.000	91.000	22.000	896.00	2639.0	0.3395
1077	53.000	91.000	22.000	896.00	2639.0	0.3395
1078	53.000	91.000	22.000	896.00	2639.0	0.3395
1079	53.000	91.000	22.000	896.00	2639.0	0.3395
1080	53.000	91.000	22.000	896.00	2639.0	0.3395
1081	54.000	91.000	22.000	920.00	2850.0	0.3228
1082	54.000	91.000	22.000	920.00	2850.0	0.3228
1083	54.000	91.000	22.000	920.00	2850.0	0.3228
1084	54.000	91.000	22.000	920.00	2850.0	0.3228
1085	54.000	91.000	22.000	920.00	2850.0	0.3228
1086	54.000	91.000	22.000	920.00	2850.0	0.3228
1087	54.000	91.000	22.000	920.00	2850.0	0.3228
1088	54.000	91.000	22.000	920.00	2850.0	0.3228
1089	54.000	91.000	22.000	920.00	2850.0	0.3228
1090	54.000	91.000	22.000	920.00	2850.0	0.3228
1091	54.000	91.000	22.000	920.00	2850.0	0.3228
1092	54.000	91.000	22.000	920.00	2850.0	0.3228

Appendix D

Figure D-1
Histogram (AFMC and SPC Bases)

Box and Whisker Plot (AFMC and SPC Bases)

Figure D-3 Wilk-Shapiro/Rankit Plot (AFMC and SPC Bases)

Figure D-4 Scatter Plot: MBTU vs. HDD (AFMC and SPC Bases)

Figure D-5 Scatter Plot: MBTU vs. CDD (AFMC and SPC Bases)

Figure D-6 Scatter Plot: MBTU vs. CHDD (AFMC and SPC Bases)

Figure D-7 Scatter Plot: MBTU vs. SQFT (AFMC and SPC Bases)

Figure D-8 Plot of Fitted Values vs. Standardized Residuals (AFMC and SPC Bases)

Figure D-9 Wilk-Shapiro Plot of Standardized Residuals (AFMC and SPC Bases) Appendix E

Figure E-1 Histogram (AMC and ACC Bases)

Figure E-2 Box and Whisker Plot (AMC and ACC Bases)

Figure E-3 Wilk-Shapiro/Rankit Plot (AMC and ACC Bases)

Figure E-4
Scatter Plot: MBTU vs. HDD (AMC and ACC Bases)

Figure E-5
Scatter Plot: MBTU vs. CDD (AMC and ACC Bases)

Figure E-6
Scatter Plot: MBTU vs. CHDD (AMC and ACC Bases)

Figure E-7
Scatter Plot: MBTU vs. SQFT (AMC and ACC Bases)

Figure E-8
Plot of Fitted Values vs. Standardized Residuals (AMC and ACC Bases)

Figure E-9 Wilk-Shapiro Plot of Standardized Residuals (AMC and ACC Bases) Appendix F Figure F-1 Histogram (AETC and ACC Bases) Figure F-2
Box and Whisker Plot (AETC and ACC Bases)

Figure F-3
Wilk-Shapiro/Rankit Plot (AETC and ACC Bases)

Figure F-4
Scatter Plot: MBTU vs. HDD (AETC and ACC Bases)

Figure F-5
Scatter Plot: MBTU vs. CDD (AETC and ACC Bases)

Figure F-6
Scatter Plot: MBTU vs. CHDD (AETC and ACC Bases)

Figure F-7
Scatter Plot: MBTU vs. SQFT (AETC and ACC Bases)

Figure F-8
Plot of Fitted Values vs. Standardized Residuals (AETC and ACC Bases)

Figure F-9 Wilk-Shapiro Plot of Standardized Residuals (AETC and ACC Bases) Appendix G Figure G-1 Histogram (ACC Bases) Figure G-2 Box and Whisker Plot (ACC Bases) Figure G-3 Wilk-Shapiro/Rankit Plot (ACC Bases) Figure G-4
Scatter Plot: MBTU vs. HDD (ACC Bases)

Figure G-5
Scatter Plot: MBTU vs. CDD (ACC Bases)

Figure G-6 Scatter Plot: MBTU vs. CHDD (ACC Bases) Figure G-7
Scatter Plot: MBTU vs. SQFT (ACC Bases)

Figure G-8
Plot of Fitted Values vs. Standardized Residuals (ACC Bases)

Figure G-9 Wilk-Shapiro Plot of Standardized Residuals (ACC Bases) Appendix H Figure H-1 Histogram (ACC Bases w/ Supplemental Data)

Figure H-2 Box and Whisker Plot (ACC Bases w/ Supplemental Data)

Figure H-3 Wilk-Shapiro/Rankit Plot (ACC Bases w/ Supplemental Data)

Figure H-4
Scatter Plot: MBTU vs. HDD (ACC Bases w/ Supplemental Data)

Figure H-5
Scatter Plot: MBTU vs. CDD (ACC Bases w/ Supplemental Data)

Figure H-6 Scatter Plot: MBTU vs. CHDD (ACC Bases w/ Supplemental Data)

Figure H-7
Scatter Plot: MBTU vs. SQFT (ACC Bases w/ Supplemental Data)

Figure H-8 Scatter Plot: MBTU vs. AGE (ACC Bases w/ Supplemental Data)

Figure H-9
Scatter Plot: MBTU vs. MAINT (ACC Bases w/ Supplemental Data)

Figure H-10 Plot of Fitted Values vs. Standardized Residuals (ACC Bases w/ Supplemental Data)

Figure H-11 Wilk-Shapiro Plot of Standardized Residuals (ACC Bases w/ Supplemental Data) Appendix I

Figure I-1 Histogram (Nonflying Bases)

Figure I-2 Box and Whisker Plot (Nonflying Bases)

Figure I-3 Wilk-Shapiro/Rankit Plot (Nonflying Bases)

Figure I-4 Scatter Plot: MBTU vs. HDD (Nonflying Bases)

Figure I-5 Scatter Plot: MBTU vs. CDD (Nonflying Bases)

Figure I-6 Scatter Plot: MBTU vs. CHDD (Nonflying Bases)

Figure I-7
Scatter Plot: MBTU vs. SQFT (Nonflying Bases)

Figure I-8 Plot of Fitted Values vs. Standardized Residuals (Nonflying Bases)

Figure I-9
Wilk-Shapiro Plot of Standardized Residuals (Nonflying Bases)

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